

# PE MAGNUM METAL LOCATOR

ANDY FLIND

Cheap metal detectors are usually disappointing in use whilst good ones tend to be very expensive. Although there is a lot of work involved in building the machine in this article, it can be completed for around £40-50, less than a quarter of the cost of most ready-made ones of similar performance. It is not strictly a design for the beginner to attempt, but a step by step construction and test procedure has been devised to make it as simple as possible. The only absolutely essential item of test equipment required is a reasonable quality test meter.

Until now, most metal detector designs for the home constructor have been BFOs. True, there have been one or two notable exceptions, but even these were relatively unsophisticated examples of their type, so readers might be interested in a brief description of the basic methods of detection and the reasons for the choice of system used in this design.

## TYPES OF DETECTOR

Broadly speaking there are five main ways of detecting metal; BFO (beat frequency oscillator), induction balance, pulse induction, off resonance, and the magnetometer. The latter works by detecting small anomalies in the Earth's magnetic field strength. It's fascinating but quite useless for treasure hunting since it can detect only ferrous objects. The BFO and off resonance types both operate by detecting the small changes in the search coil inductance which occur when a metal object is present. Both suffer from a basically poor sensitivity. Some sophisticated attempts have recently been made to produce a really good off resonance machine, so far without obvious success.

Pulse induction detectors are another matter however; good ones are very sensitive indeed and some of the most expensive detectors currently available are these. They operate by exposing the ground to powerful pulses of magnetism and listening between the pulses for signals due to eddy currents set up in any metal objects present in the field. Despite their sensitivity they have a couple of important drawbacks. Their battery consumption is heavy due to the power required by the pulsed transmitter, and they are extremely sensitive to even tiny ferrous objects. Their use is thus primarily restricted to beach searching, where objects are likely to be buried at considerable depths, and where large holes can be easily and rapidly dug. On inland sites, their users can become discouraged by the frequent digging of large holes in hard ground to recover rusty nails, etc.

This leaves the induction balance types which have become more or less the standard general purpose detector for both serious treasure hunters and detecting hobbyists alike. It has two coils in its search head, one of which is fed with a signal which sets up an alternating field around it. The other coil is placed so that normally the field around it balances and it has no electrical output. A metal object approaching the coils will distort the field, resulting in an imbalance so the pickup coil will produce an output. This can be amplified and used to inform the operator of a "find" in a variety of ways. Frequently in simple detectors an audio modulated transmitted signal is used, the output from the pickup coil then being amplified and demodulated like an AM radio signal. There are many possible coil arrangements, but most detectors available today use one of the two shown in Fig. 1. Fig. 1(a) shows a "widescan" coil, so called because its most sensitive area (shaded) extends right across the coils. Fig. 1(b) shows a "pinpoint" type, also known as a "4B". In the author's experience the pinpoint is by far the better coil in use, as widescans have poor pinpointing ability and tend to give false signals for ferrous objects off centre, coins on edge and the like. It's noticeable that many of the best imported American machines use pinpoint coils.

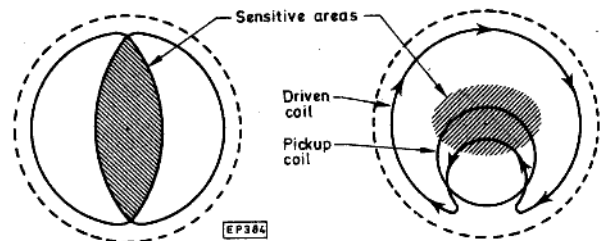


Fig. 1 (left). 'Widescan' coil layout; (right) 'Pinpoint' coil layout

## DISCRIMINATION

All of this is fine, but there are a couple of extra refinements necessary in a really good metal detector. One of these is the ability to discriminate between unwanted junk such as silver paper, scraps of iron etc., and desired objects. The other is some means of eliminating false signals due to "ground effect". Ground capacitance effects can easily be prevented by Faraday shielding around the coils, but most inland soils contain a proportion of iron oxide which gives a signal similar to a piece of ferrite. Beaches wet with seawater on the other hand are slightly conductive, and this too causes false signals to be produced in the pickup coil. Obviously some means of "tuning out" these effects will improve the detector considerably.

Fortunately the signals from the search coil consist of more than just amplitude variations; they also contain information in the form of phase shifts which differ markedly according to the type of object causing the signal. With a relatively simple phase sensitive detector therefore, a machine can be designed which will totally reject ground effects and can also, with practice on the part of the user, eliminate the majority of the rubbish detected without the necessity of having to dig it up.

## NOMENCLATURE

Some of the terms used by manufacturers to describe their machines in recent years have been somewhat confusing so, before we proceed, a note on these may not be amiss. 'VLF' stands for "very low frequency". The ability to discriminate from phase information against thin section objects like foil depends on frequency. At higher frequencies, 'Skin effect' eddy current conduction makes such discrimination ineffective. Therefore manufacturers began using lower and lower frequencies, at least one machine actually worked at less than 2kHz. This created problems of its own, as at such low frequencies sensitivity to cupro-nickel coins is not so good and "Q" problems arise in the coil design. Most detectors nowadays operate somewhere between 10 and 20kHz. where discrimination is still excellent but sensitivity and coil design problems do not arise.

"GEB" means "ground exclusion balance" and refers to the phase sensitive means of excluding ground effect. "TR" means "transmit-receive" and is often used to describe the discriminate mode, suggesting that the machines operate with different frequencies or coil configurations in the different modes--they don't: the only thing that is changed between modes is the phase reference point. It is not possible to avoid ground effect and discriminate at the same time, so one normally searches in GEB mode, and on finding an object, checks it with the discriminate mode before digging. Beer can pull rings can be rejected by the way, but machines capable of doing this will also reject any cupro-nickel coin smaller than a 10p when set to do so. It is probably better to tolerate the rings - many charities now collect these anyway.

## BLOCK

Fig. 2 (dotted) shows a schematic of the Magnum detector. The drive oscillator sets up a field around the search coil, and the pickup coil is positioned so that it only gives an electrical output when a metal object distorts this field. The operating frequency of these stages is approximately 15kHz. Signals from the pickup coil are amplified, buffered and then inverted so that non-inverted and inverted versions of it are simultaneously available. These are fed to the two inputs of an electronic changeover switch, operated by a reference signal derived from the drive oscillator. This reference signal has first been passed through a phase shifting network which can be adjusted as required by the user. The output from the switch is passed through a 3rd order low-pass active filter with a cut-off point set at 40Hz. which removes practically all of the 15kHz signal, leaving only the average d.c. level.

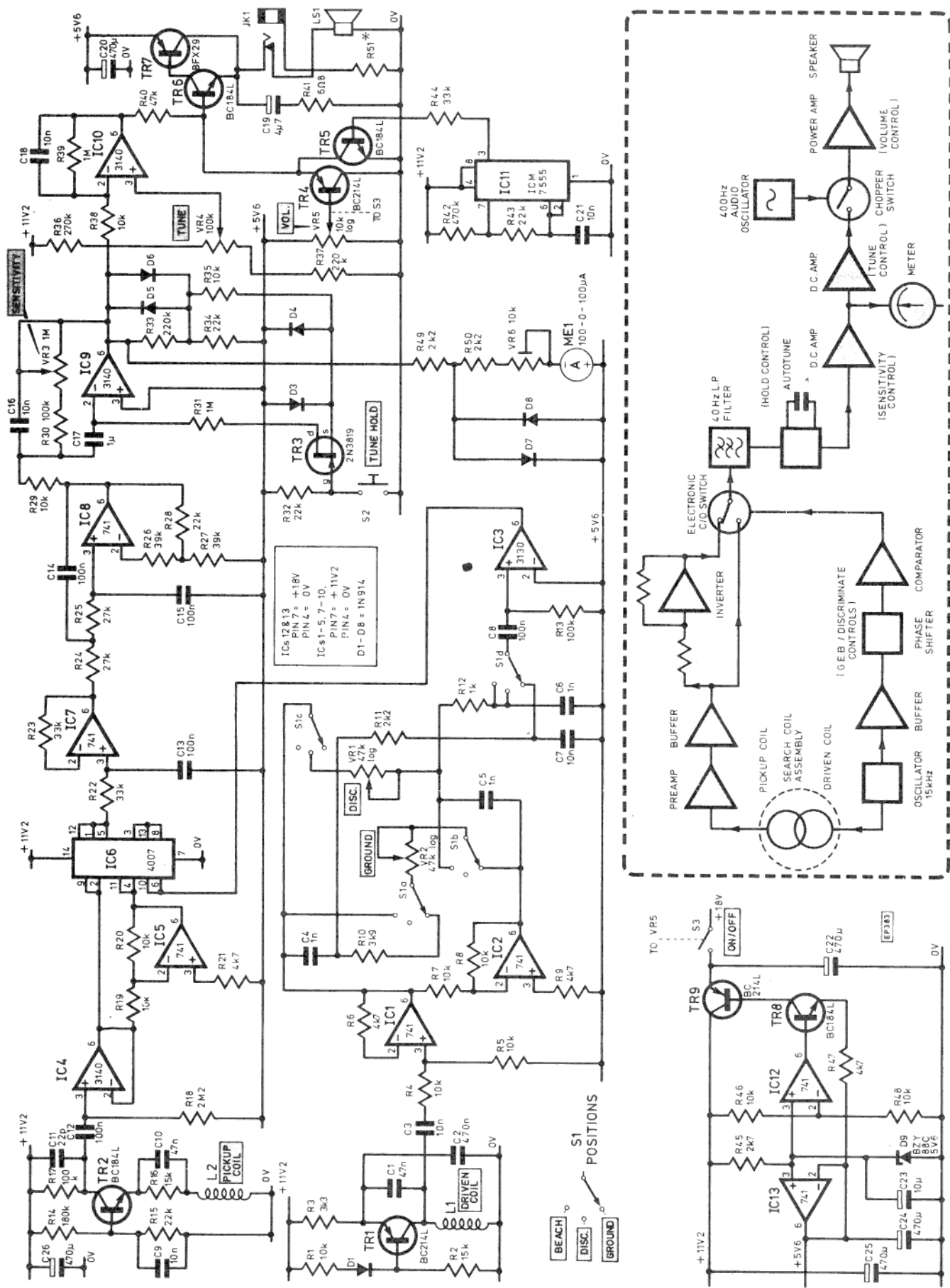
Any given signal producing object causes changes in both magnitude and phase of the received signal, so by adjusting the phase shift network correctly a point can be found where these changes either cancel out or cause a net fall in the d.c. level, enabling unwanted signals from ground, foil, iron etc., to be eliminated. Incidentally, most similar designs to date have used either pulse sampling phase detectors, or have selected only half-cycles of the input signal. The use of the inverter and changeover switch requires very few extra components and greatly improves the signal-to-noise ratio, ultimately resulting in more sensitivity.

After the filter, the d.c. signal is amplified. It is only changes in the signal that are of interest, so a means of "tuning out" the initial standing d.c. level is required. In simple machines this is a manual control, but the need for readjustment after each operation of the phase controls - say switching from "ground" to "discriminate" - makes some form of automatic tuning desirable. On most commercial machines a "tune" button resets the output to zero every time it is pressed, but these are notoriously prone to drift. Attempts to use continuously resetting systems have been made, but this tends to lower the overall sensitivity as most manufacturers use rather crude filtering, resulting in considerable delay in the response to a detected object. In effect the autotune tries to reset the output to zero at the same time as the detected object is trying to cause it to rise! The highly efficient filtering used in this design ensures an instant response to a signal, so a continuously resetting tuning system can be used. This does away with all the drift problems, and allows the machine to be used continuously at maximum sensitivity if required. A "freeze" button is provided to stop the tuning action whilst pinpointing the exact position of finds or discriminating.

After the autotune and amplifier stage the signal is fed to a centre-zero meter; in "discriminate" this indicates positive for "good" finds and negative for "bad" ones. Then it goes to a further amplifier with a control which sets the point at which the audio output is to start. The output from this is of course still d.c., so it is chopped up by an audio oscillator, providing a signal which only needs a power output stage to drive the loudspeaker.

## CIRCUIT

Fig. 2 shows the complete circuit of the machine. TR1 and associated components form the drive oscillator, which provides a very pure 15kHz sinewave output. IC1 buffers part of this signal and the circuitry around IC2 introduces the phase shift as required. In "ground" the available shift is about -10 to +40 degrees, whilst in "discriminate" and "beach" it is about 0 to -170 degrees. IC3 is a comparator; the 3130 was chosen for its high slew rate and good output drive signal for the CMOS switch IC6. TR2 is the received signal preamp and is connected as a common base amplifier. This and oscillator TR1 are both based on



designs which have been used in several manufactured machines because they are simple and work well. The receive coil L2 is untuned; this, coupled with the low impedance input load of TR2 ensures the predictable phase response required for reliable discrimination. The output of TR2 is at high impedance so IC4 acts as a buffer, whilst IC5 is a unity gain inverter. IC6 is connected as a CMOS electronic changeover analogue signal switch. IC7 and IC8 together are the 3rd order low-phase active filter.

IC9 is a d.c. amplifier and also the auto-tune stage. The action of this is probably easier to understand if one first considers an ordinary opamp inverting amplifier, as shown in Fig. 3. If the +input is at 0 volts, the -input must also be at 0 volts, so if a voltage is applied to the input resistor  $R_{in}$  the output will change until it restores the 0 volts at the -input via  $R_f$ . Now consider the effect of placing a capacitor at point "x". If the output is connected directly to the -input, it will go to 0 volts. If at the same time a voltage is applied to  $R_{in}$ , the capacitor will acquire a charge. If the output is now disconnected from the -input it will remain at 0 volts because the capacitor will retain the charge necessary to the input voltage. A change in the input voltage will be reflected in a change in the output voltage, the gain given by  $R_f/R_{in}$ . In this way an amplifier can be constructed using only one opamp which will offset large d.c. voltages and yet provide high d.c. amplification of very small input voltage changes.

In the main circuit TR3 provides a means of connecting the output to the -input. The output is divided by R33 and R34 and fed through R31, so that the reset rate is relatively slow but continuous, as TR3 is normally conducting. If the tuning error is very large however, as it would be after switching on or operating the discriminating controls, D5 or D6 will conduct and greatly accelerate the tuning rate. D3 and D4 prevent the gate junction of TR3 from becoming forward biased at any time.

VR4 sets the threshold of IC10 and is normally adjusted to that it's output is at negative rail voltage. On receipt of a signal it rises towards positive. IC11 is a low-power 555 timer connected as an astable oscillator, giving very short (about 100 microsecond) negative pulses at about 400Hz. Thus TR5 is normally on and turns off only during these pulses so after R40 any output from IC10 is chopped into short positive going pulses. This is the ideal waveform to create lots of noise with an economic power consumption. The volume control in a design such as this is normally only required to limit the maximum noise level, so in this design VR5 and TR4 act as an adjustable clamp. In this way the sensitivity is not reduced if the volume has to be kept turned down. TR6 and TR7 are a complementary Darlington pair, their current gain enabling the signal to drive the loudspeaker or headphones.

## SUPPLIES

Two separate power supplies are used in this machine. The bulk of the circuitry is supplied with 18 volts from two PP3 batteries in series, regulated by the circuit around IC12 and IC13. With so many opamps its far easier to arrange the design around a centre-tapped supply, so the reference generated by the Zener is buffered by IC13. It is then doubled by IC12, TR8 and TR9, to give a regulated positive rail of twice the Zener voltage, nominally +11.2

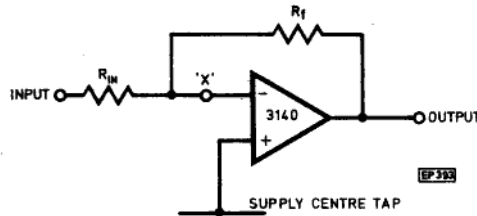


Fig. 3. Op-amp inverter

## COMPONENTS

### RESISTORS

R1,4,5,7,8,19,20,29,35,38,46,48	10k
R2,16	15k
R3	3k3
R6,9,21,47	4k7
R10	3k9
R11,49,50	2k2
R12	1k
R13,17,30	100k
R14	180k
R15,28,32,34,43	22k
R18	2M2
R22,23,44	33k
R24,25	27k
R26,27	39k
R31,39	1M
R33,37	220k
R36	270k
R40	47k
R41	6R8
R42	470k
R45	2k7

### POTENTIOMETERS

VR1,2	47k log carbon
VR3	1M lin. carbon
VR4	100k lin. carbon
VR5	10k log with switch
VR6	10k preset, sub min horiz.

### CAPACITORS

C1,C10	47n polyester
C2	470n polyester
C3,7,9,16,18,21	10n polyester
C4,5,6	1n polystyrene
C8,12,13,14,15	100n polyester
C11	22p polystyrene
C17	1µF polycarbonate
C19	4.7µF 63v electrolytic
C20,24,25,26	470µF 16v electrolytic
C22	470µF 25v electrolytic
C23	10µF 25v electrolytic

### DIODES

D1 to 8	1N914
D9	BZY88C 5V6, 5.6v Zener

### TRANSISTORS

TR1,4,9	BC214L
TR2,5,6,8	BC184L
TR3	2N3819
TR7	BFX29

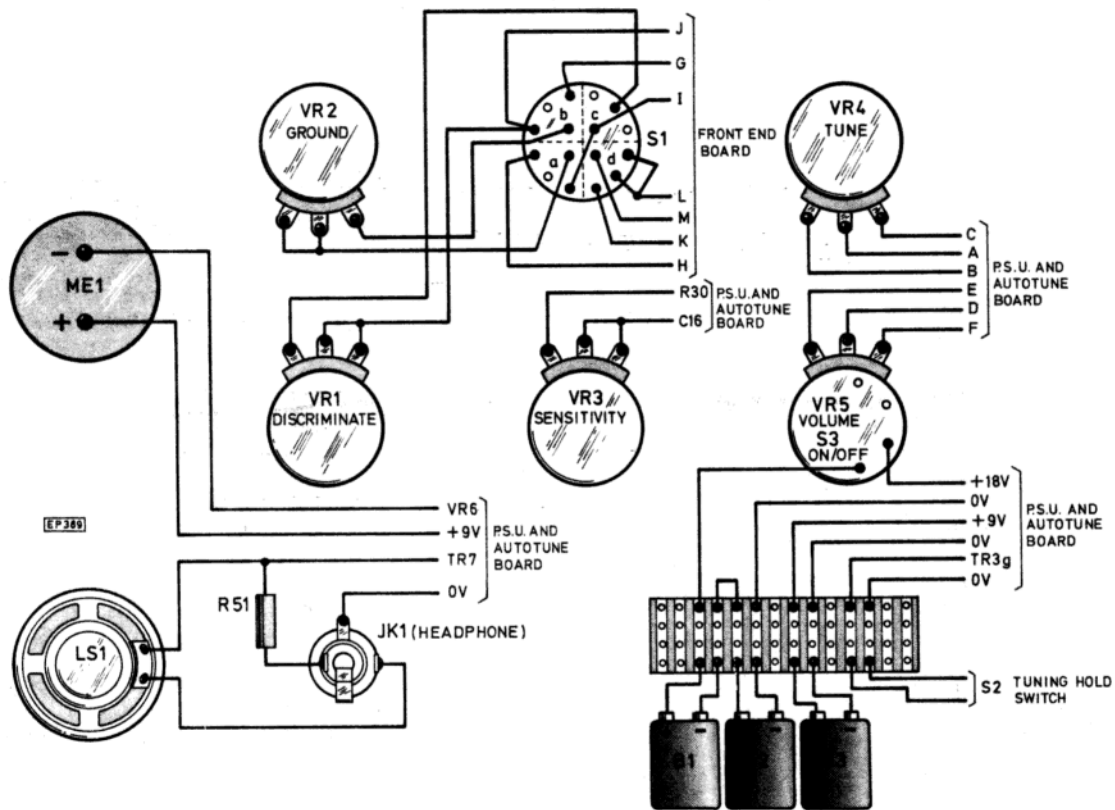
### INTEGRATED CIRCUITS

IC1,2,5,7,8,12,13	741
IC3	CA3130
IC4,9,10	CA3140
IC6	4007UBE
IC11	ICM7555

### MISCELLANEOUS

S1, 4-pole 3-way rotary switch, S2, miniature press to make, Meter, 100-0-100 microamp center zero, LS1- 2-1/2 in. 8-ohm loudspeaker, 12 off 8-pin d.i.l. i.c. holders, 1 off 14-pin d.i.l. i.c. holder, 5-pin DIN plug and socket, headphone socket, 3 PP3 battery clips, 32 and 36 SWG enamelled copper wire, 5A bare tinned copper fuse wire, 2 metres of 4-core individually screened cable, case, Vero type 75-1411-D, 6 control knobs, approx 25mm skirt, plus plastic plumbing components, "Melaware" plate, glassfibre repair kit etc. to make coil, stem, and handle - see text.

Kits available from **Maplin Electronics Supplies Ltd.**



**Fig. 4. Connections to controls and headphone jack socket. Other connections as marked on p.c.b. overlays**

volts. This arrangement has been used in preference to an integrated regulator since it will operate until the battery voltage has fallen to only 0.1 volt above the regulator output. Most integrated regulators require a differential of at least 2 volts, which in practice means that the batteries have to be replaced rather more frequently. The total power consumption of all this circuitry is about 20mA, less than many radios at normal volume.

Power for the loudspeaker output stage comes from a separate 9 volt battery, as this is the simplest way of avoiding decoupling difficulties in this very sensitive circuit. An extra PP3 is far smaller than the decoupling capacitors which would otherwise be required. Only the one power supply switch is required as the output draws no current unless an input signal is present.

## CONSTRUCTION

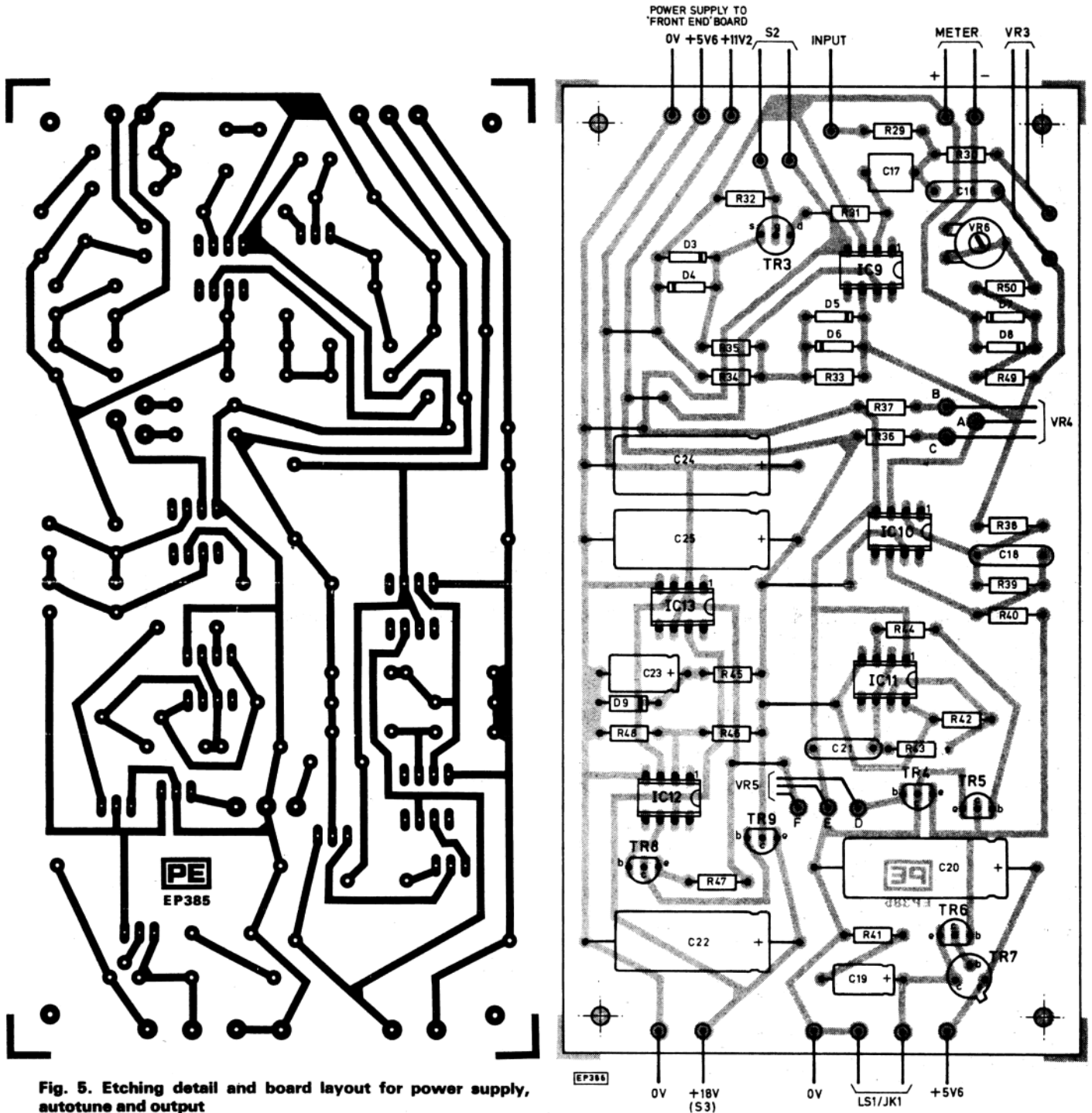
Construction is on two printed circuit boards and should be adhered to as this is a very sensitive circuit indeed; the result of any changes may well prove to be severe instability. The two boards are stacked vertically in the final assembly resulting in a control box which is smaller and neater than many very expensive manufactured products.

The board containing the power supply, autotune and output should be built first as the power supply will be required for testing the "front end" board (Fig. 5).

## ASSEMBLY DETAILS

Start construction by fitting the six links. The fit R45 to R48, C22 to C25, ZD1, TR8, TR9, IC12 and IC13. Apply the 18 volt battery via a 100mA meter and a 220 ohm series resistor, which will limit the current if any faults are present. It's as well to use this resistor throughout the testing of both boards. After a brief surge as the electrolytics charge the current should settle to about 5mA. Check that about 11 volts appears across C25. and about 5.5 volts across C24. This completes the power supply section.

Continue by fitting R40 and R41, C19 and C20, TR6 and TR7. Hook up the speaker, apply the 9 volt power supply via the 100mA meter and a 100 ohm resistor, again in case a fault is present. After a brief surge the current drawn should drop to zero. A finger on R40 and the battery positive at the same time should cause a crackle and an indicated current flow. Fit R42 to R44, C21, TR5 and IC11. IC11 is the low power 555 timer; despite the manufacturers' notes to the contrary these are a little sensitive to handling so treat it with care and use a holder. I.c. holders are advisable throughout in fact; there is ample room for them. Apply both power supplies. A finger on 9 volts positive and on R40 should now produce the 400Hz output tone, albeit possibly at rather



**Fig. 5. Etching detail and board layout for power supply, autotune and output**

low volume. After this the 100R resistor can be left out of the 9 volt supply during testing, although the 220R in the 18 volt supply should be retained. Fit TR4 and hook up VR5. Apply power supplies, place fingers on R40 and 9 volts positive, and check that the volume can be controlled with VR5. This is one of those many jobs in electronics for which one requires three hands!

Fit R33, R34, R36 to R39, C18, and IC10. IC10 may be in either an 8-pin d.i.l. package, or the round metal T079 version. You can now hook up VR4 and apply power. It should be possible to turn the output tone on and off with VR4 - gradually, since the input of IC10 at this stage is effectively taken to the supply centre-tap via R33 and R34 which reduces its gain somewhat. If there is no output tone check that the volume isn't turned right down.

## FINAL TEST

Fit all the remaining components to this board. Hook up S2, VR3 and the meter. Short the input point to the battery centre-tap. Apply power; the meter should return to zero within a couple of seconds due to the autotune action. Adjust VR4 to just below the

tone threshold point. Touch the 18 volt battery positive with one hand, and, taking a 10M resistor in the other, touch the top end of R29 via the resistor. This should produce a brief burst of tone and a positive jump on the meter, which will then return to zero. Repeat this procedure whilst pressing S2 - the sound and meter deflection produced should then be continuous. Press the button, and touch either of the 18 volt battery leads end the bottom of C17. This should cause the meter to drive fully up or down, and its full scale deflection can then be adjusted with VR6.

Next month: details will be given of the remainder of the construction and using the detector.

Part 2 (Practical Electronics, Sept. 1980)

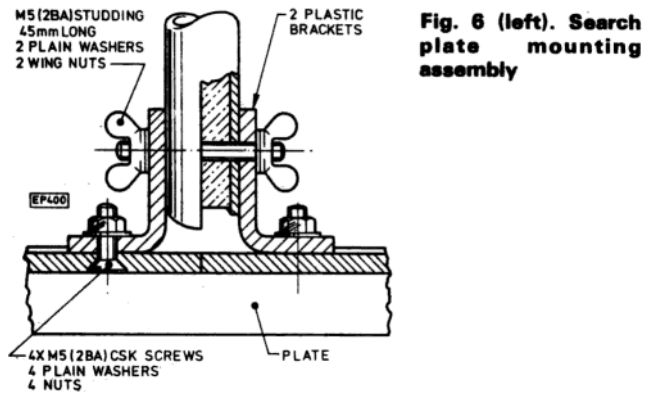
LAST month the general principles of the GEB detector were explained, and construction of a machine began with a p.c.b. comprising power supply, auto-tuning and output stages. This month the remainder of the construction will be covered.

**SEARCH COILS**

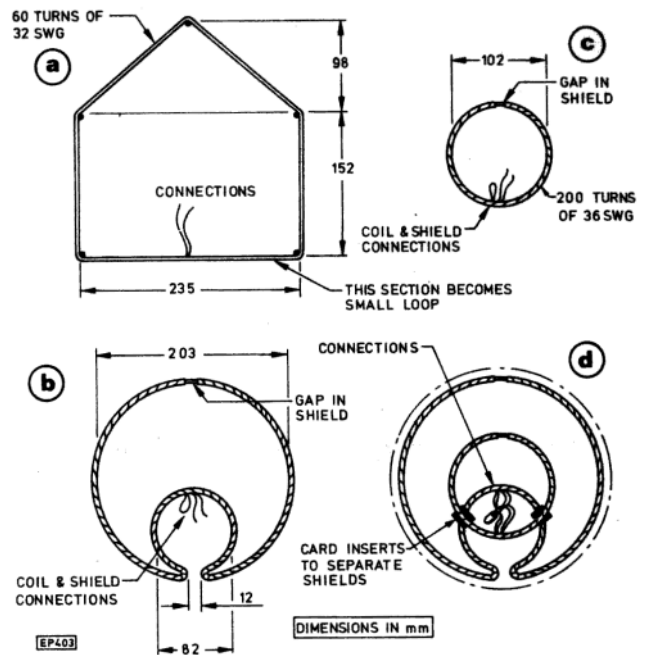
It's best to begin by winding the search coils, which will be required for testing the front-end circuit board at various stages. The Magnum uses a pinpoint coil, for reasons explained last month: these are slightly harder to make than widescans but the results obtainable are well worth the effort. The coil assembly is based on a 10in dia. 'Melaware' plate, made from a very rigid plastic, obtainable from most stores selling picnic tableware.

The inside of the plate is thoroughly roughened with glass paper to enable glassfibre resin to stick to it, and two 'L' shaped-plastic brackets are bolted to the top as in Fig. 6. These were cut from a thick, strong square-shaped clip intended for mounting square section plastic drain pipes to exterior walls, obtained from a local builders' merchants. They are bolted to the plate with 2BA countersunk screws with the heads inside, so nothing protrudes to foul the coils. A hole is drilled just behind one of the brackets to allow a 4core screened cable to pass through.

The two coils are wound on pins pushed into a suitable board. The larger transmitting coil is made with just five pins positioned as shown in Fig. 7a, on which 60 turns of 32 s.w.g. enamelled copper wire is wound. It can be tied temporarily with a few twists of wire and removed from the pins--this is fiddly but not too difficult--bent to the shape of Fig. 7b, and bound tightly with a spiral of thin bare wire such as 5 amp fusewire, leaving a loop near the lead wires for use as a connection. Remove the temporary ties as the binding proceeds. A strip of aluminium cooking foil is then wrapped over the bare wire to form a Faraday shield, and this is held in place with another tight binding of the bare wire. Note that both wire bindings and the foil must have a gap--this is most important, as if the Faraday shield were allowed to r form a complete 'turn' around the circumference of the coil it would render it useless.



**Fig. 6 (left). Search plate mounting assembly**



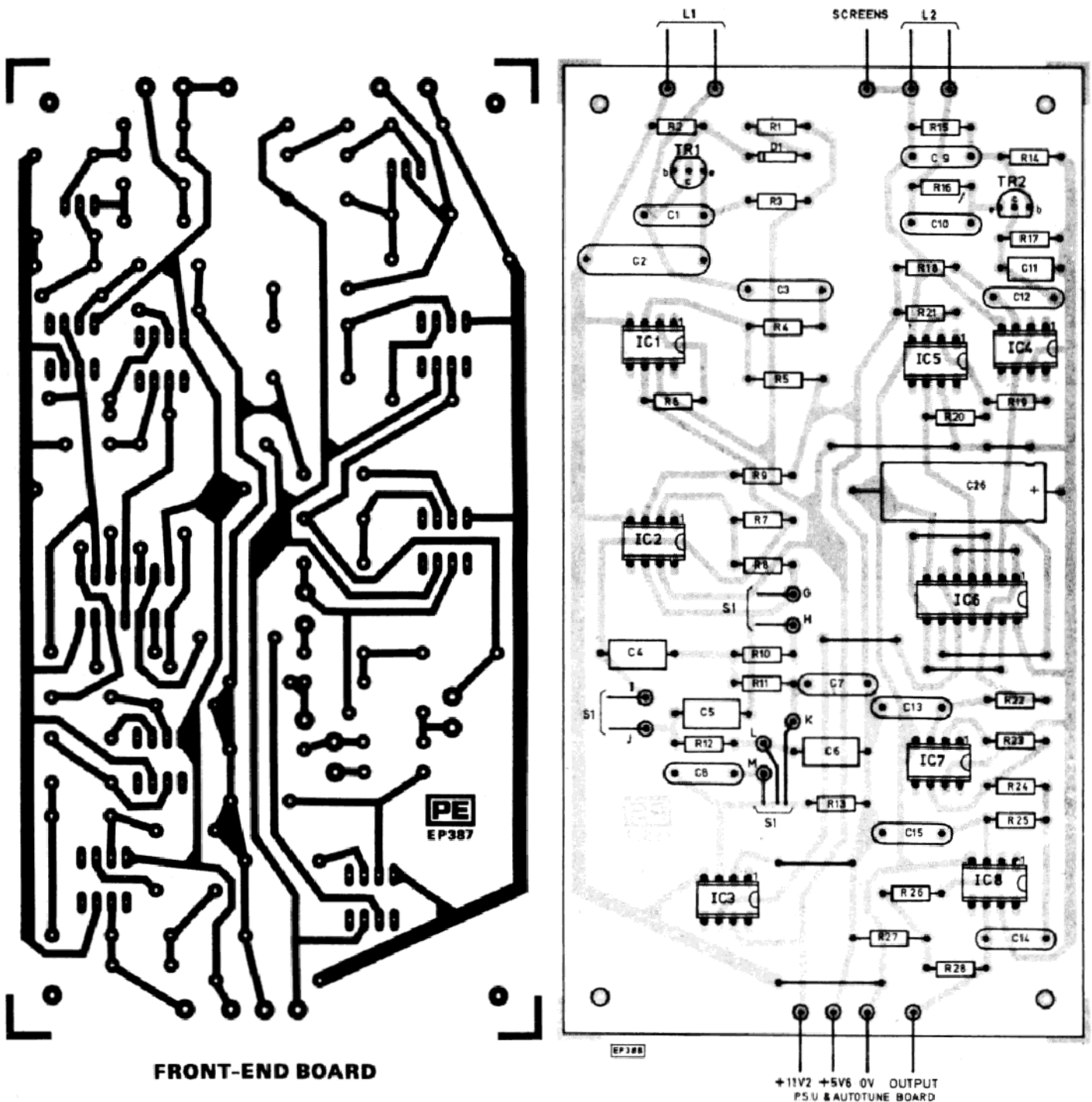
**Fig. 7 (right). (a) Winding the transmitting coil; (b) Positioning the coils; (c) Winding the Pick-up coil; (d) bent to shape**

**PICKUP COIL**

The pickup coil is made in the same manner, consisting of 200 turns of 36 s.w.g. enamelled copper wire wound around 16 pins placed in a 4in diameter circle. Faraday shielding is fitted as on the transmitting coil, again with the all-important gap.

The transmitting coil can now be fixed in place on the former using a small quantity of fibreglass resin. A Holts' 'Fibreglass Repair Kit', obtainable from motoring accessory shops, was used in making the prototype. The coil is best fixed in stages, using clothes pegs and weights to keep it in place as necessary. Apply the resin with a soft brush and have a jar of cellulose thinners handy to dunk the brush into the moment it starts to 'gel'. Push the 4-core screened lead through the hole in the plate, connect the

coil leads to two of the cores, and the Faraday shield to the screens. It can be difficult to keep the lead in place whilst the resin sets; one way of doing this is to drill two tiny holes on each side of it and secure it flat against the plate with a couple of twists of thin wire. The pickup coil is not fitted at this stage.



### FRONT-END PCB

Start building the 'front-end' circuit board by fitting all the links. Then fit R1 to 3, C1,2, and 26, D1, and TR1. Hook up the transmitting coil and apply power from the supply board. Continue using a resistor in series with the 18 volt battery in case any faults arise during tests, as described last month. The transmit oscillator should now be running, at between 15 and 16kHz. This can be checked by placing a radio tuned to a weak longwave station very close to the coil-faint whistles due to harmonics of the transmitted signal beating with station carries should be present. Faint is the word, however, as the Magnum's oscillator produces



a very clean signal. This and other parts of the circuit can be more easily checked with a 'scope of course, but if you have one you'll probably have realised this anyway.

Next fit R4 to 13, C3 to 8 and IC1. Apply power and check that IC1's d.c. output voltage (at pin 6) is equal to 5.6v. Fit IC2, apply power and check IC2's d.c. output is 5.6v. Fit IC3, hook up VR1 across points I and J, VR2 across points G and H, and fit some lengths of wire so that point M may be shorted to points K or L, and short one of these. It doesn't matter which at this stage. Apply power and check that IC3B d.c. output (pin 6) is 5.6V. The output of IC2 should actually be switching from rail to rail at the oscillator's frequency but the average value of output should be 56V. A fault will usually result in its being fully driven to one of the supply rails, so this is a useful test. Check that settings of VR1 (M shorted to L) and VR2 (M to K) makes little or no difference to IC3's output voltage.

It might be of interest to explain that in the original design, the pots were connected directly as they are in this test, and a 2-way switch was fitted to M, K and i. This provides 'Ground Reject' (VR2) and 'Discriminate' (VR1). However, on the first beach outing it was found that the 'Beach Effect' could only be rejected with the 'Discriminate' control. a predictable effect since beaches are usually conductive. This prevented the discrimination from being used to reject foil, of which large amounts are to be found on most beaches. To overcome this problem the switching was rearranged to provide a third 'Beach' position, in which VR2 is effectively switched into the discriminate circuit instead of the ground one. Thus VR2 can then be used to reject false signals from wet beaches in the same way as from ground, whilst VR1 can once again be used to check finds as intended.

Continue the construction by fitting R14 to 21, C9 to 12 and TR2. Connect the pickup coil temporarily, apply power and check that the emitter voltage of TR2 is approximately 0.6 volts above the negative rail. Fit IC4, apply power and check IC4's output voltage (pin 6) is 5.6V. Fit IC5, apply power and check that the output of IC5 is also V/2.

Fit R22 to 28 and C13 to 15. Fit IC6, observing the usual CMOS handling precautions for this chip. Place the pickup coil in approximate position over the transmitting coil, apply power and monitor the top end of R22 with a meter. The voltage present should be somewhere between 2 and 8 volts and should alter if VR1 or VR2 (whichever is selected by shorting M to K or L) is moved. Adjust the pickup coil position to obtain 5.6V at the top end of R22. Note that the Faraday shields of the coils shouldn't touch even though they are both connected to the lead screens: if they touch on both sides they can form a 'shorted turn' in the middle of the assembly. Small pieces of card should be placed between them to prevent this from happening.

Fit IC7, check it's output is the same as that at the top of R22, i.e. 56V. Fit IC8. Check 56V is still present at IC7 pin 6 -if not adjust coil position. Then check that 5.6v is also present at the output of IC8. This completes the construction of the front-end p.c.b.

## HARDWARE ASSEMBLY

The rest of the hardware can be constructed next. This is made mainly from 3/4in diameter plastic plumbing pipe and fittings, assembled as shown in Fig. 8. It's simply glued and pushed together, making a very presentable handle and stem in a surprisingly short time. Wood dowelling is inserted at strategic points of the stem to prevent it from flattening when bolts are passed through it and tightened. The search coil is fixed by a length of studding passing through the two brackets and the end of the stem, with a wingnut at each end, so that it's tilt may be easily adjusted by the user. The control box base is secured to the shaft with two bolts, and the tuning button is fitted into the end of a bicycle handlebar grip which is then pushed onto the plastic pipe, threading the wires through the pipe to emerge through a small hole close to the control box.

## CONTROL BOX ASSEMBLY

The electronics now have to be assembled into the control box. The top should be cut to accept meter, pots and switch in the layout shown in Fig. 9. Note that the top only fits the base one way round before starting this! A pattern of holes can be cut in one of the aluminium side panels to act as a speaker fret, the speaker being glued into place. A clip to hold the three PP3 batteries is fashioned from sheet aluminium and wood and bolted to the same panel, and to the ends of the bolts a piece of Veroboard is

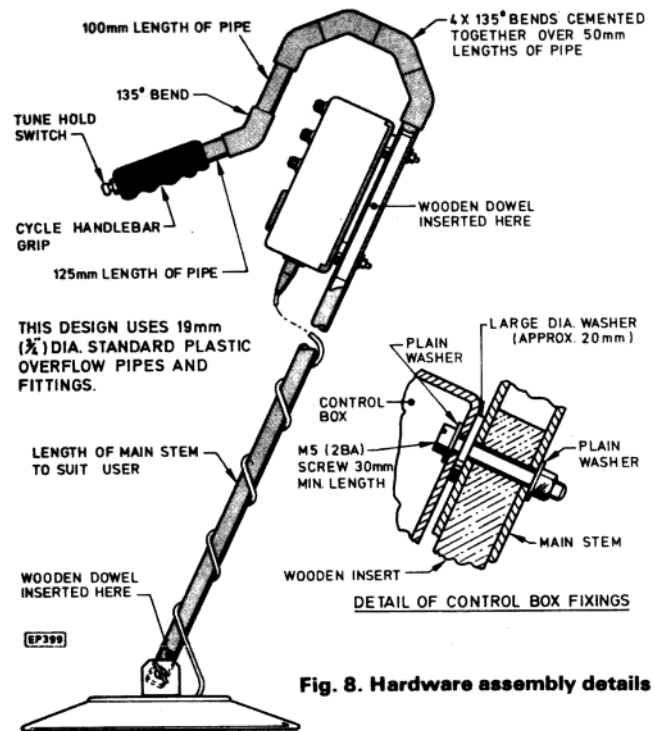
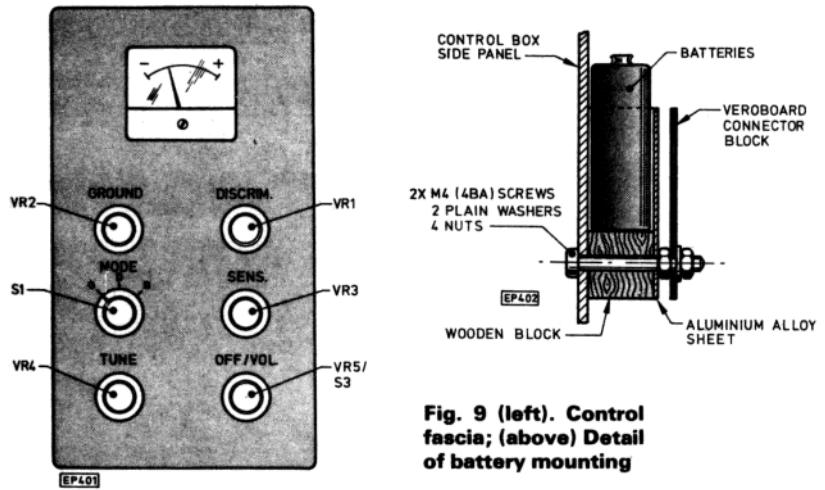


Fig. 8. Hardware assembly details

attached to act as a connecting block for the leads from the batteries and tuning button. Four 4BA bolts passing up through the base of the box act as stand-off pillars on which the two b.c. boards are mounted one above the other, the front-end board being uppermost.

The best way to make all the connections to the boards is with ribbon cable, soldering this to them before fitting them into the case and noting the point to which each coloured wire goes. A headphone socket is optional: if required it may be connected as shown in Fig. 5. 'R' will have to be selected for the phones to be used, in the prototype a value of 100 ohms was found to be suitable. A 5-pin DIN plug and socket was used for the coil lead, whilst not strictly necessary this does allow for experimenting with different coils at a later date.

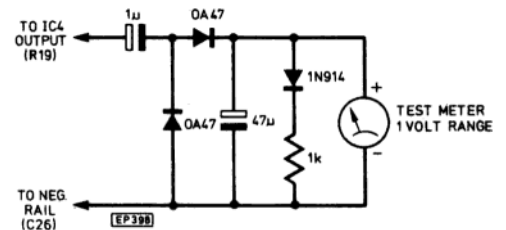
The box specified is supplied with feet which were discarded, the securing bolts being shortened a little to compensate.



**Fig. 9 (left). Control fascia; (above) Detail of battery mounting**

### SETTING UP THE SEARCH COILS

When all the components have been wired up the final tricky part has been reached; the setting up of the search coils. This must be done with metal parts such as the securing bolt and wing nuts in place, though there is no need to have the coil assembled to the stem. There should be no large metal objects close to the coil during this stage. This might also be a good time to mention that the machine can be affected by line timebase radiation from 625-line TV sets, so if you get a 'mushy' sound or a pulsed audio effect from it, check this first. Coil adjustment is actually not as critical as it is for a normal IB machine, but there is a best point and for a GEB machine it is the position where absolute minimum residual amplitude output (and maximum phase shift effect) is obtained from the pickup coil. (Conventional IBs usually work best with a slight 'offset' from absolute null.) This cannot be monitored with the phase sensitive detector in the machine itself, so the circuit of Fig. 10. should be lashed up and connected to IC4 output (top end of R19) and used with the 1 volt range of a testmeter to facilitate setting up minimum amplitude.



**Fig. 10. Circuit for setting up search coils**

Set VR1, VR2 and VR3 to mid-point. Switch to 'Discriminate' and switch on. The meter monitoring amplitude will probably indicate full scale. Carefully adjust the pickup coil position until the reading falls - this may take some patience as it's easy to push the coil right past the null position without noticing it if you're too hasty. Remember to keep those Faraday shields apart! Once you have the coils somewhere near the null, try presenting metal objects to the coil whilst watching the centre-zero meter. A non-ferrous object such as a copper coin should cause it to rise, whilst a ferrous object such as a nail should cause a fall. If the opposite happens the phase of the pickup coil must be reversed, either by turning it over or by reversing its lead connections.

Once correct coil phase has been established setting up consists of adjusting the pickup coil position for absolute minimum output from the amplitude monitoring test circuit, use resin to stick it down in stages, rechecking the adjustment at each stage. Final fine trimming can be done with only a small section of the pickup coil still moveable.

After the positioning of the coils has been completed the coils can be given a coat of resin, followed by a layer of chopped strand glassfibre mat and more resin, which produces a search head assembly that is neat, tough and totally waterproof. One word of caution; don't use more resin than you have to or the finished head may be heavier than necessary.

### FINAL ASSEMBLY AND TESTS

All the test components can now be removed and the machine finally assembled and tested. If you've never used a GEB machine before, you're in for some pleasant surprises.

On switching on, the meter should self-zero within a couple of seconds and the tuning control should then be set just below the threshold of the audio tone. The sensitivity of this machine is quite incredible; on most inland sites you'll probably need to keep the sensitivity control set to around mid-point. With the switch in 'Ground' position, a point can be found on the 'Ground' control

where moving the head to and from the ground has no effect whatever - on one side of this point there will be positive ground effect, on the other negative, so it's not difficult to find. Adjusting this control for wet beaches is the same, except that the switch should be set to 'Beach'.

Once an object has been located, the machine should be switched to 'Discriminate' and the nature of the object determined. A certain amount of ground effect will be apparent in this mode, depending upon the actual terrain being searched. Ferrous objects produce a negative response at all settings of the discriminate control, but as this control is advanced so the machine will begin to reject small pieces of silver paper, then larger pieces, thick foil, and finally pull rings. It should be noted that in the pull-ring reject setting, however, it will also reject silver coins up to about 10p size. All discriminators suffer from this problem; but the ability to reject scrap iron and foil without difficulty is an absolute boon. Some practice with assorted objects - coins, nails and scraps of foil etc., is recommended before setting forth with this machine.

The tuning 'Hold' button will be found necessary for discriminating and for pinpointing the exact position of finds.

So, Good Hunting! Don't forget you need a licence for your detector; application forms for this can be obtained from: The Home Office, Radio Regulatory Dept., Waterloo Bridge House, London SE1.

