



US006002708A

United States Patent [19]

[11] Patent Number: **6,002,708**

Fleming et al.

[45] Date of Patent: **Dec. 14, 1999**

[54] SPREAD SPECTRUM LOCALIZERS

5,742,635 4/1998 Sanderford, Jr. 375/200

[75] Inventors: **Robert Alan Fleming; Cherie Elaine Kushner**, both of Nicasio, Calif.

OTHER PUBLICATIONS

“Spread Spectrum Systms,” R. C. Dixon, John Wiley and Sons, Second Edition, 1984, chapter 2.

[73] Assignee: **Aether Wire & Location, Inc.**, Nicasio, Calif.

“Frequency-Sharing and Spread-Spectrum Transmission with Large Relative Bandwidth,” H. F. Harmuth, IEEE Transactions on Electromagnetic Compatibility, vol. EMC-20, No. 1 Feb. 1978, pp. 232-239.

[21] Appl. No.: **08/863,090**

(List continued on next page.)

[22] Filed: **May 23, 1997**

Related U.S. Application Data

Primary Examiner—Amanda T. Le
Attorney, Agent, or Firm—Trial & Technology Law Group

[62] Division of application No. 08/279,329, Jul. 22, 1994, Pat. No. 5,748,891.

[57] ABSTRACT

[51] Int. Cl.⁶ **H04B 15/00**

A network of localizers determines relative locations in three-dimensional space to within 1 cm by cooperatively measuring propagation times of pseudorandom sequences of electromagnetic impulses. Ranging transmissions may include encoded digital information to increase accuracy. The propagation time is determined from a correlator circuit which provides an analog pseudo-autocorrelation function sampled at discrete time bins. The correlator has a number of integrators, each integrator providing a signal proportional to the time integral of the product of the expected pulse sequence delayed by one of the discrete time bins, and the non-delayed received antenna signal. With the impulses organized as doublets the sampled correlator output can vary considerably in shape depending on where the autocorrelation function peak falls in relation to the nearest bin. Using pattern recognition the time of arrival of the received signal can be determined to within a time much smaller than the separation between bins. Because operation of standard CMOS circuitry generates noise over a large frequency range, only low-noise circuitry operates during transmission and reception. To provide the time accuracy necessary for distancing, a high-frequency clock operates during inter-localizer communications. The high-frequency clock uses a phase-lock loop circuit to increase the clock rate and a programmable delay to provide still finer time graduations. A stage in the low-frequency clock uses low-noise circuitry during transmissions and receptions, and standard circuitry at other times.

[52] U.S. Cl. **375/200; 375/206; 375/210; 375/343; 327/336**

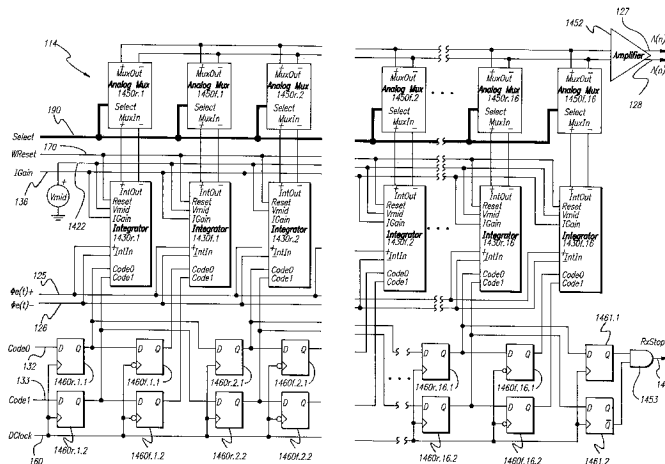
[58] Field of Search 375/200, 206, 375/208-210, 343; 364/605, 733, 829, 830; 327/336, 337; 342/378, 189

[56] References Cited

U.S. PATENT DOCUMENTS

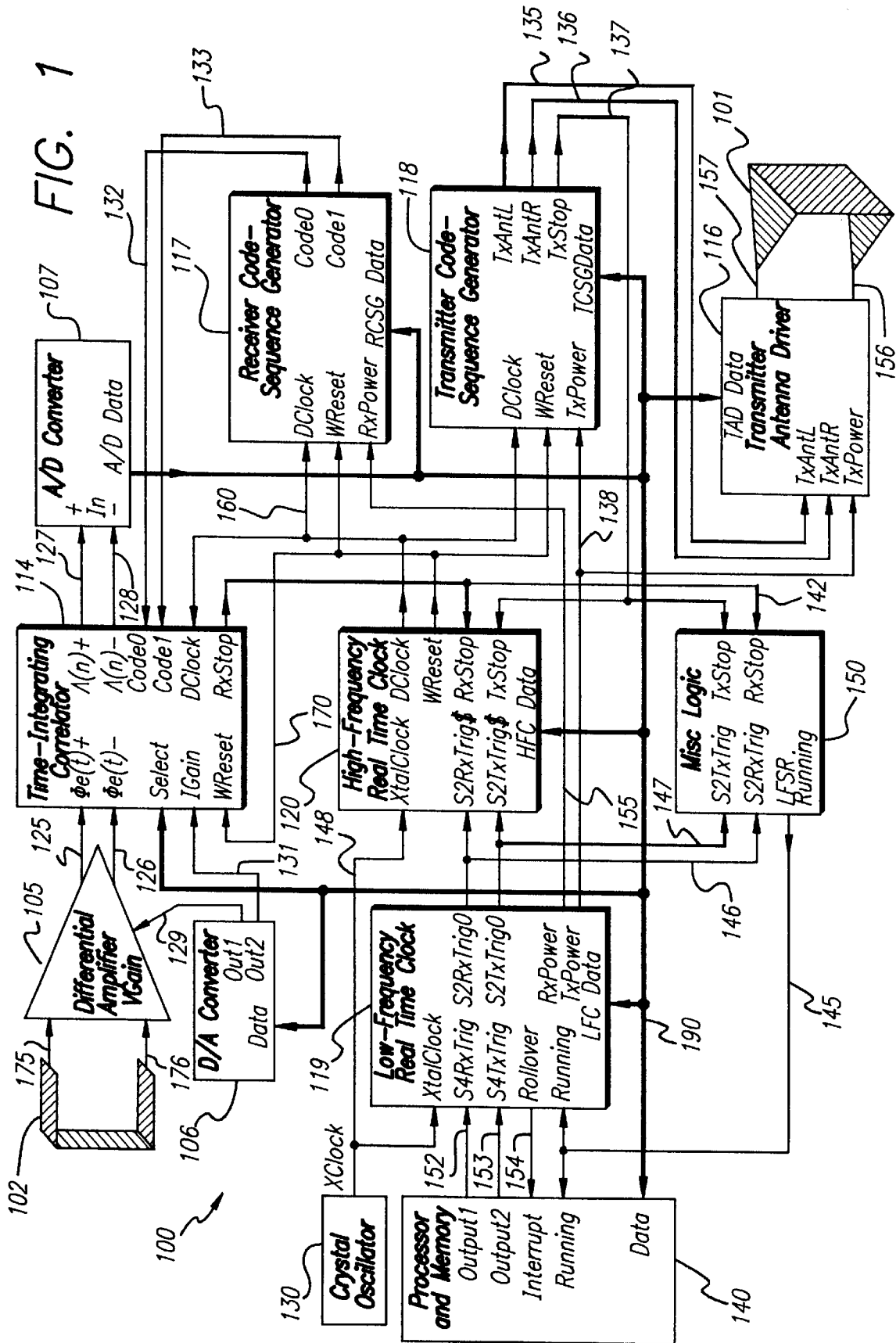
4,357,609	11/1982	Spencer	343/12
4,374,335	2/1983	Fukahori et al.	327/336
4,506,267	3/1985	Harmuth	.
4,513,285	4/1985	Pike et al.	343/5
4,559,606	12/1985	Jezo et al.	364/728
4,707,839	11/1987	Andren e al.	375/200
5,003,271	3/1991	Swanson	330/298
5,072,141	12/1991	Eisenbart et al.	307/571
5,134,408	7/1992	Harmuth	342/21
5,179,573	1/1993	Paradise	375/1
5,184,135	2/1993	Paradise	342/149
5,216,691	6/1993	Kaufmann	375/1
5,220,332	6/1993	Beckner et al.	342/125
5,274,271	12/1993	McEwan	.
5,345,471	9/1994	McEwan	.
5,361,070	11/1994	McEwan	.
5,365,516	11/1994	Jandrell	370/18
5,408,235	4/1995	Doyle et al.	341/143
5,432,827	7/1997	Mader	375/576
5,488,662	1/1996	Fox et al.	380/34
5,523,758	6/1996	Harmuth	342/22

30 Claims, 35 Drawing Sheets



OTHER PUBLICATIONS

- "An Overview of Impulse Radar Phenomenon," D. L. Black, IEEE AES Systems Magazine, Dec. 1992, pp. 6-11.
- "Shift Register Sequences," S. W. Golomb, Aegean Park Press, Laguna Hills, CA, 1982, pp. 2-6 and 24-30.
- "New approach to microwave reflectometry: correlation: reflectometry via stochastic noise signals," V. S. Korostel'ov, et al., IAEA Technical Meeting on Microwave Reflectometry for Fusion Research, Abingdon, England, Mar. 1992.
- "Noise-Modulated Distance Measuring Systems," B. M. Horton, Proceedings of the I.R.E., May, 1959, pp. 821-828.
- "CCD Time-Integrating Correlator," B. E. Burke and D. L. Smythe, Jr., IEEE Journal of Solid-State Circuits, vol. SC-18, No. 6, Dec. 1983, pp. 736-744.
- "Programmable, Four Channel, 128-Sample, 40-Ms/s Analog-Ternary Correlator," S. C. Munroe, et al., IEEE Journal of Solid-State Circuits, vol. 25, No. 2, Apr. 1990, pp. 425-430.
- "CMOS Active Filter Design at Very High Frequencies," Y.-T. Wang and A. A. Abidi, IEEE Journal of Solid-State Circuits, vol. 25, No. 6, Dec. 1990, pp. 1562-1574.
- "A Ratio-Independent Algorithmic Analog-to-Digital Conversion Technique," P. W. Li, et al., IEEE Journal of Solid-State Circuits, vol. SC-19, No. 6, Dec. 1984, pp. 828-836.
- "A BiCMOS Time Interval Digitizer For High-Energy Physics Instrumentation," M. J. Loinaz and B. A. Wooley, IEEE 1993 Custom Integrated Circuits Conference, pp. 28.6.1-28.6.4.
- "Charge-Pump Phase-Lock Loops," F. M. Gardener, IEEE Transactions on Communications, vol. Com.-28, No. 11, Nov. 1980, pp. 1849-1858.
- "Radiation of Nonsinusoidal Electromagnetic Waves," H. F. Harmuth, Academic Press, San Diego, CA, 1990, pp. 36-47.
- "DC Motors, Speed Controls, Servo Systems," Electro-Craft Corporation, Hopkins, MN, Third Edition, 1975, pp. 4-31 and 4.32.
- "Guide to GPS Positioning," D. Wells, Canadian GPS Associates, Second Printing, 1987, pp. 4.10 to 4.15 and 6.0 to 6.6.
- "The GPS message on the hardware platform," P. Mattos, Electronics World+Wireless World, Feb. 1993, pp. 146-151.
- "Global Positioning System," Institute of Navigation, Washington, D.C., vol. 1, 1980, pp. 81-86.
- Loinaz, et al., A BiCMOS Time Interval Digitizer for High-Energy Physics Instrumentation, IEEE 1993, pp. 28.6-28.6.2.
- Harmuth, Radiation of Nonsinusoidal Electromagnetic Waves, Academic Press, Inc., San Diego CA 1990, pp. 36-47.
- Wells, et al., Guide to GPS Positioning, Canadian GPS Associates, Second Printing, 1987, pp. 4.10-4.15 and 6.0-6.6.
- Burke, et al., A CCD Time-Integrating Correlator, IEEE Journal of Solid-State Circuits, vol. SC-18, No. 6, Dec. 1983, pp. 736-744.
- Glazer, GPS Receiver Operation, Institute of navigation, Washington, D.C. vol. 1, 1980, pp. 81-86.
- Horton, Noise-Modulated Distance Measuring Systems, Proceedings of the I.R.E., May 1959, pp. 821-828.



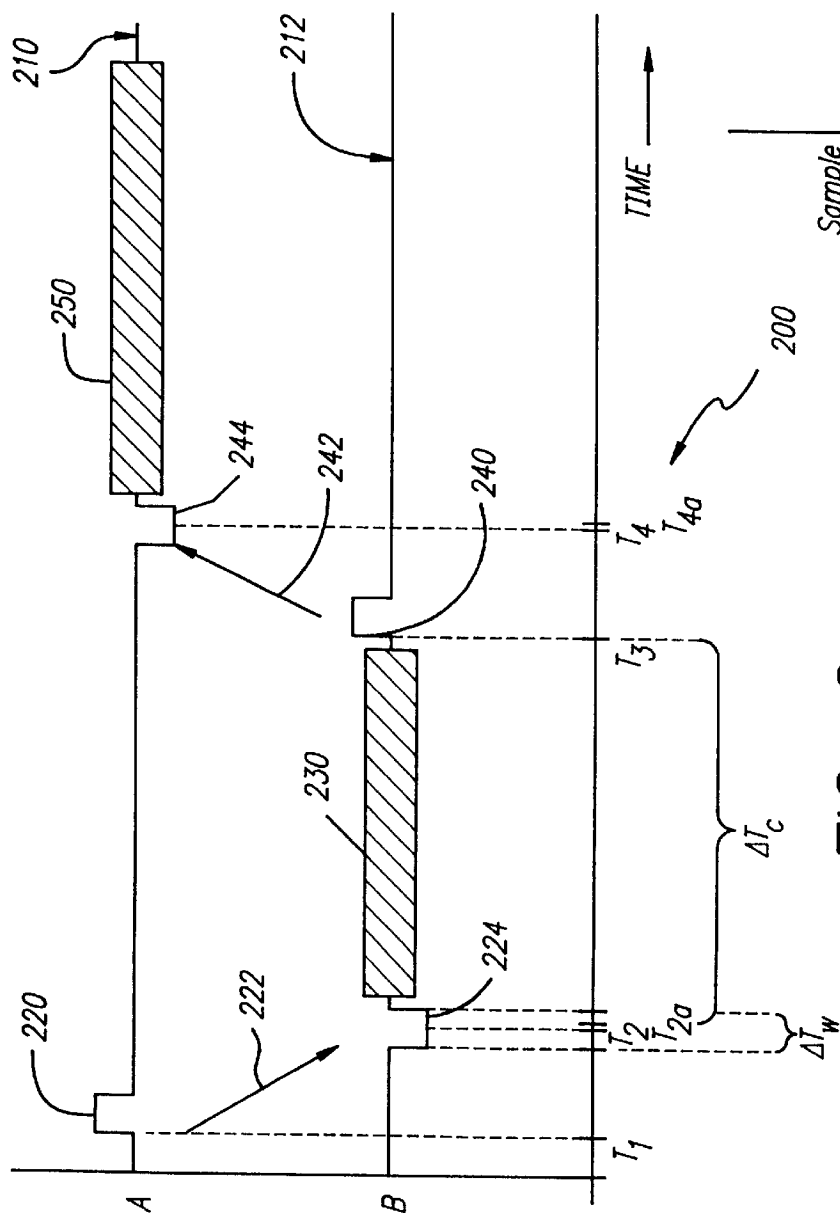


FIG. 2

FIG. 20

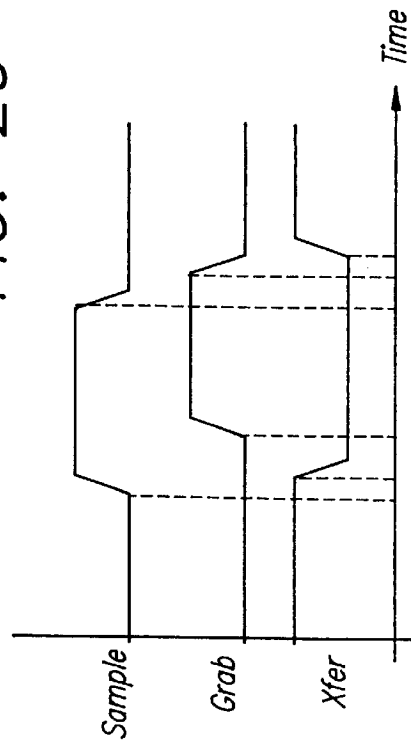


FIG. 3

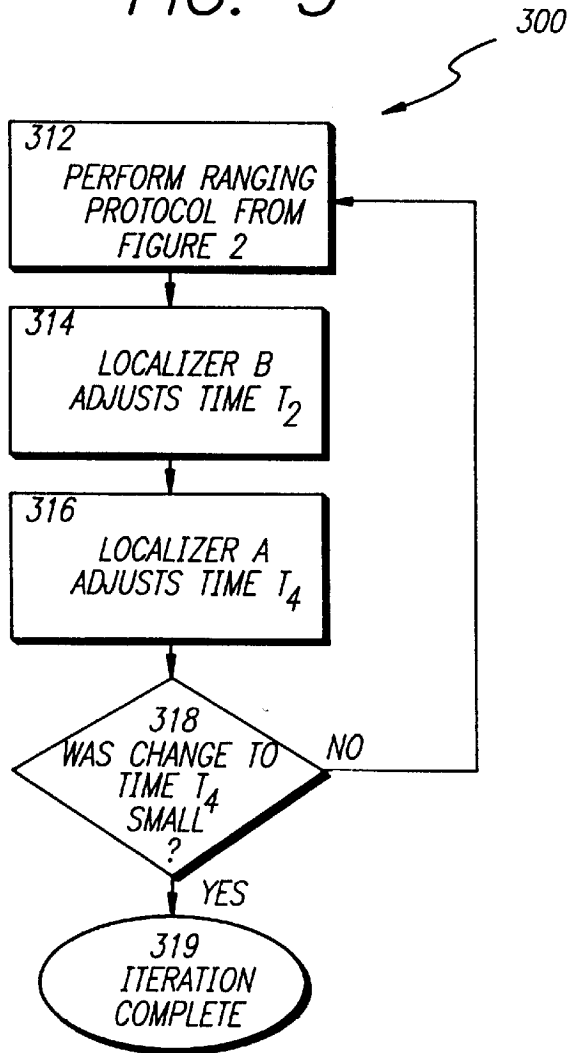


FIG. 5

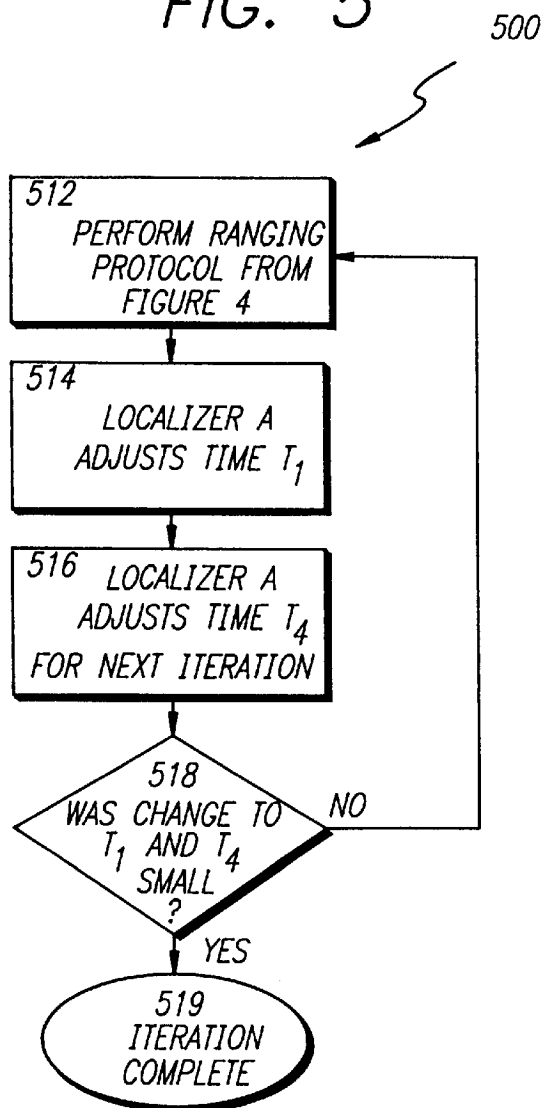


FIG. 4

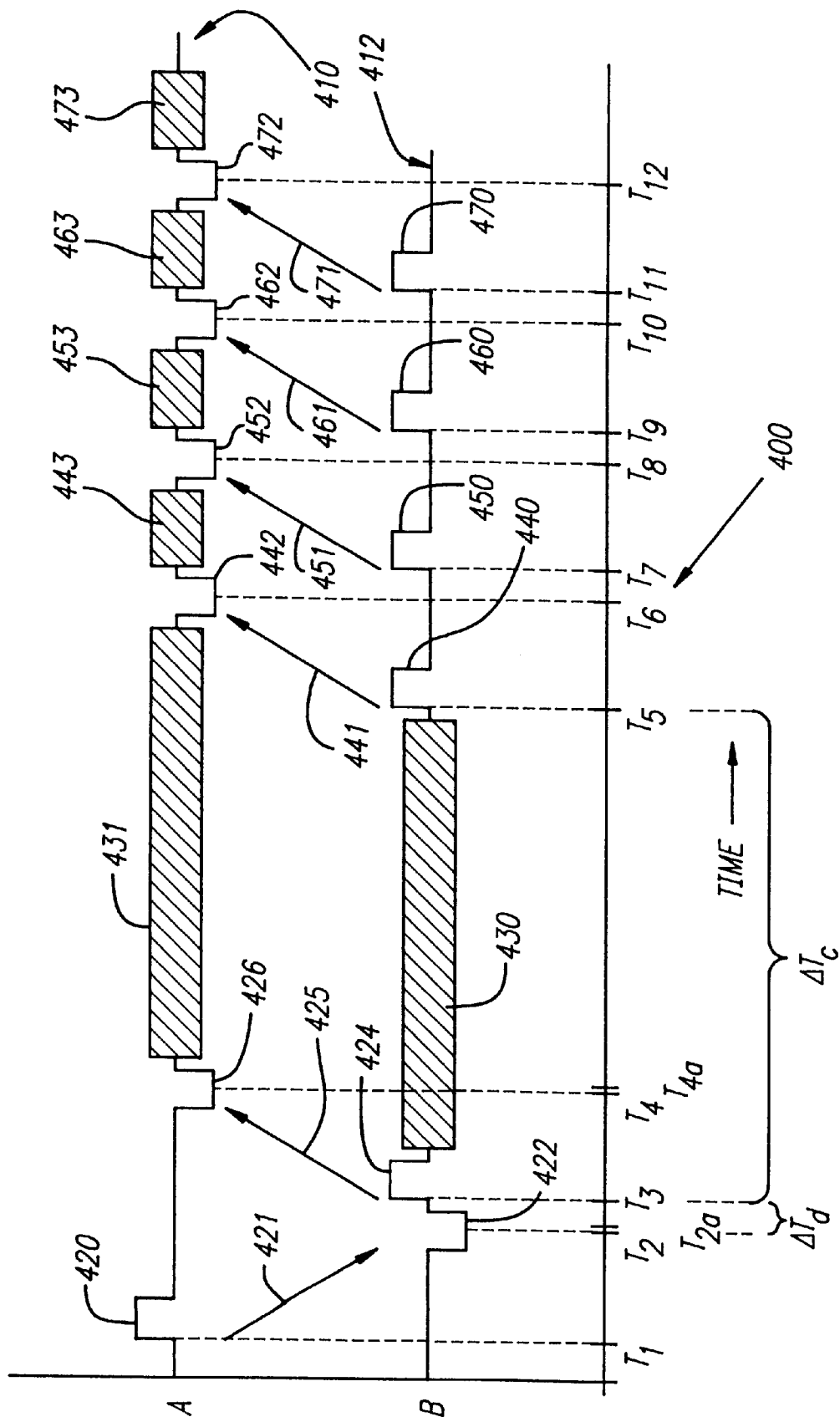
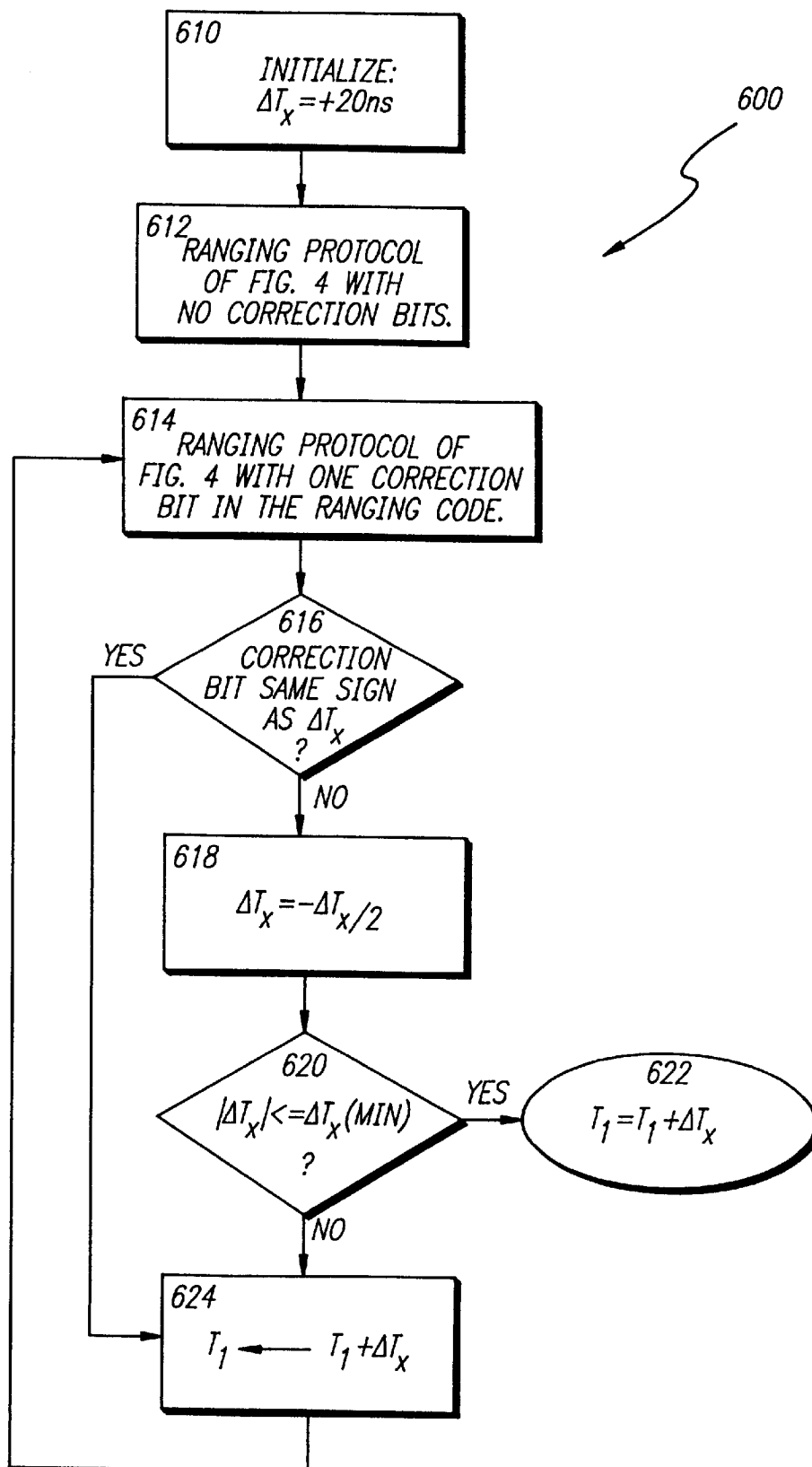


FIG. 6



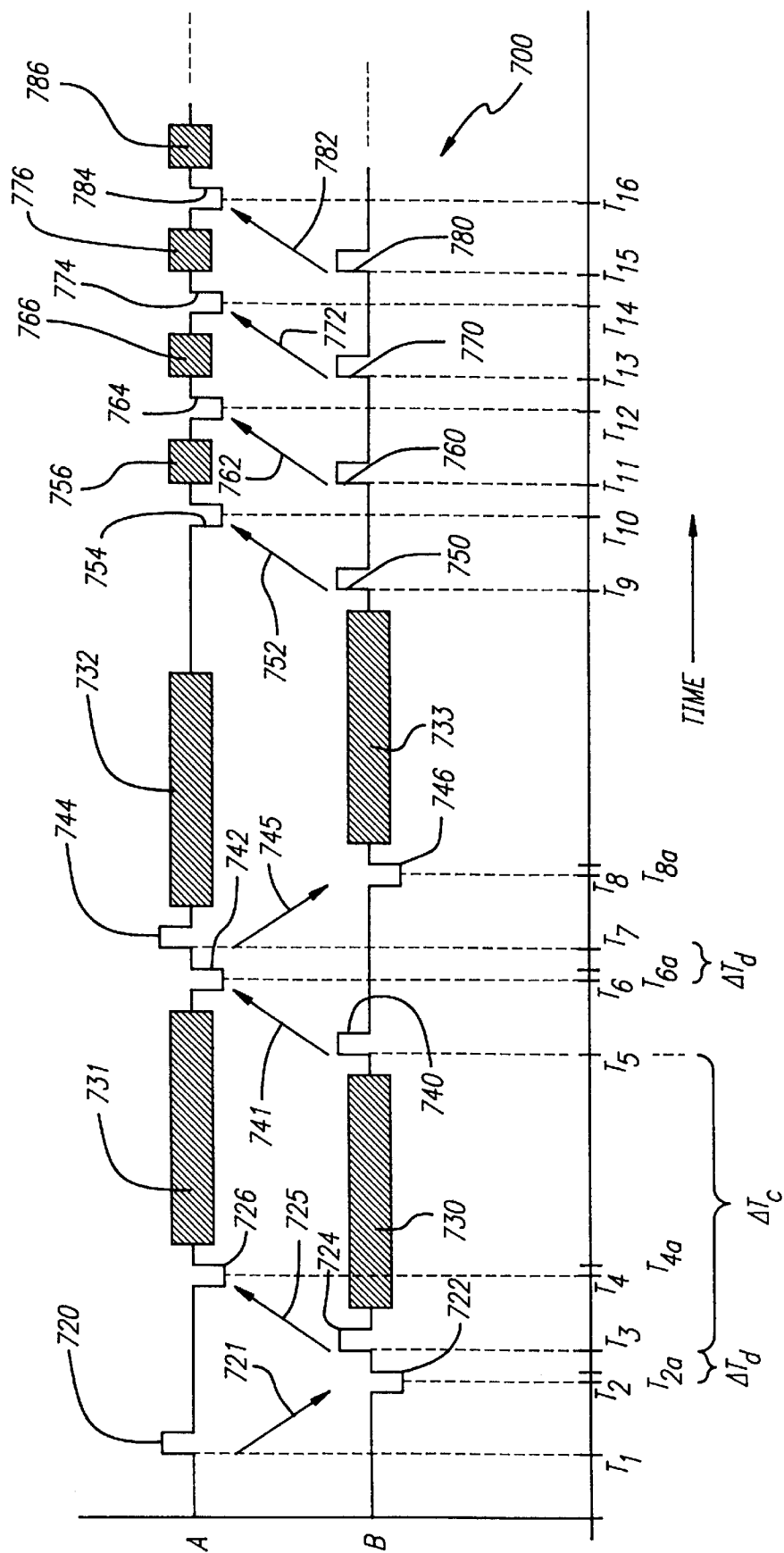


FIG. 7a

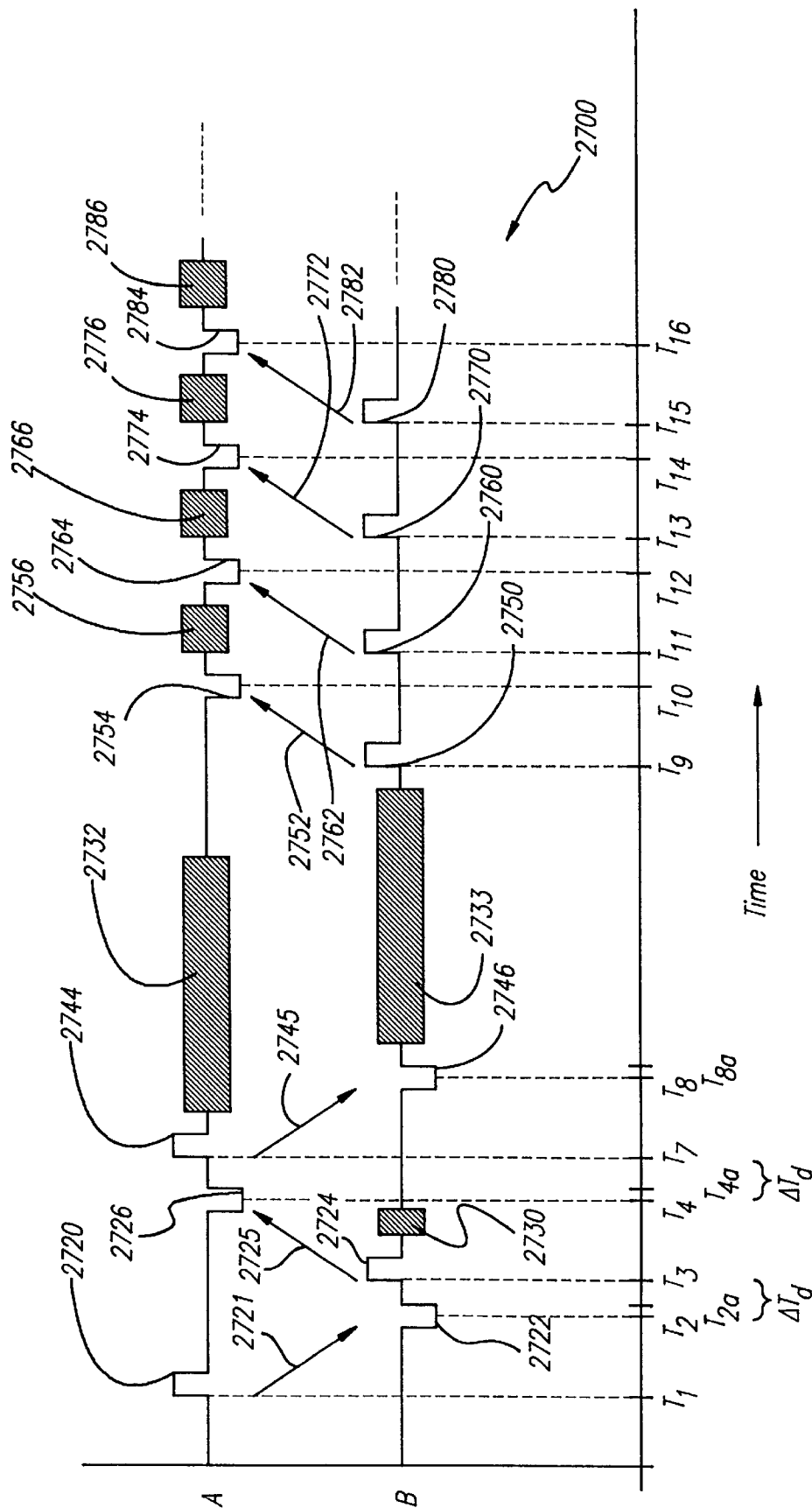


FIG. 7b

FIG. 8

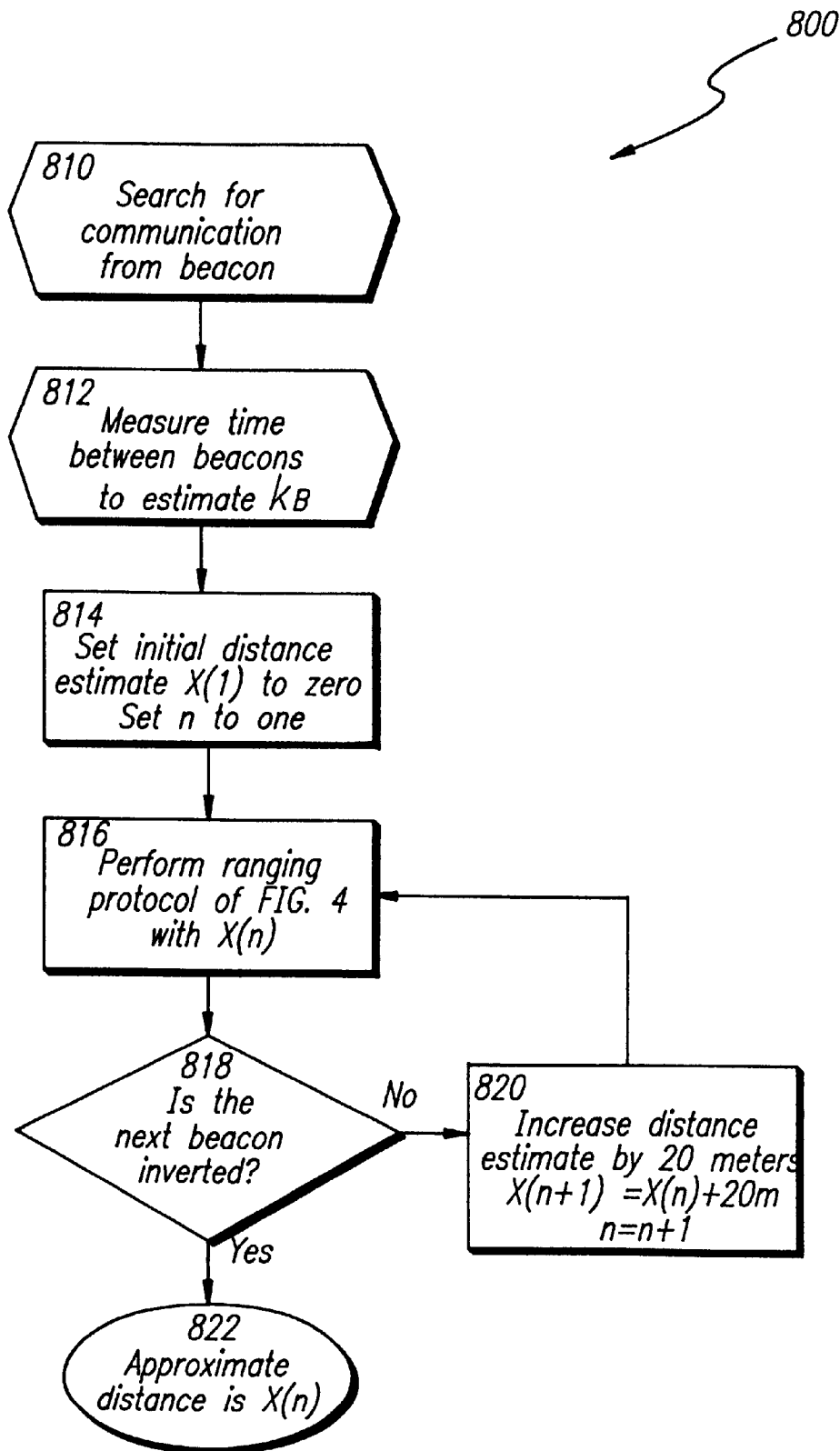


FIG. 9

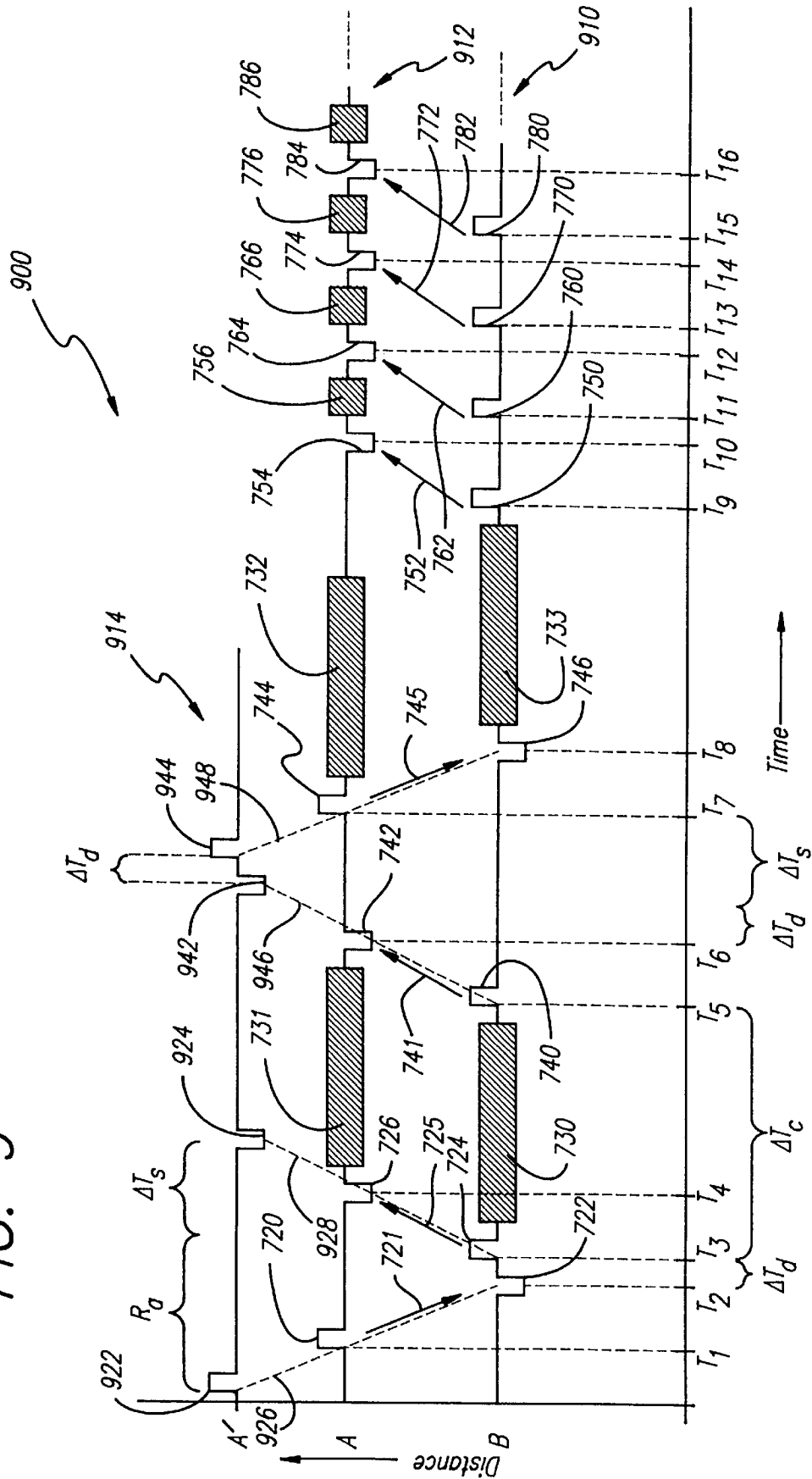


FIG. 10a.1

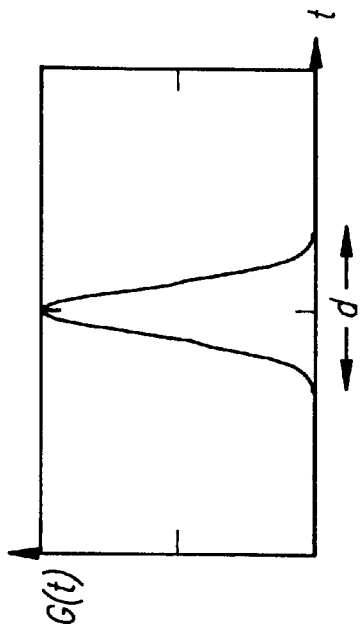


FIG. 10a.2

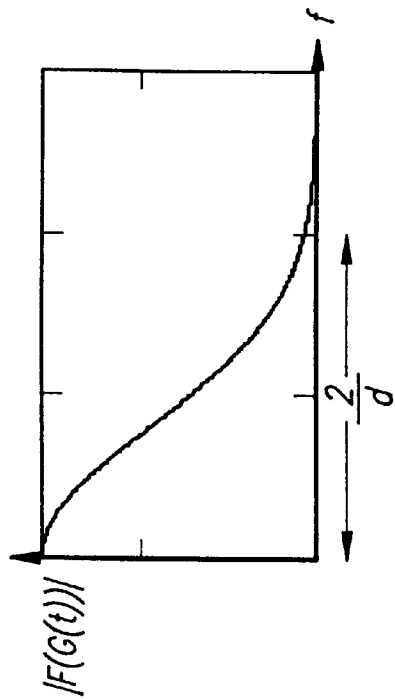


FIG. 10b.1

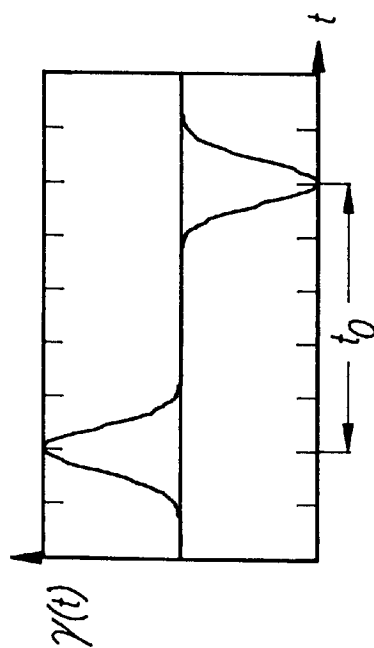


FIG. 10b.2

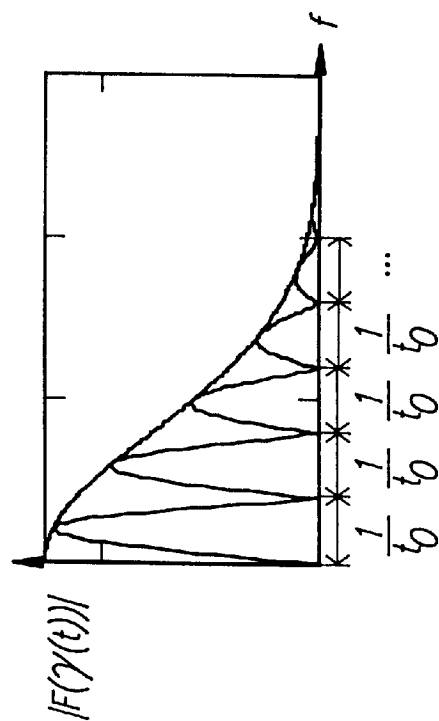


FIG. 10c.2

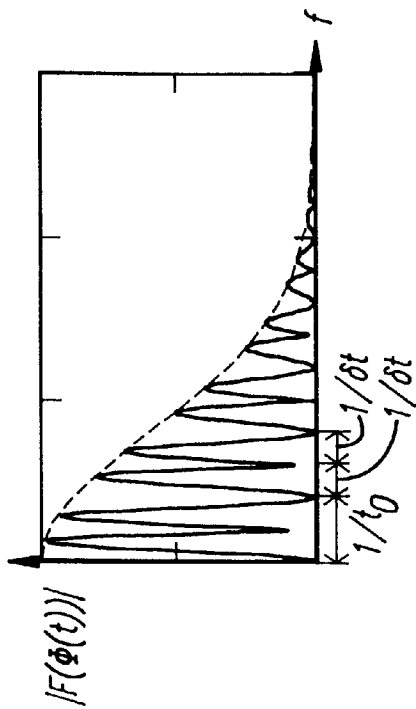


FIG. 10c.1

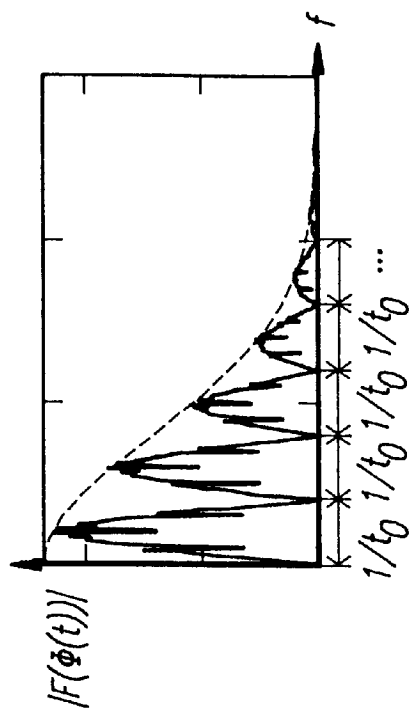
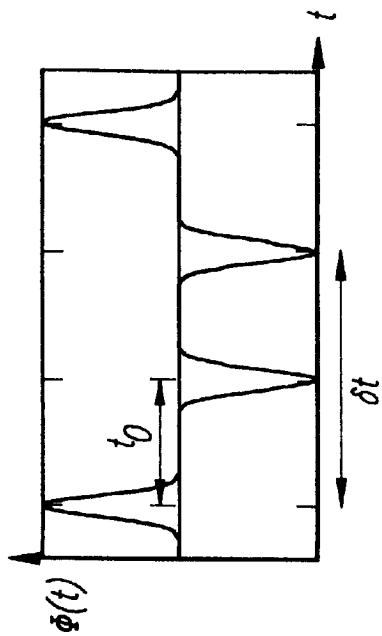


FIG. 10d.2

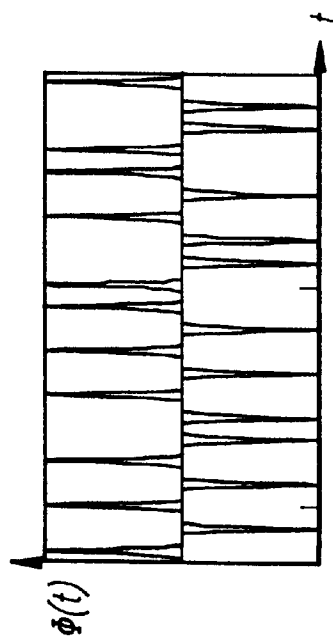


FIG. 10d.1

FIG. 10e.2

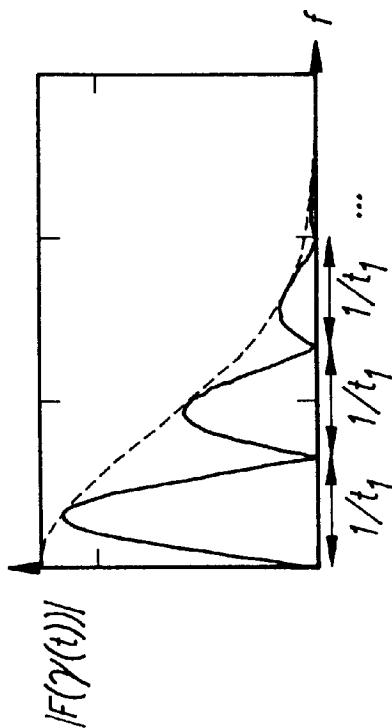


FIG. 10f.2

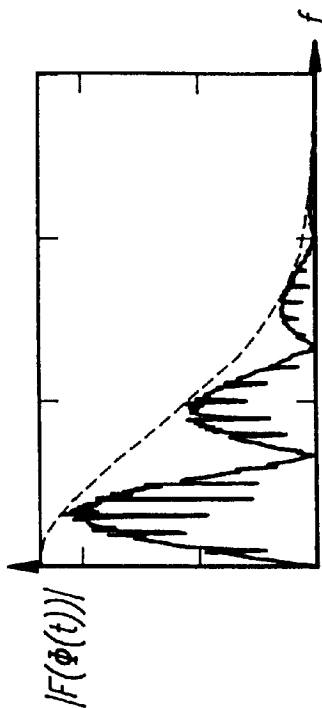


FIG. 10e.1

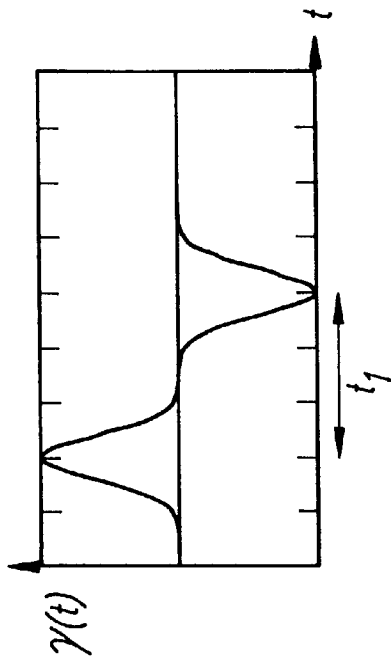
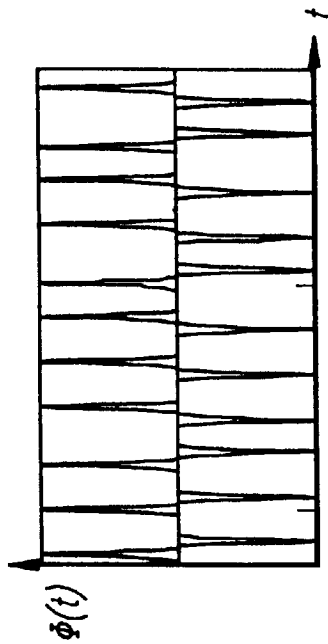
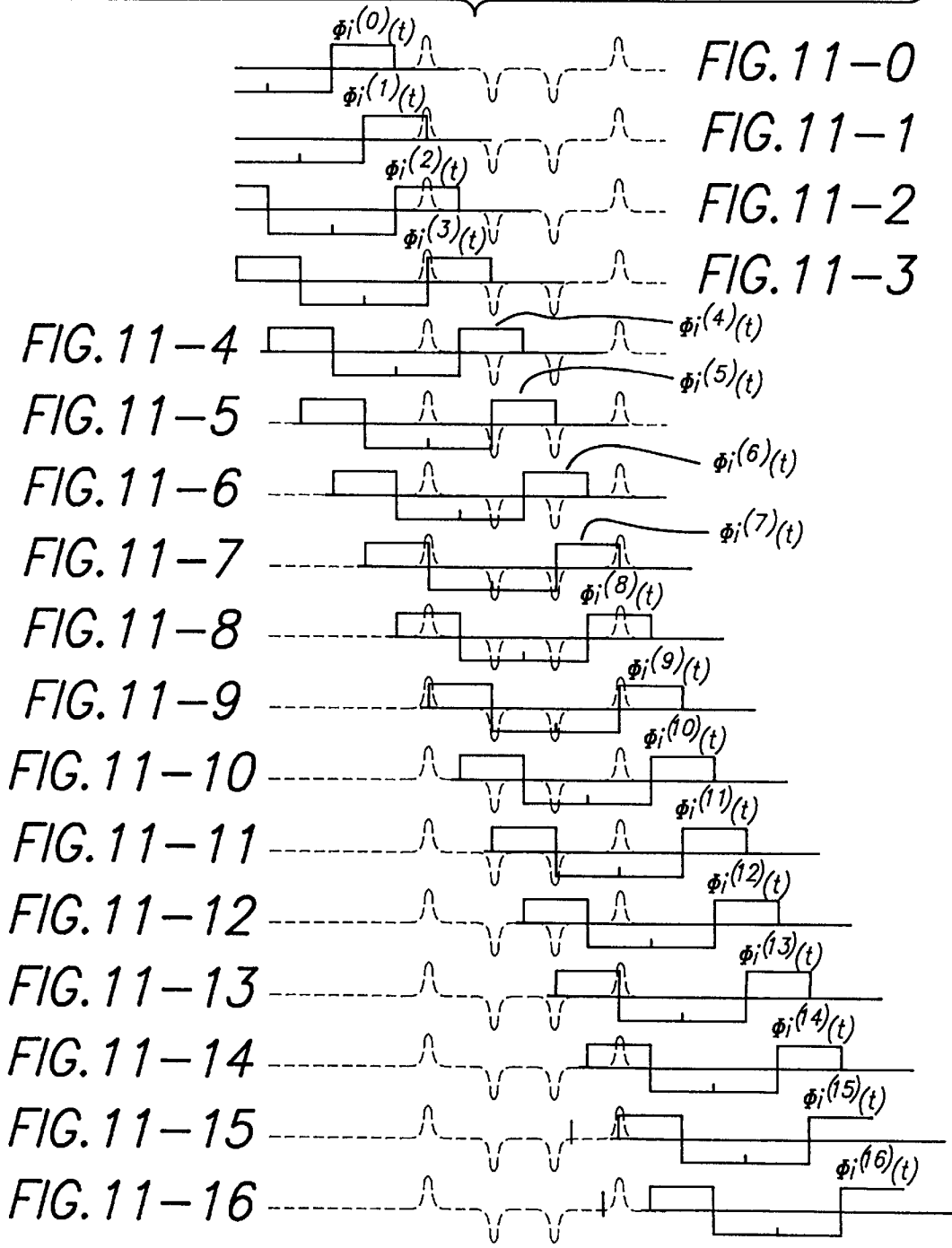
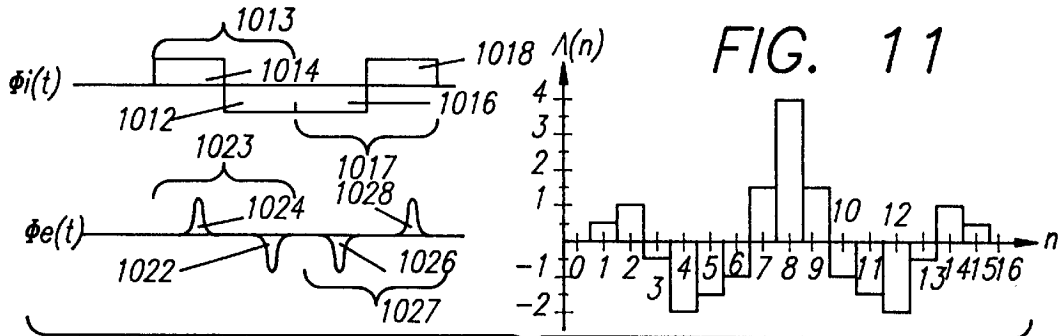
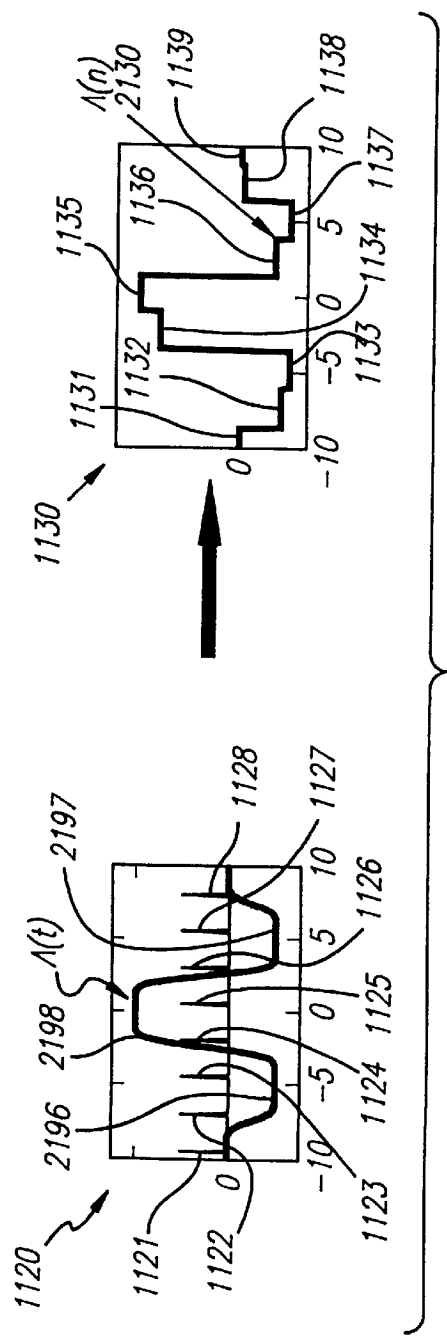
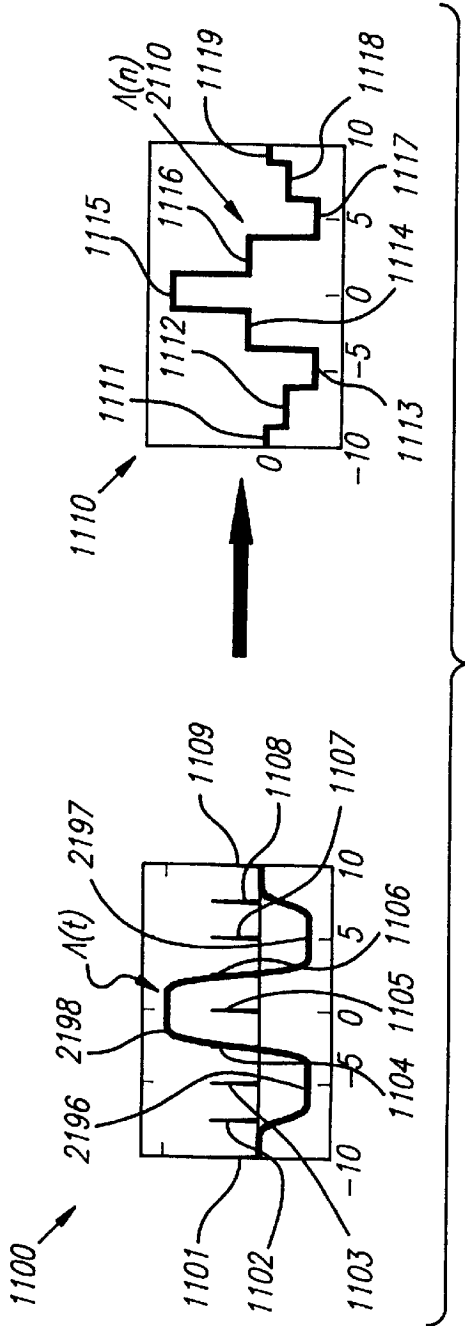


FIG. 10f.1







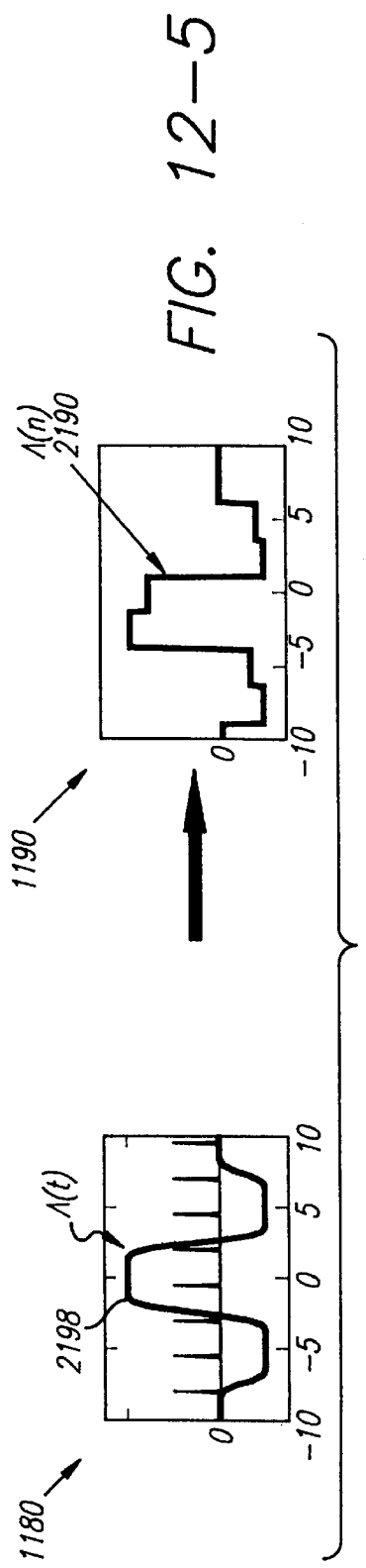
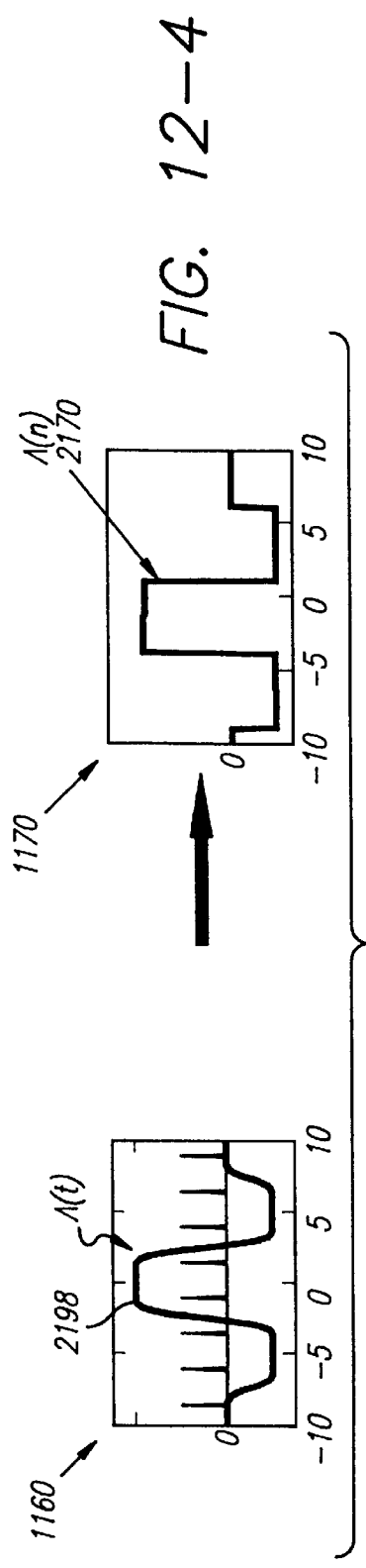
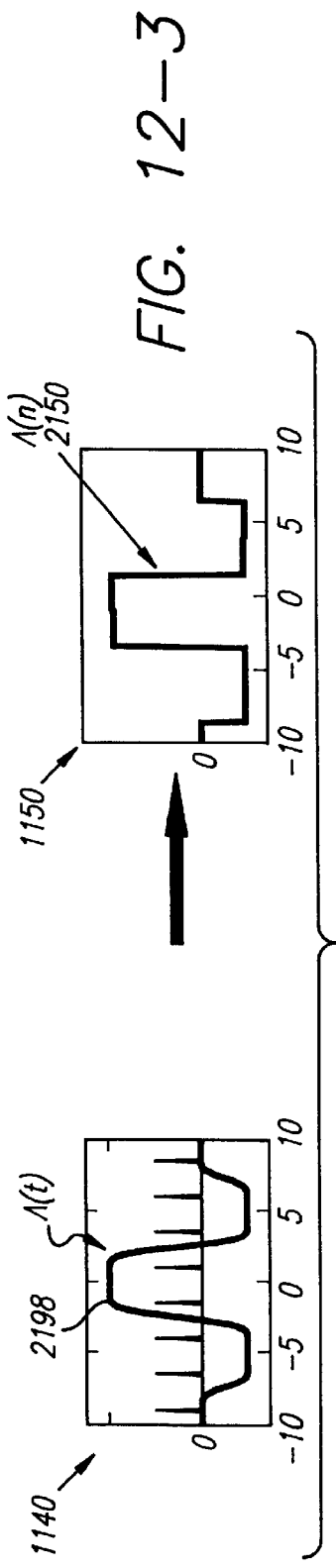


FIG. 13-1

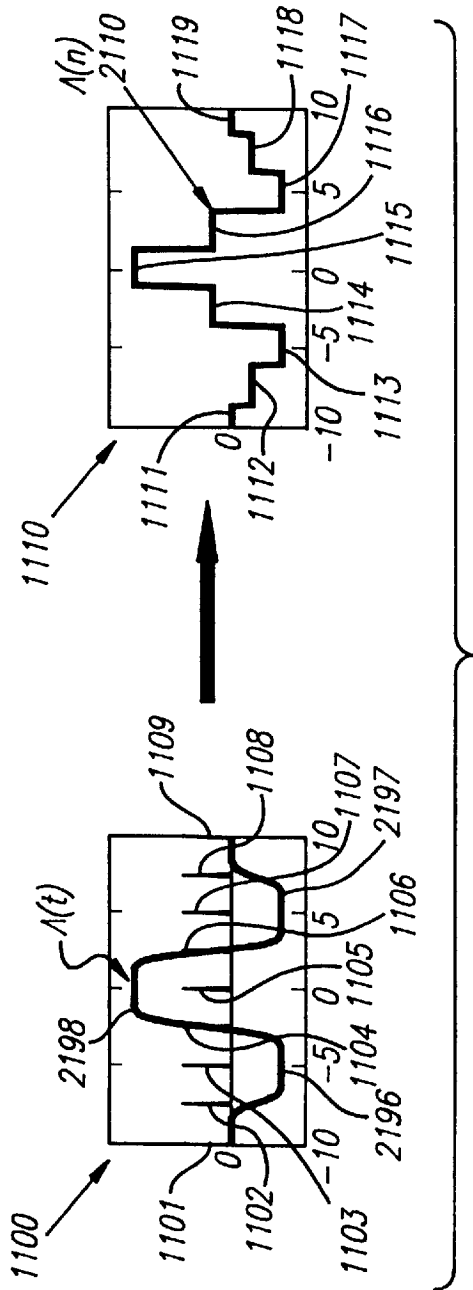


FIG. 13-2

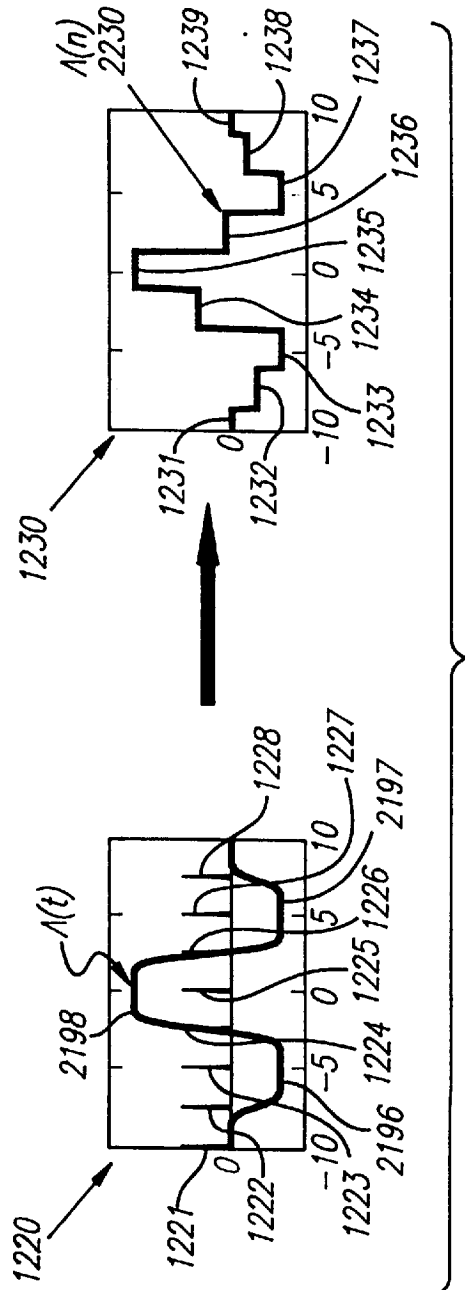


FIG. 13-3

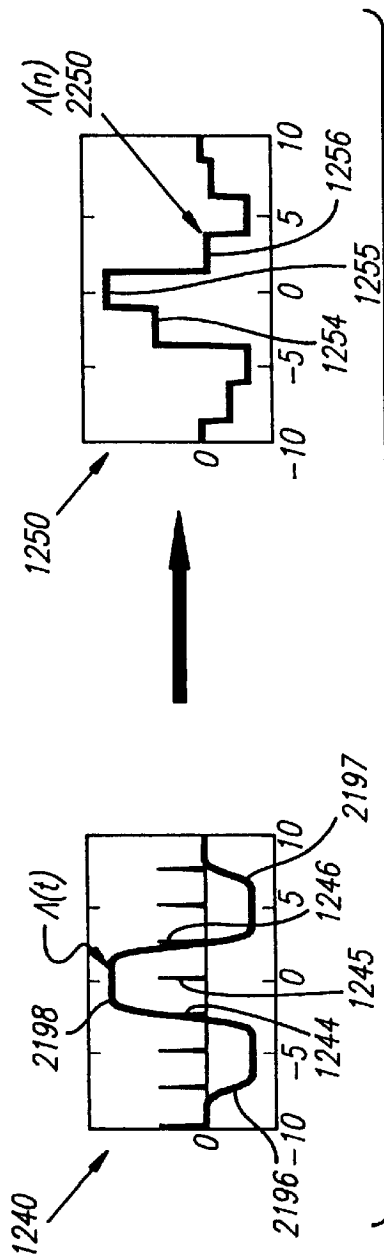


FIG. 13-4

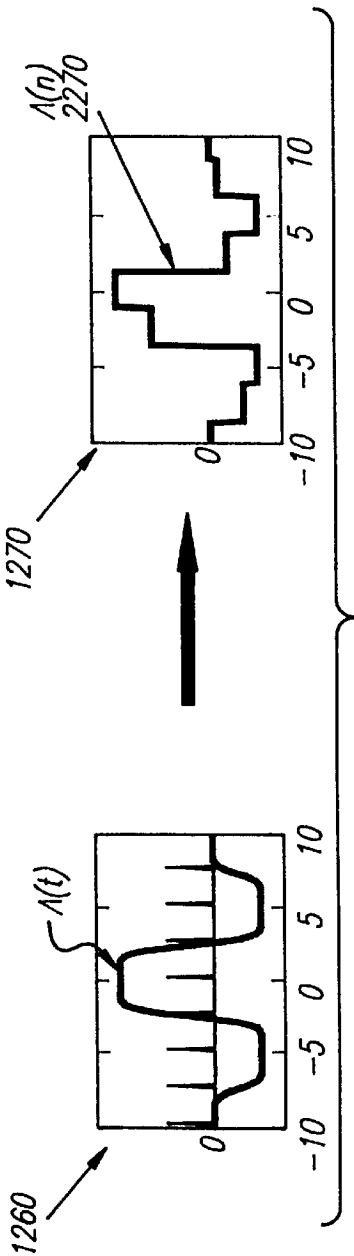


FIG. 13-5

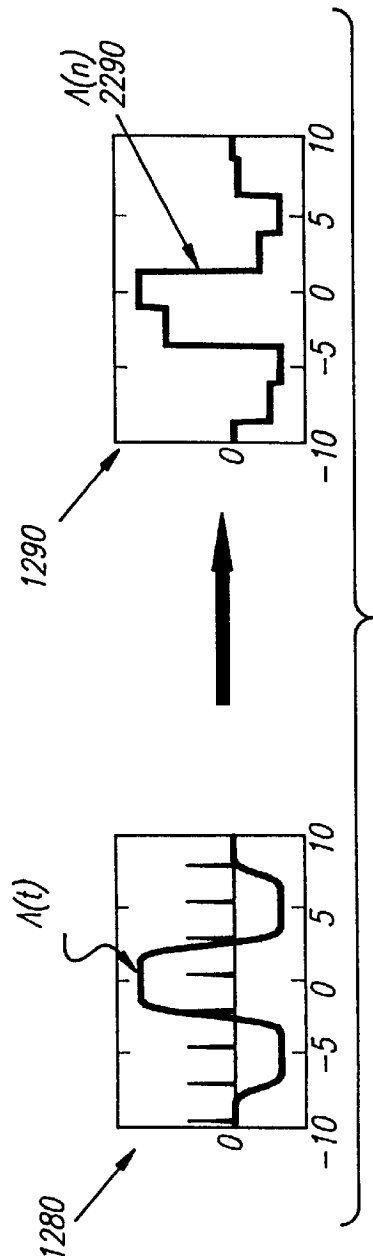


FIG. 14a

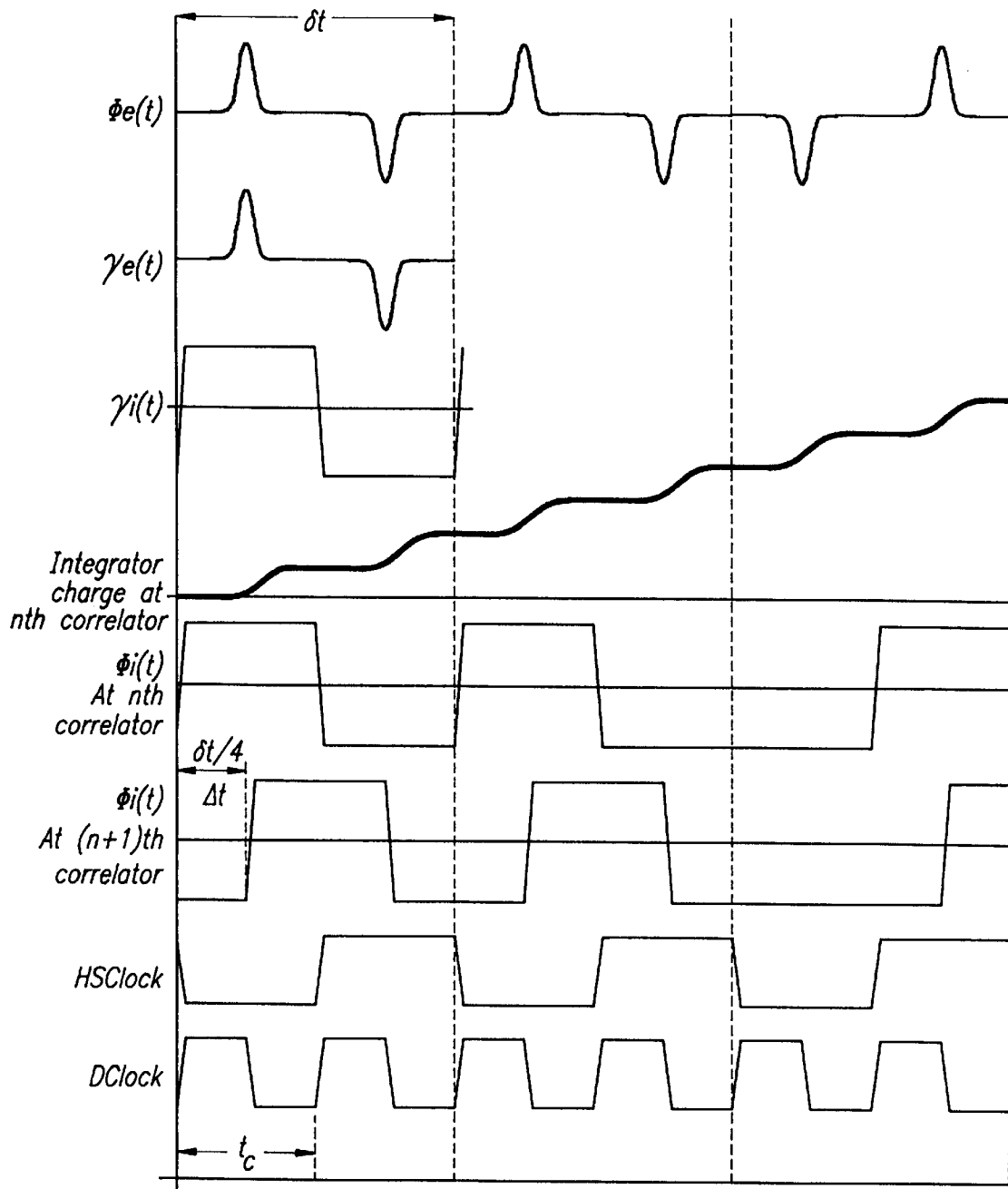


FIG. 14b

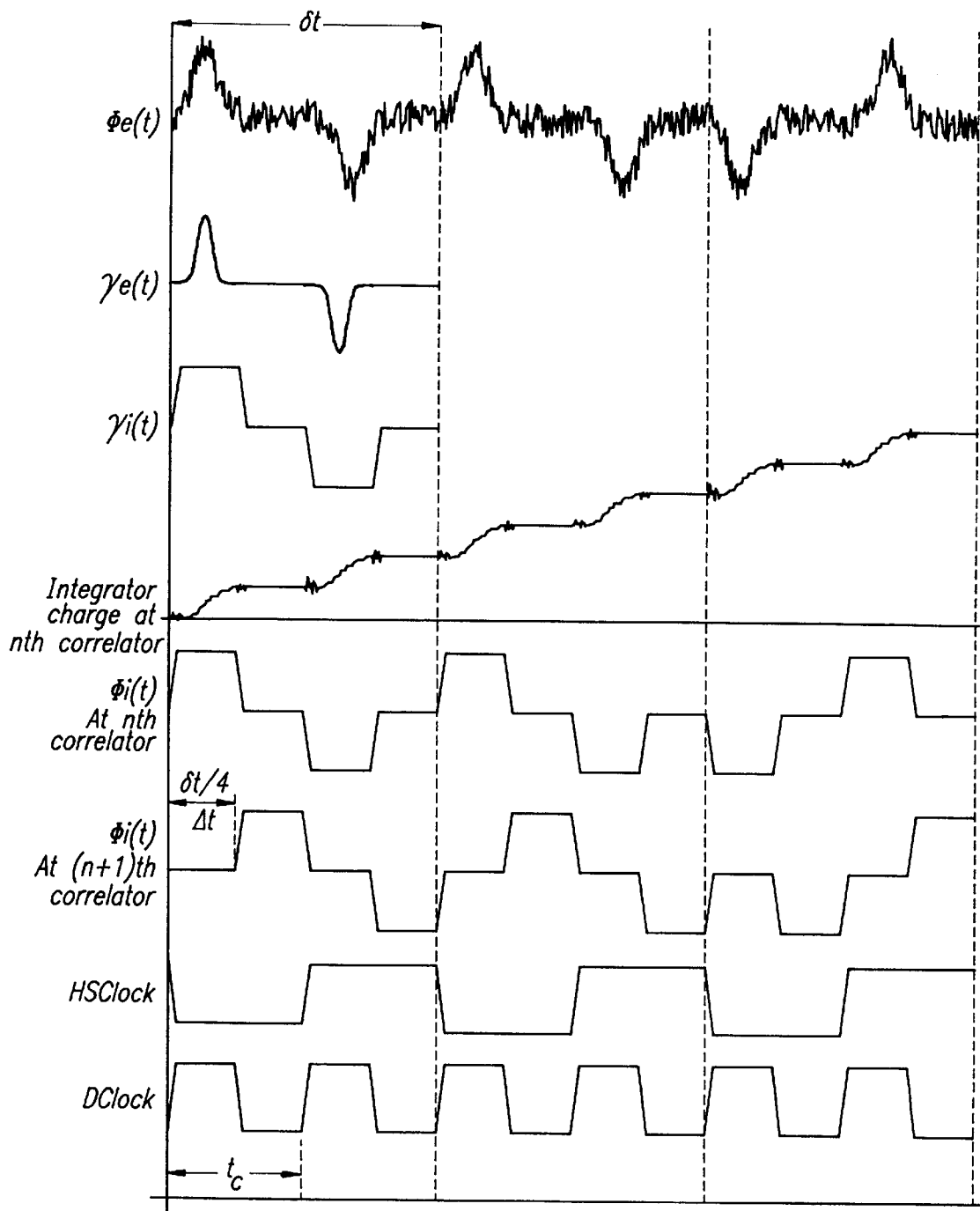


FIG. 14c

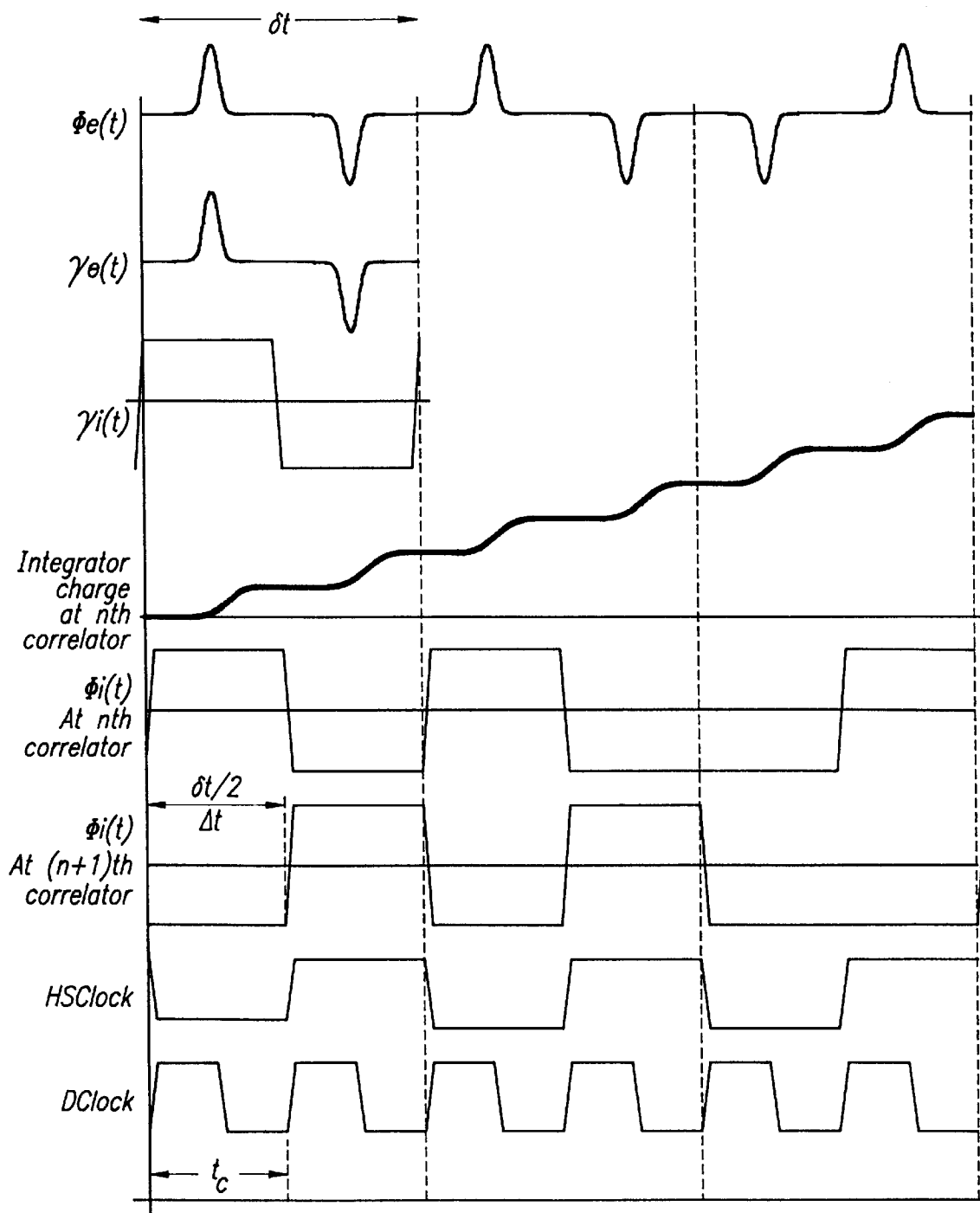


FIG. 15

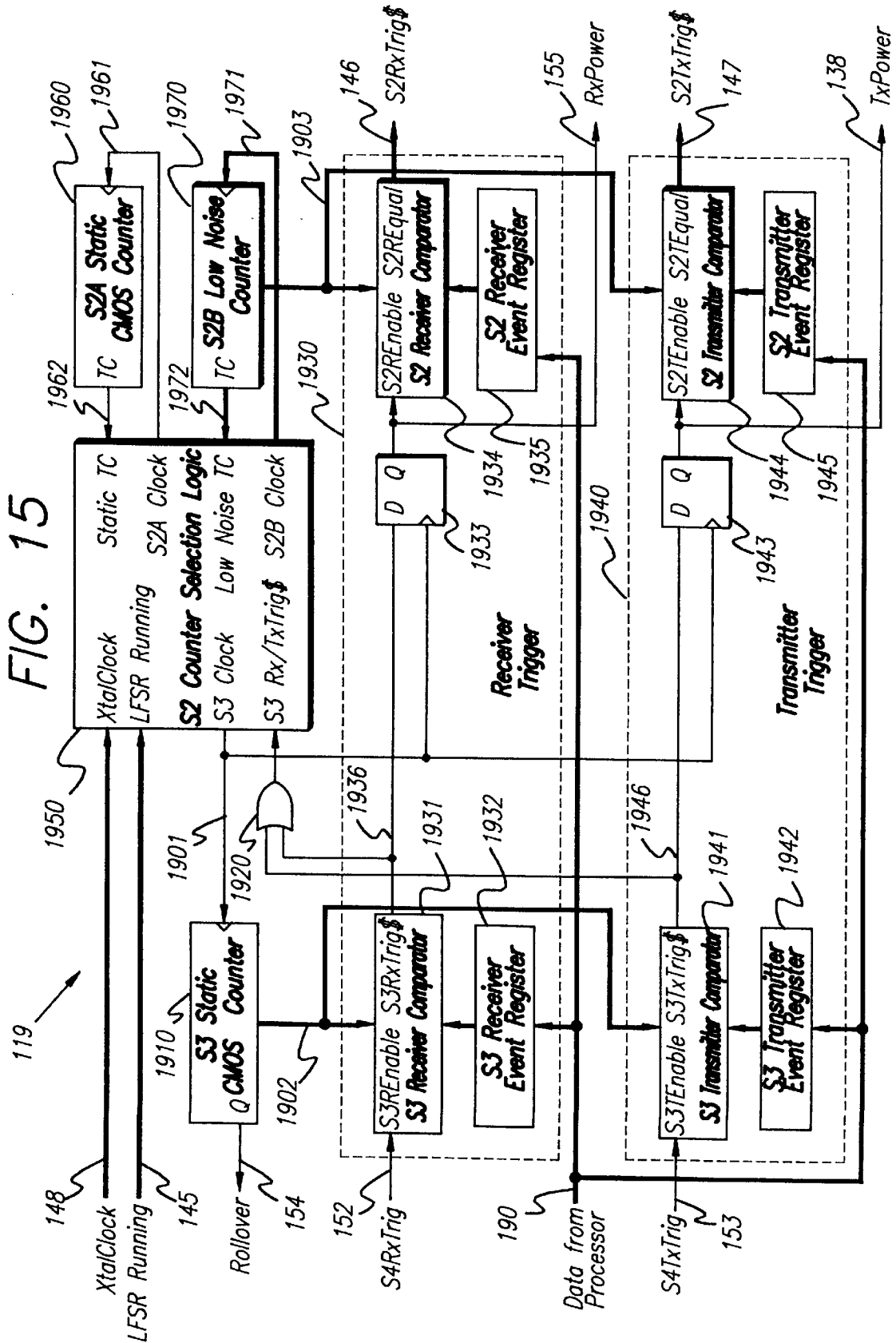


FIG. 16

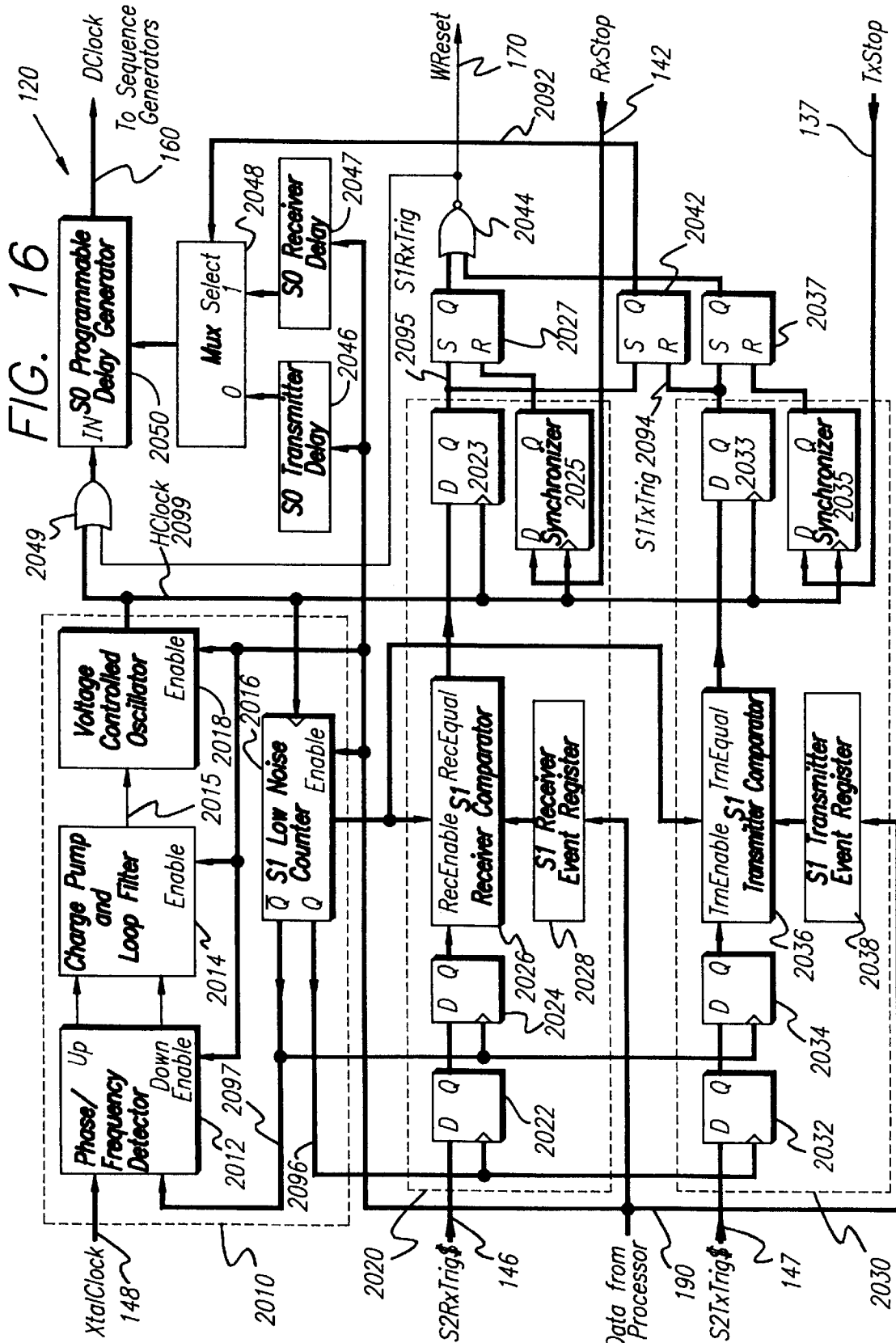


FIG. 17a

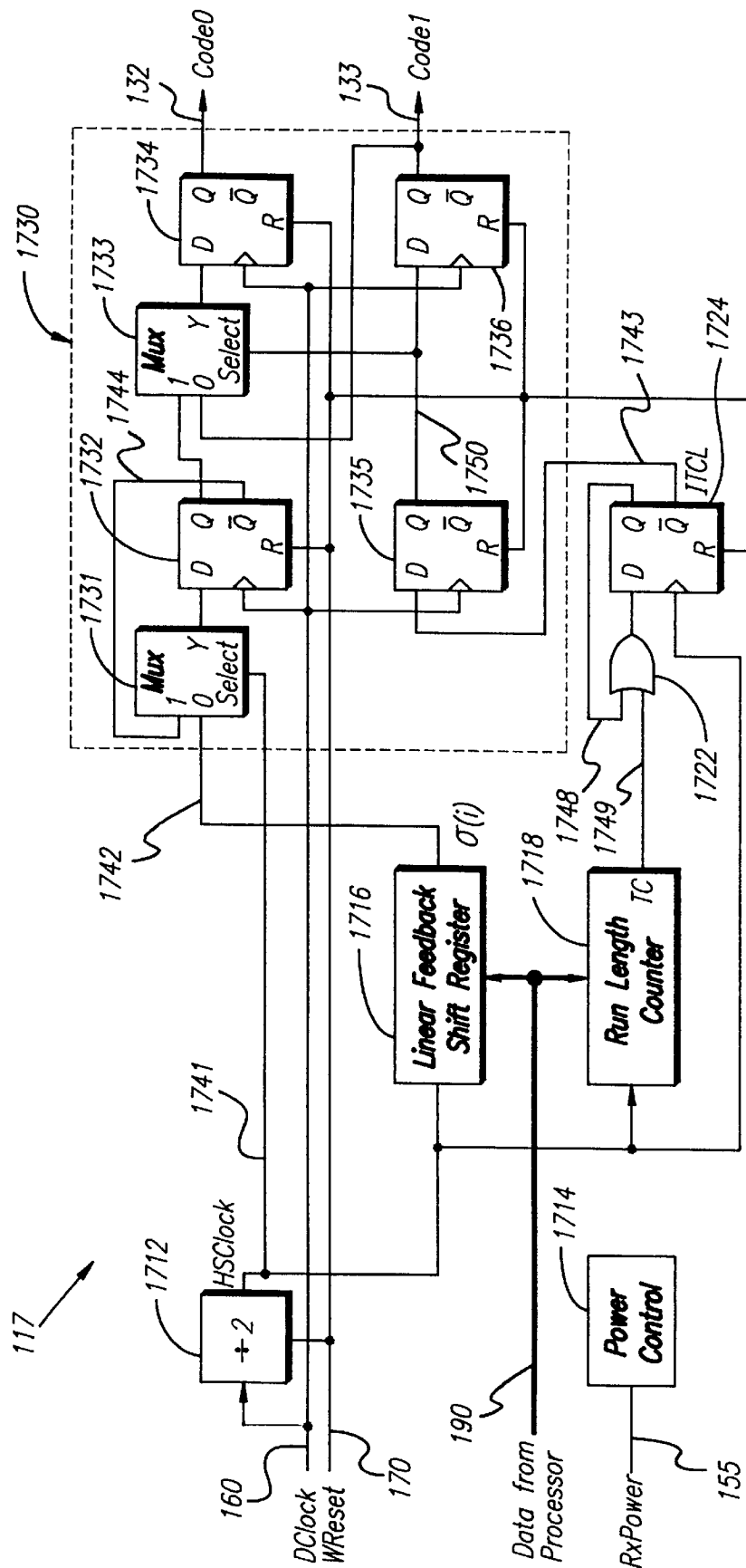


FIG. 17b

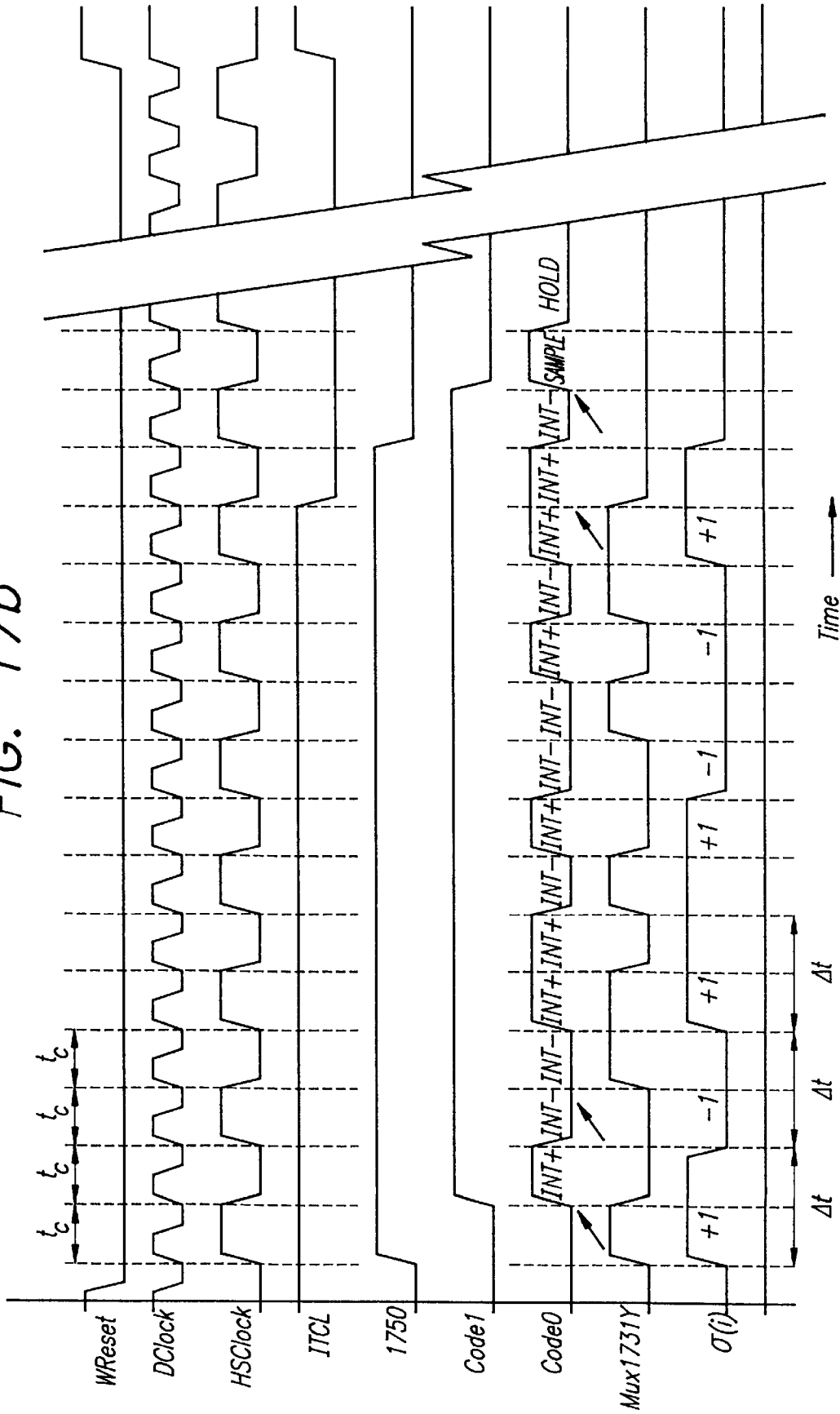


FIG. 18-1

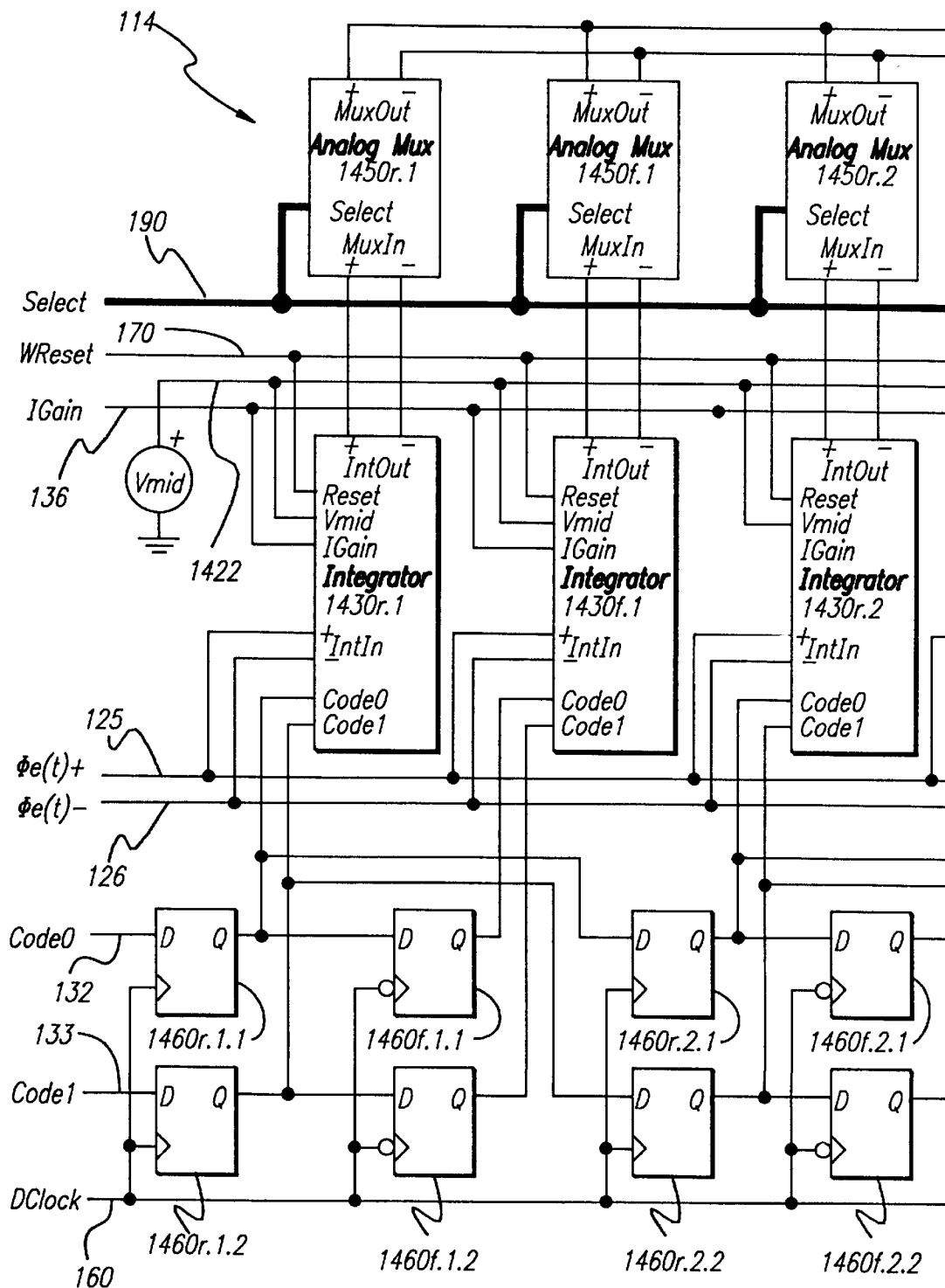


FIG. 18-2

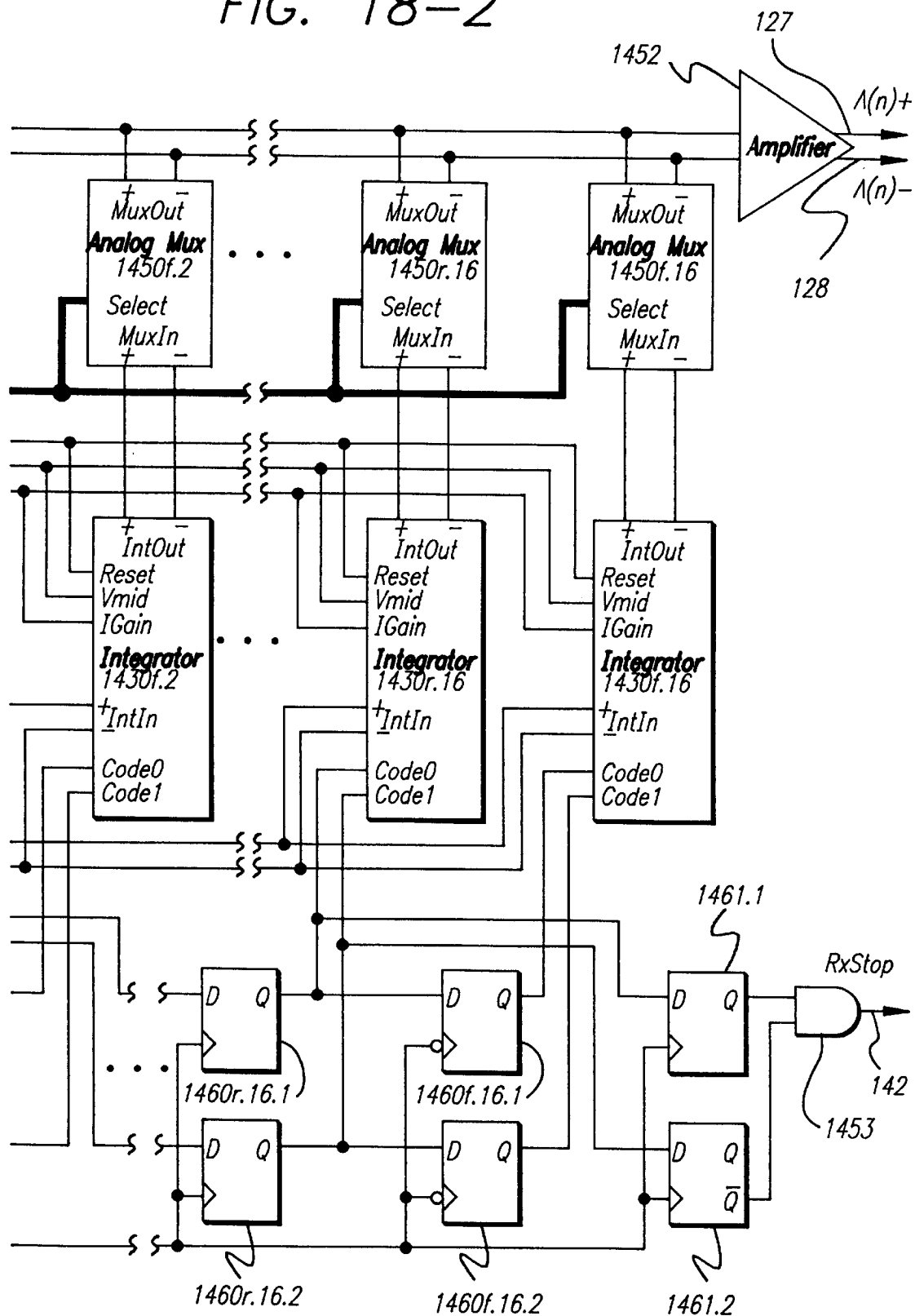
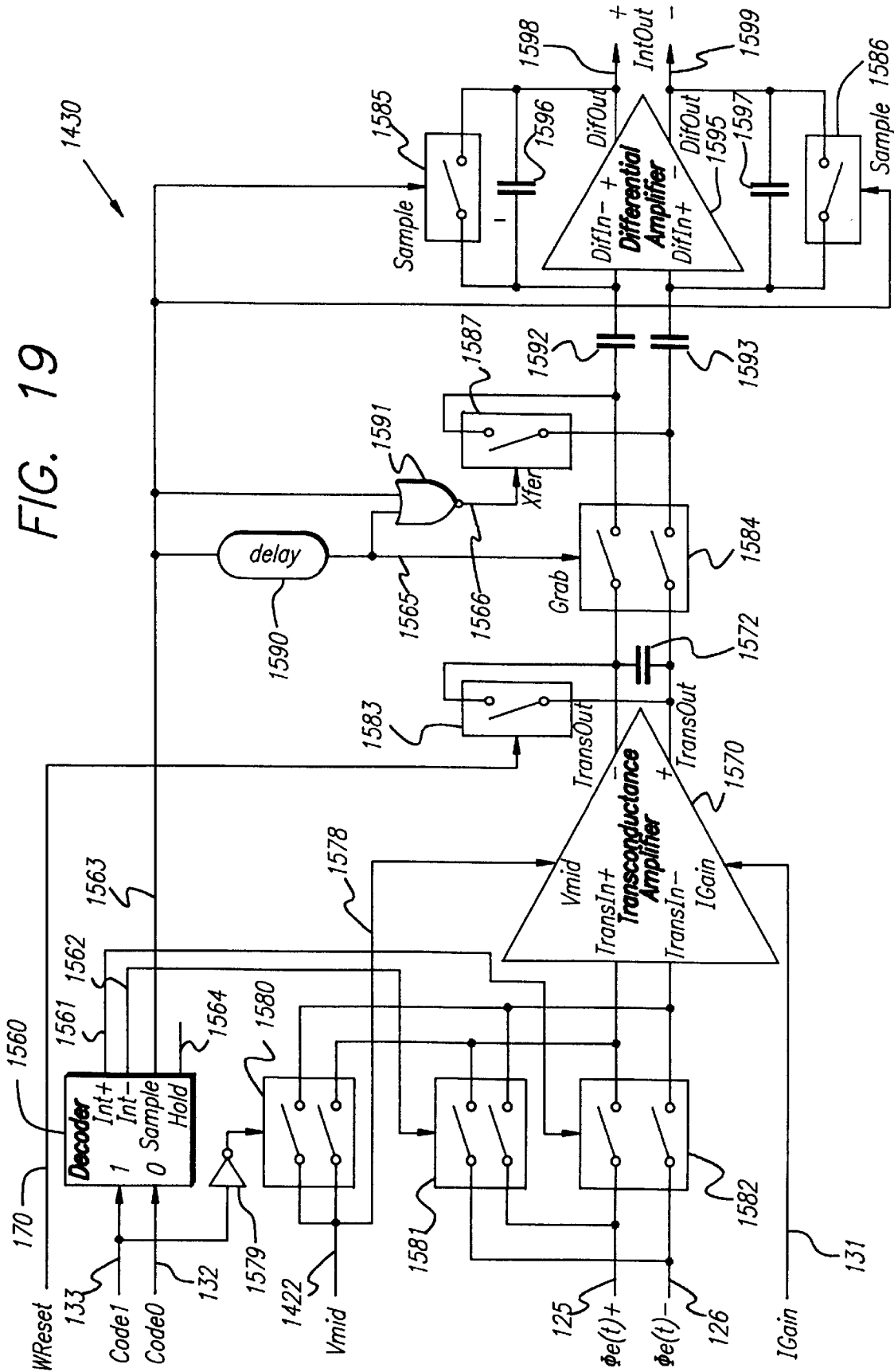


FIG. 19



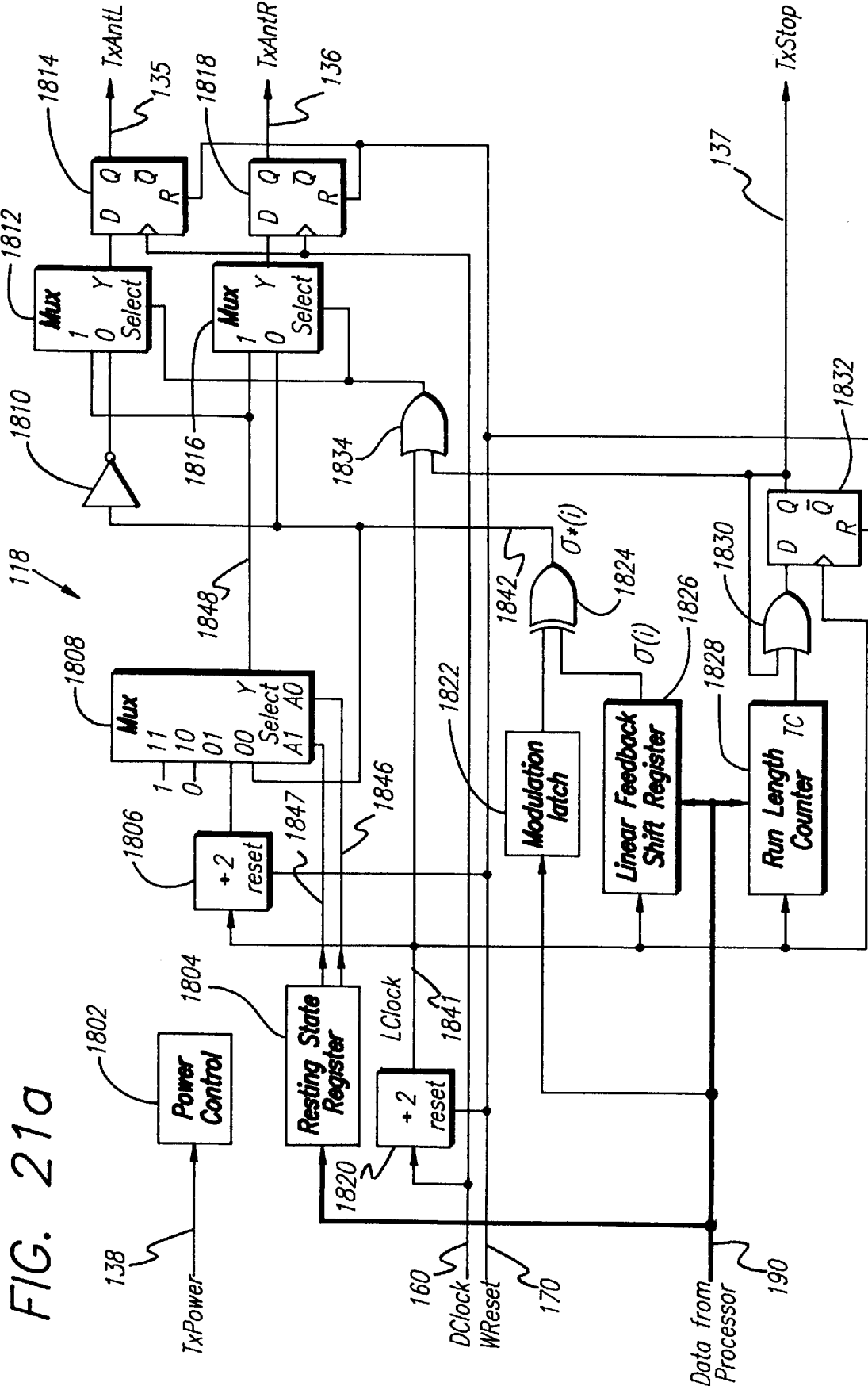


FIG. 21a

FIG. 21b

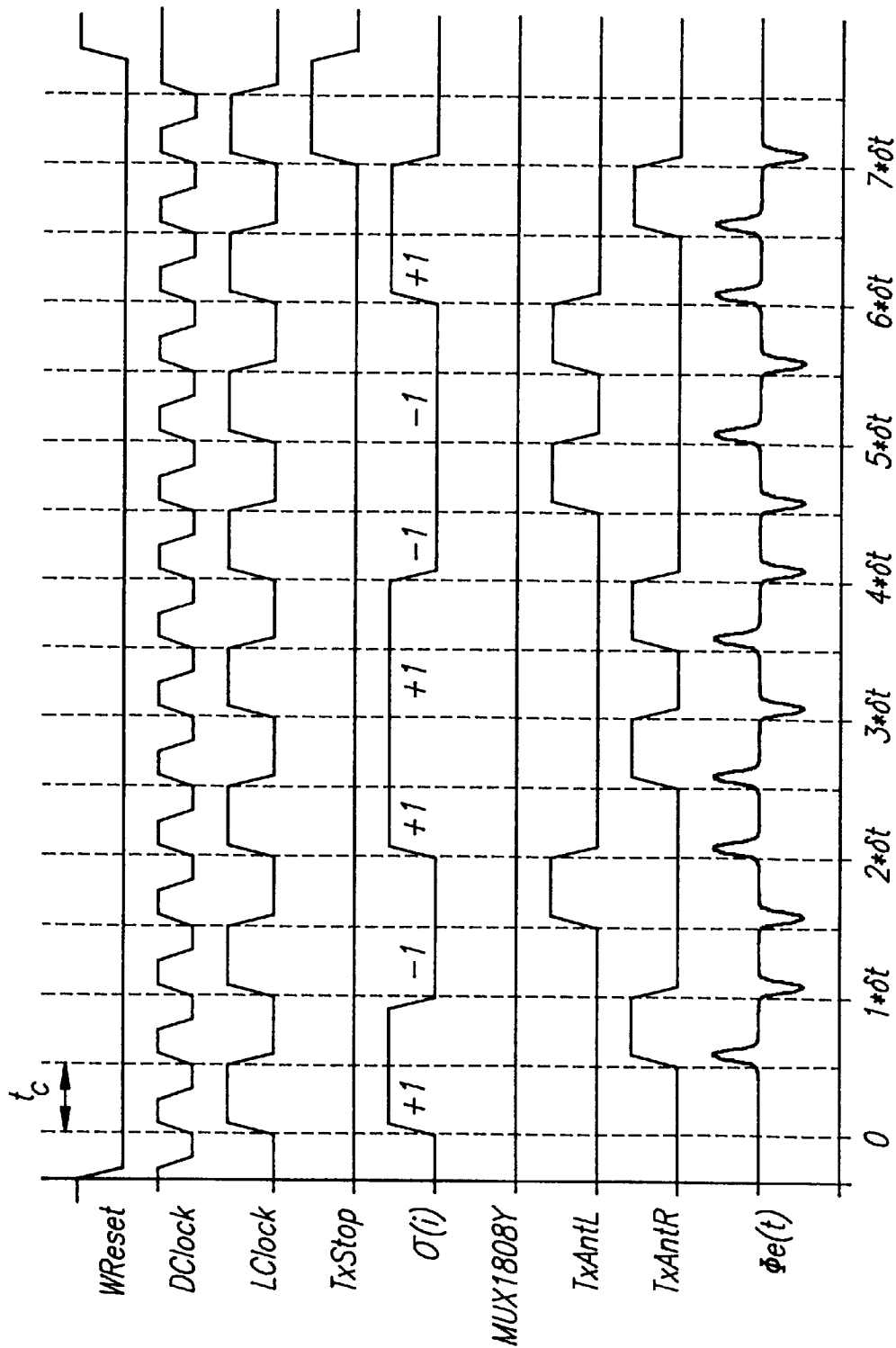


FIG. 21C

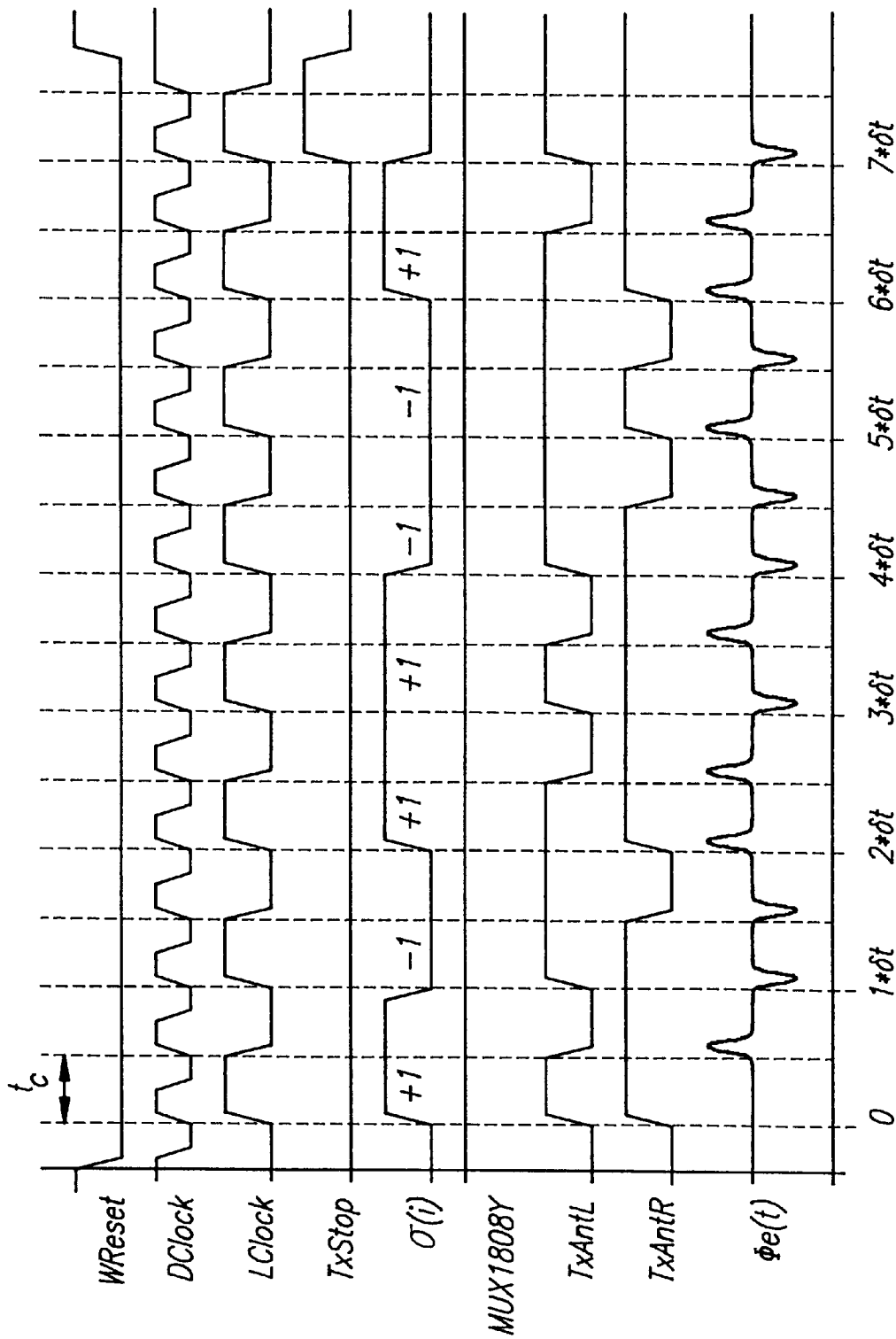


FIG. 21d

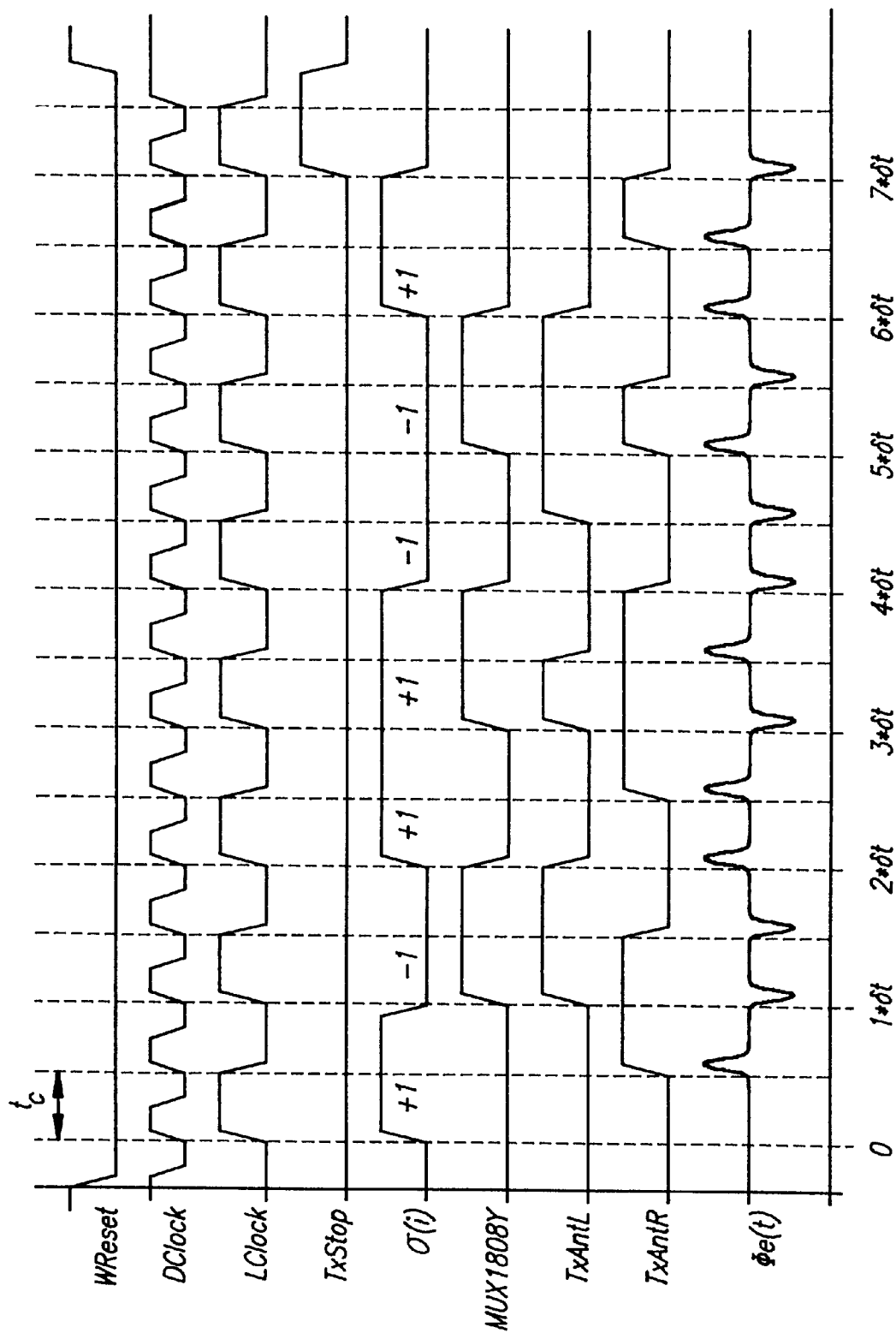


FIG. 21e

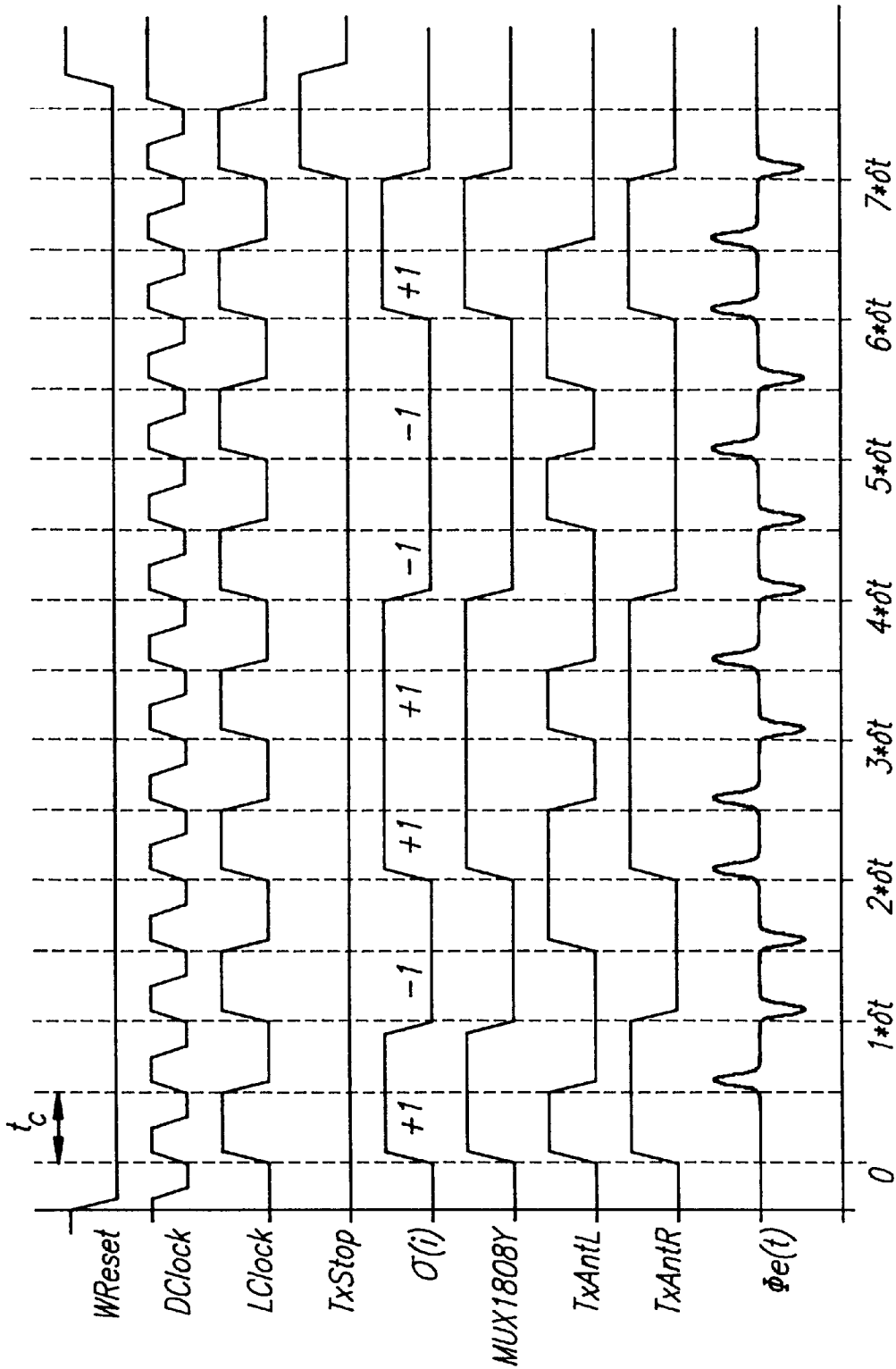
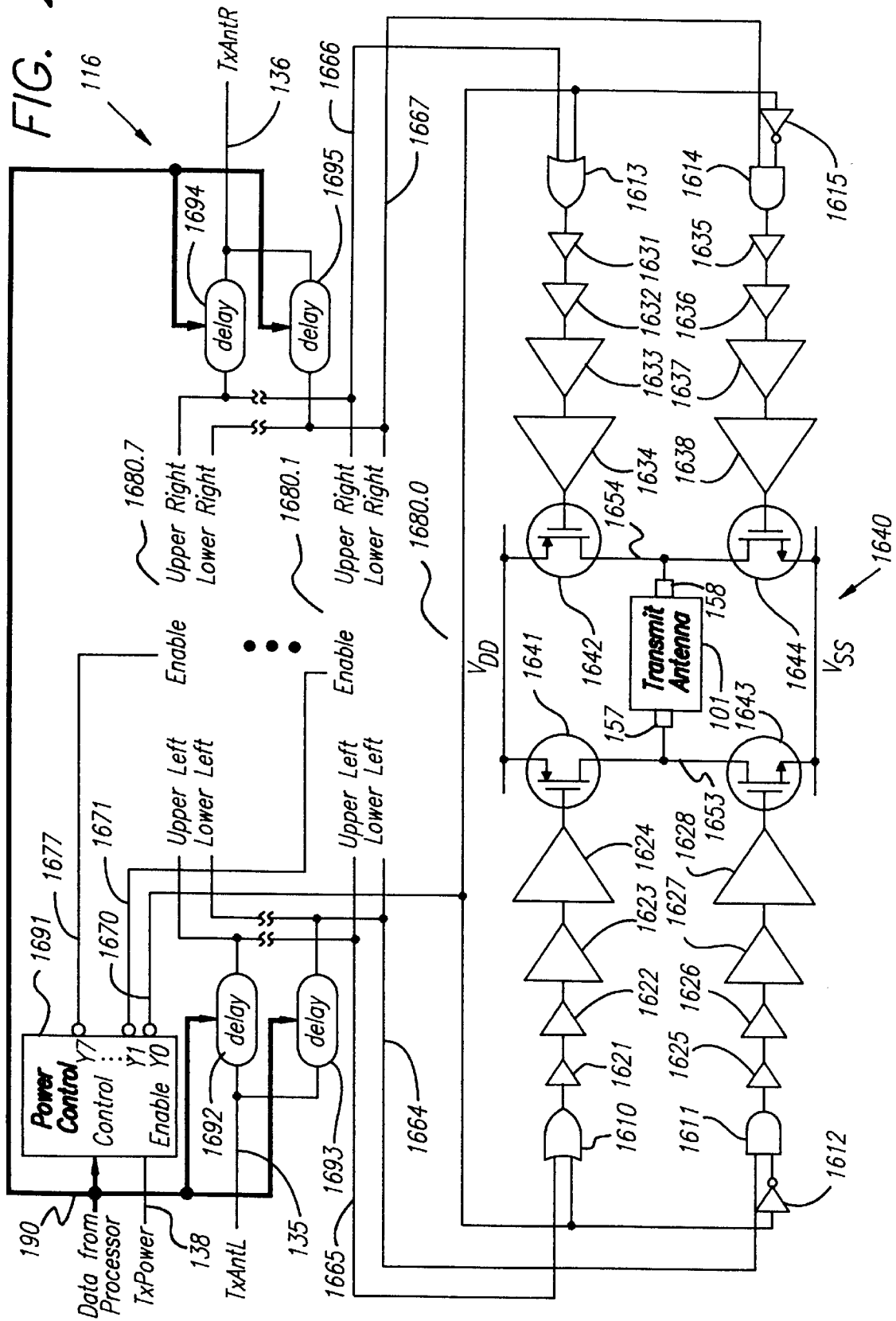


FIG. 22



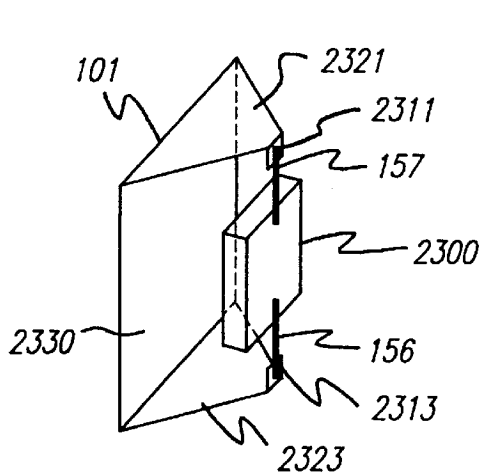


FIG. 23a

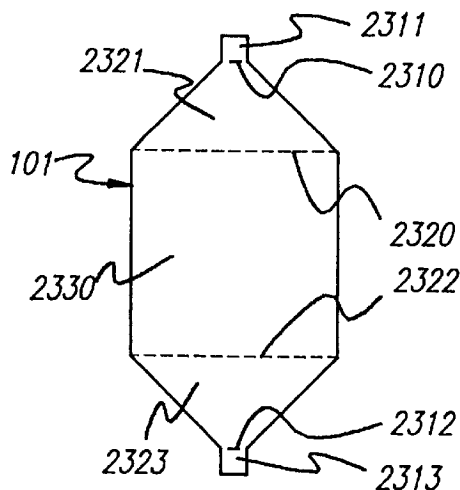


FIG. 23b

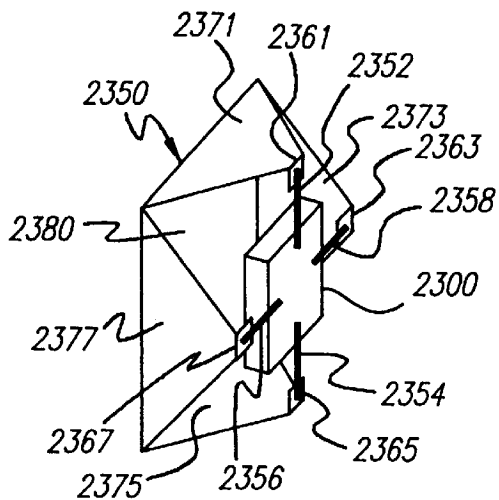


FIG. 23c

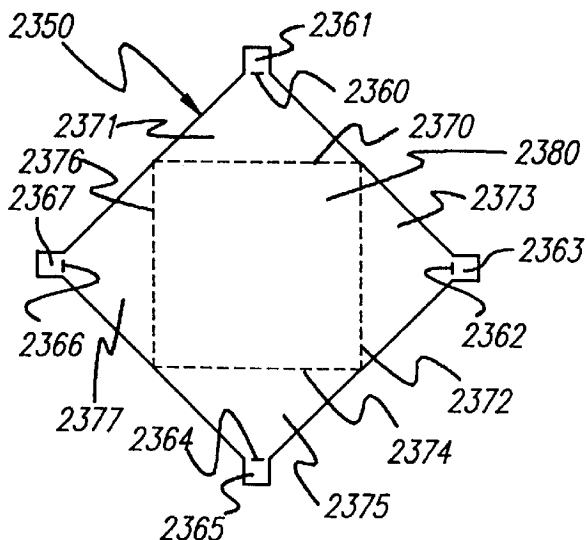


FIG. 23d

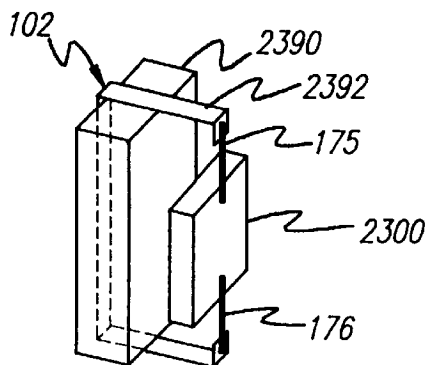


FIG. 23e

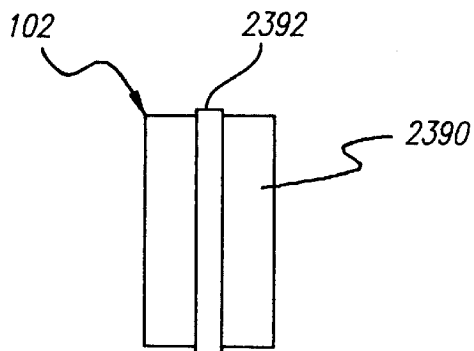
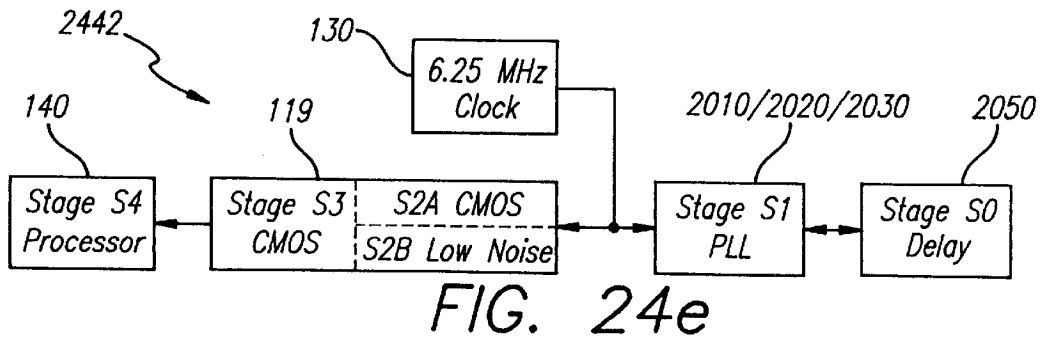
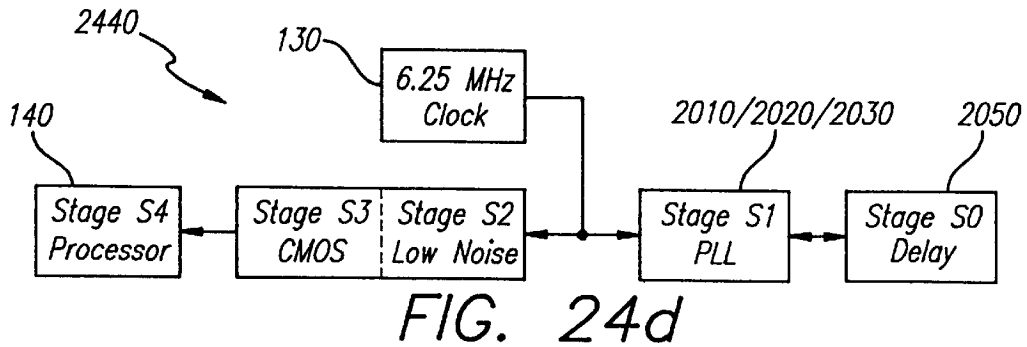
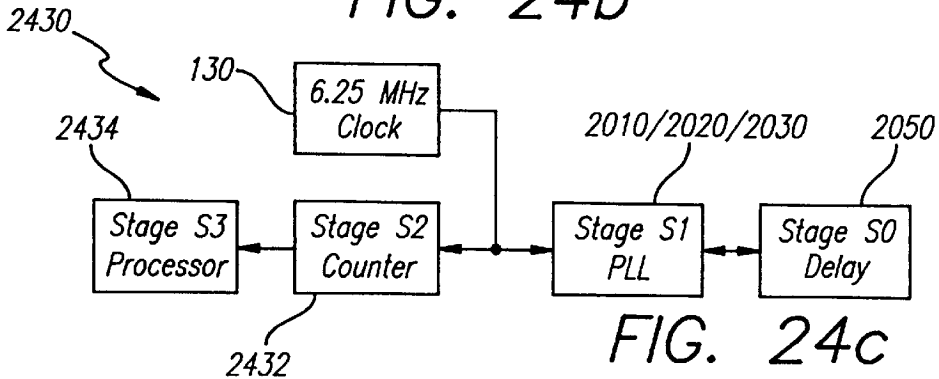
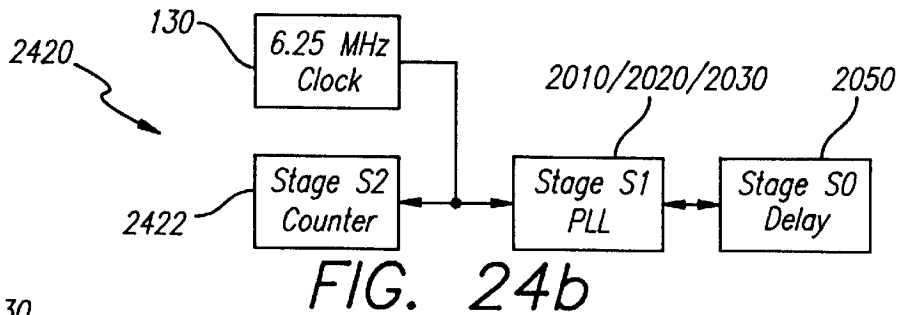
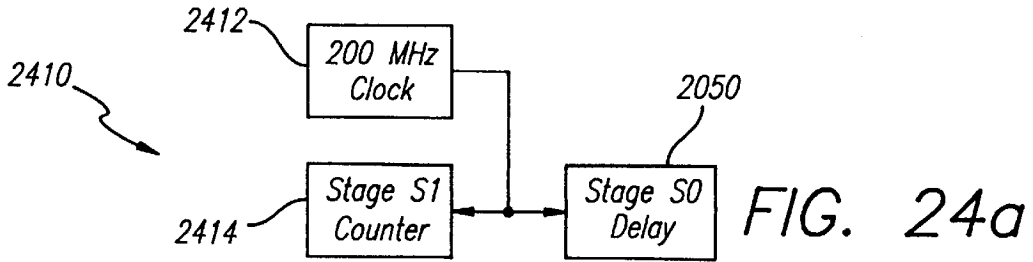


FIG. 23f



SPREAD SPECTRUM LOCALIZERS

This is a division of application Ser. No. 08/279,329 filed on Jul. 22, 1994, now U.S. Pat. No. 5,748,891.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention is related generally to spread spectrum radio communication systems, and more particularly to nonsinusoidal spread spectrum radio communication systems used to determine the locations of transceivers.

2. Prior Art

In traditional radio communication systems the transmitted electromagnetic power is concentrated in a narrow frequency band, whereas in spread spectrum communication systems the power is distributed over a relatively large bandwidth. Spread spectrum radio communications are used in place of traditional systems to circumvent communications jamming by interference signals, prevent detection and interception by unwanted receivers so as to provide privacy, provide tolerance to multipath transmissions, send multipole independent signals over a frequency band, and/or provide accurate ranging information.

The standard categories of spread spectrum radio communication techniques include direct sequence, frequency modulation, chirp modulation (or linear frequency modulation), and time hopping. In chirp modulation each transmitted pulse has a carrier frequency which changes linearly with time. The reception circuitry is designed such that the propagation of the signal through the circuitry is inversely related to the carrier frequency, so that the length of chirped pulses are shortened and there is increased signal power during the pulses in comparison to unchirped signals. In frequency hopping transmissions the frequency of the carrier changes according to a pseudorandom sequence. The receiver must know the pseudorandom sequence to be able to tune to the correct carrier frequencies at the proper times. Time hopping transmissions consist of a sequence of frames, each frame having a single impulse or monocycle (see R. A. Scholtz, "Multiple Access with Time-Hopping Impulse Modulation," MILCOM'93, Bedford, Mass. 1993). the location of the pulses in the frames is determined by a pseudorandom sequence, and without knowledge of the sequence the signal cannot be detected.

In direct-sequence spread-spectrum transmissions, the transmitted signal $a(t)$ is encoded with a data string $d(t)$ of positive and negative unity according to

$$a(t) = \Psi(t) d(t) \cos(\omega t + \theta),$$

where t is time, ω is the angular frequency of the carrier, θ is a phase angle, and the modulating signal $\Psi(t)$ is a string of pseudorandom sequences $\Phi(t)$, the pseudorandom sequences $\Phi(t)$ being repeated M times, i.e.,

$$\Psi(t) = \Phi(t \bmod t_3),$$

where "mod" represents the modulo operation, t_3 is the length of the pseudorandom sequence, $\Phi(t)$ is zero outside the range $0 \leq t \leq t_3$, and $\Psi(t)$ is equal to zero outside the range $0 \leq t \leq M t_3$. The signal $d(t)$ is a data stream of positive and negative unity values, the values of $d(t)$ changing at the beginning of each cycle of the pseudorandom signal $\Phi(t)$. Each pseudorandom sequence $\Phi(t)$ consists of a string of basic units called "chips." Each chip consists of a chip function $\gamma(t)$ —in the simplest cases the chip function $\gamma(t)$ has a constant value—multiplied by a code sequence $\sigma(i)$, where

i is an integer and σ takes on the phase factor values of plus and minus one. Each chip has a length of δt , and if there are L chips per pseudorandom sequence $\Phi(t)$ then $\Phi(t)$ has a period t_3 of $(L * \delta t)$. The pseudorandom sequence $\Phi(t)$ therefore has the functional form

$$\Phi(t) = \gamma(t \bmod \delta t) * \sigma[t/\delta t],$$

where the square brackets indicate the largest integer less than or equal to the argument within the brackets, and $\gamma(t)$ is zero outside the range $0 \leq t \leq \delta t$. When $1/\omega$ is much smaller than the chip length δt , and the value of $\Phi(t)$ changes much faster than the value of $d(t)$ (for instance when L is much greater than unity) the transmitted spectrum has a width on the order of the width of the spectrum of the chip function $\gamma(t)$. This relation allows the transmitted spectrum to be "spread" by imposing a chip function $\gamma(t)$ with a wide spectrum. To receive the direct sequence transmission it is necessary to know the pseudorandom sequence $\Phi(t)$ and the phase of the carrier and the chip function $\gamma(t)$. It should be noted that all the above-mentioned spread spectrum techniques rely on a sinusoidal carrier.

Historically, localization systems have been used for surveying and military applications, such as troop positioning and aircraft and missile guidance. The most prevalent military localization systems, Loran, Omega, and Global Positioning System (GPS), determine position based on the propagation time of the electromagnetic signals from beacons at known locations. Loran and Omega beacons are ground-based, and GPS transmitters are satellites. In these localization technologies, pulses are modulated onto a sinusoidal carrier, and traditional resonant circuits are used for transmission and reception.

The GPS system utilizes 21 active satellites in 12-hour orbits above the Earth to allow determination of three-dimensional position to an accuracy to about 10 meters, and velocity to an accuracy of 0.03 meters/second. At any location on Earth at least four GPS satellites are above the horizon at all times. Each satellite transmits the position of the satellite in space, and highly accurate time information derived from an onboard atomic clock. The user's position and the bias of the user's clock are determined by measuring the time for propagation of the signals from the satellites to the user.

Because refraction effects, deviations in velocity and variations in amplitude of radio waves propagating through the ionosphere increase with decreasing frequency, the accuracy of a satellite-based localization system is increased by using high frequency radio transmissions. However, the frequency is limited by practical circuit-design considerations and the fact that the absorption of radio transmissions by water molecules, even in fair weather, increases sharply near 10 GHz. The satellites transmit at two frequencies 1.227 GHz and 1.575 GHz, to allow corrections to be made for frequency-dependent time delays in the propagation of the signals through the atmosphere. Because gigahertz radio transmissions are line-of-sight, a GPS receiver must have a clear view of the sky and at least four satellites to function. This limits the applications to which this technology can be applied.

Since it is difficult to construct gigahertz resonant systems using inexpensive integrated circuitry, such localization systems must be constructed from discrete components, and powered accordingly. To provide reasonable efficiency, antennas for gigahertz reception must be on the order of at least ten centimeters. These limitations in the miniaturization of sinusoid-based localizers, while within bounds acceptable for military and industrial applications, provide

limits as to the applicability of sinusoid-based localization technologies, such as GPS, to many aspects of everyday life. Overview of the Present Invention

The present invention is directed to a network of nonsinusoidal spread spectrum (NSS) transceivers capable of precisely locating objects in three-dimensional space. In the preferred embodiment these "localizers" are about the size of a coin, can operate without a clear view of the sky, have a low enough power consumption that they can operate for long periods of time powered by a small battery, do not require a system of satellites, and are very inexpensive.

Such localizers can be utilized in a myriad of applications, serving as extensions of the senses of people and machines. It is envisioned that these localizers will someday be commonly used in almost every aspect of everyday life. For instance, a localizer could be attached to the clothing of a young child, and if that child were to enter an area that presented a danger to her an alarm could sound to alert her or her guardians. Such localizers might also be used to help members of a group, such as a family, locate each other in a crowd or a large building complex. Such localizers might also be placed on each item in a store, so that the items could be easily located and an inventory of the store items could be tallied electronically.

The method of the present invention is to be contrasted with radar distancing where there is lower distance resolution since radar pulses must be relatively long to modulate a sinusoidal carrier. Furthermore, radar distancing requires high-power transmissions since the detected signals are reflected from the target rather than broadcast by the target.

The limitations of the sinusoidal-carrier transmissions are circumvented in the present invention by a radio communication system where sequences of electromagnetic impulses are not modulated by a sinusoidal carrier. (In this specification an "impulse" will refer to an electromagnetic signal, or the electric signal in a circuit generating the electromagnetic signal or otherwise directly corresponding thereto, which is a Gaussian or short rectangular signal and does not modulate another signal. In contrast, a "pulse" will refer to an electromagnetic signal, or the electric signal in a circuit generating the electromagnetic signal or otherwise directly corresponding thereto, which has a sinusoidal carrier modulated by a short signal such as a Gaussian. Also, a "pulse" will refer to short signals in a circuit which do not directly correspond to or generate electromagnetic signals, such as "clock pulses.") These nonsinusoidal spread spectrum (NSS) transmissions $a(t)$ are of the form

$$a(t) = \Psi(t) * d(t),$$

where, as before,

$$\Psi(t) = \Phi(t \bmod t_3),$$

t is time, $d(t)$ is the data function with values of positive and negative unity, $\Phi(t)$ is a pseudorandom sequence of impulses of length t_3 and is nonzero over the range $0 \leq t \leq t_3$, and $\Psi(t)$ is a string of M repeated pseudorandom sequences $\Phi(t)$ and is nonzero over the range $0 \leq t \leq M * t_3$. One or more bits of data from $d(t)$ is encoded on each repetition of the pseudorandom sequence $\Phi(t)$. The transmitted spectrum has a width on the order of the width of the spectrum of an impulse. NSS radio technology can generate bandwidths 10–100 times as great as those for sinusoidal-carrier technologies mentioned above. By controlling the spacing between impulses, maxima in the energy of the transmitted signals can be placed at strategic locations, such as between commercial radio and television bands.

Reception of such NSS transmissions is accomplished by circuitry which calculates the correlation between the received signal and the expected pseudorandom sequence $\Phi(t)$. To receive a transmission, the transmitted pseudorandom sequence must be known by the receiver. Useful pseudorandom sequences must have low cross-correlations and sharp peaks in their autocorrelation function. With low cross-correlations the communications between one pair of localizers using one pseudorandom sequence will not interfere with the communications of other localizers in the vicinity using other pseudorandom sequences. A sharply peaked autocorrelation function is required to determine the arrival time of an impulse sequence. The fine detail of the autocorrelation function is used to improve the accuracy of the arrival time determination.

To generate the sequences of impulses that are transmitted, and to process the sequences of impulses that are received, the circuitry of the localizers must switch currents on and off at a rate comparable to the rate of transmitted impulses in the pseudorandom sequences. However, the operation of normal digital logic generates noise which is electrically coupled back into the receiving circuitry, so it may mask the reception of communications. Also, since a change in current generates an electromagnetic field, the circuitry generates NSS noise which contributes to the noise, masking communications transmissions. Therefore, during reception the localizers of the present invention use only low-noise circuitry to raise the signal-to-noise ratio. The low-noise circuitry has a higher power consumption than normal CMOS circuitry, since it uses current-steering logic rather than current-switching logic, and is therefore operated only when necessary. During transmission the localizers of the present invention use circuitry having parallel routing of differential signals to reduce the susceptibility of the logic to noise, and balance the current flow between sections of the circuit. In the preferred embodiment, portions of the circuitry which are used for both transmission and reception utilize both current-steering logic and parallel routing of differential signals.

Relative distances between localizers are determined by measuring the propagation time of pulse sequences between localizers. Knowing the distance between a first localizer and a second localizer, then the relative position of the first localizer is known to be on a sphere with a radius equal to the known distance centered around the second localizer. Similarly, knowing the distances from a first localizer to a second localizer and a third localizer, and the distance between the second and third localizers, then the relative position of the first localizer is known to be on a circle. Knowing the distances from a first localizer to a second localizer, a third localizer, and a fourth localizer, and the distances between the second, third, and fourth localizers, then the relative position of the first localizer is known to within one of two points, a reflection about the plane defined by the second, third and fourth localizers. Therefore, to actually determine the relative position of a localizer more information is needed: the distance of that localizer to four other localizers and the relative positions of those four localizers must be known. Therefore, the relative positions of a large network of localizers may be determined by repeatedly determining the distances from a localizer with an unknown relative position to four localizers with known relative positions.

However, it should be noted that there are combinations of locations that make the determination of the three-dimensional locations impossible. For example, when all the

localizers of known relative positions are on a plane then the position of another localizer can only be determined to within two points, a reflection about the plane in which the other localizers are located. In addition, some reference points are necessary to determine absolute locations since the distancing communications only provide relative locations. In a survey application, for example, reference localizers would be arranged on known control points so absolute positions could be determined. Another option is to place localizers on both ends of rods that hang free in gravity, thereby providing orientation information.

To determine distances to an accuracy of 1 cm it is required that the clocks in the localizers are accurate to 30 picoseconds over times on the order of the time for propagation of radio waves between localizers. A typical separation distance is 300 meters, so a typical propagation time is 1 microsecond. The clock rates must also be stable to times on the order of tens of picoseconds over the length of a pulse sequence, which is on the order of 10 microseconds. This represents a required stability of one part in one million. Pairs of localizers of the preferred embodiment prearrange when their next communication will occur, and listen for the communication during a time window of approximately 100 nanoseconds centered around the prearranged time. Times between localizer communications can be on the order of one tenth of a second, and so the clocks must also be stable to about 100 nanoseconds over periods on the order of one tenth of a second, representing a required stability of one part in one million to maintain synchronization.

Inexpensive quartz oscillators are normally not considered accurate enough for this task due to the difference between their actual frequency and their normal frequency. But their stability (i.e., the rate at which the frequency may wander with time) is sufficient for use with the localizers of the present invention. Because localizers have on-board processors, each processor can monitor the clocks of other localizers and calculate the ratios of their clock rates to its own. This allows each localizer of the present invention to correct for differences between its clock rate and those of the localizers it is communicating with. Therefore, the localizers of the present invention can provide a highly accurate clock timebase from a network of inexpensive, inaccurate oscillators.

Ranging protocols which determine the relative clock rates as well as the distances between localizers may be implemented. If a network of communicating localizers includes at least one localizer having a very precise timebase, the other localizers can determine the deviations of their timebases from the precise timebase using such protocols. Similarly, a known accurate distance between two localizers can be used to provide an accurate timebase, and other localizers can determine the deviations of their timebases from the precise timebase using ranging protocols. It is advantageous in terms of size, cost and power to use protocols which determine relative clock rates to provide a network with a highly accurate timebase, rather than providing each localizer with a timebase of comparable accuracy.

A transmission from a localizer is composed of the following events: (i) a sequence generator is programmed to produce a code sequence; (ii) the power to the antenna is adjusted to compensate for the expected distance the signal must travel; (iii) a set of event registers is armed to trigger the transmission circuitry at a pre-arranged time; and (iv) when the transmission event is triggered the transmitter uses the code sequence to generate a series of positive and negative currents through the antenna to transmit a non-

sinusoidal spread spectrum (NSS) radio signal composed of doublets of Gaussian impulses. Each doublet consists of an impulse of a first polarity and an impulse of a second polarity opposite the first. During a time period surrounding and including the transmission, the CPU and any other non-essential circuitry is shut down to prevent the transmissions from interfering with the functioning of the circuitry.

The reception of a code sequence consists of a similar sequence of operations, namely: (i) a sequence generator is programmed to produce an internally-generated integration sequence which resembles the expected code sequence of the received signal; (ii) the receiver antenna and integrator amplifiers are adjusted to compensate for the distance the received signal is expected to have traveled and the length of the code sequence; (iii) a set of event registers is armed to trigger reception processing circuitry at a pre-arranged time; (iv) the CPU and other nonessential circuitry is turned off during a time period surrounding and including the reception time to decrease noise; (v) during the reception event the received signal is multiplied by integration sequences delayed by thirty-two (in the preferred embodiment) different time offsets; (vi) during the reception event the products of the received signal and the delayed integration sequences are integrated and the outputs are stored in thirty-two analog bins; and (vii) after the reception event the CPU, which has been reactivated, converts these thirty-two analog bins to digital values and analyzes these values to calculate the precise arrival time of the communication.

Overview of the Pseudo-autocorrelation Function

According to the present invention the time when an impulse sequence is received is determined from the location of the peak and other features of the correlation between the received antenna signal $a(t)$ and a set of delayed internally-generated integration sequences $\Psi_i(t)$. (For simplicity of notation the following discussion will assume that only one bit of information is transmitted via a single pseudorandom sequence, i.e., $\Psi(t)=\Phi(t)$.) It will be assumed that the received antenna signal has been encoded on an externally-generated pseudorandom sequence $\Phi_c(t)$ at a remote transmitter. The externally-generated pseudorandom sequence $\Phi_c(t)$ consists of a series of externally-generated chip waveforms $\gamma_c(t)$, i.e.,

$$a(t)=\Phi_c(t)=\sigma_c \int [t/\delta t] * \gamma_c(t \bmod \delta t).$$

Similarly, the internally-generated pseudorandom sequence $\Phi_i(t)$ consists of a series of internally-generated chip waveforms $\gamma_i(t)$, i.e.,

$$\Phi_i(t)=\sigma_i \int [t/\delta t] * \gamma_i(t \bmod \delta t),$$

where $\gamma_i(t)$ resembles, but is not equal to, $\gamma_c(t)$. The correlation function Λ between the received signal $\Phi_c(t)$ and the internally-generated "integration" sequence $\Phi_i(t)$ is

$$\Lambda(t)=\int \Phi_i(\tau-t) * \Phi_c(\tau) d\tau,$$

or

$$\Lambda(t)=\int \sigma_i \int [\tau-t]/\delta t * \sigma_c \int [\tau/\delta t] * \gamma_i((\tau-t) \bmod \delta t) * \gamma_c(\tau \bmod \delta t) d\tau.$$

The correlation function $\Lambda(t)$ is termed the pseudo-autocorrelation function, since for the special case $\sigma_i=\sigma_c$ and $\gamma_i=\gamma_c$ the function is the autocorrelation function. The family of pseudorandom code sequences $\sigma(i)$ is chosen such that the

values of $\Lambda(t)$ are small if $\sigma_i(i)$ is not equal to $\sigma_c(i)$. If the internally- and externally-generated code sequences $\sigma_i(i)$ and $\sigma_c(i)$ are the same (i.e., $\sigma_i = \sigma_c = \sigma$), then

$$\Lambda(t) = \int \sigma[\tau/\delta t] * \sigma[(\tau-t)/\delta t] * \gamma_1(\tau-t) \text{ mod } \delta t * \gamma_c(\tau \text{ mod } \delta t) d\tau,$$

and the substitution $\tau \rightarrow \tau+t$ shows that the pseudo-autocorrelation function is symmetric about $t=0$. For $t=0$ and $\sigma_i = \sigma_c = \sigma$,

$$\begin{aligned} \Lambda(0) &= \int \gamma_i(\tau \text{ mod } \delta t) * \gamma_c(\tau \text{ mod } \delta t) d\tau \\ &= L \int_0^{\delta t} \gamma_i(\tau) * \gamma_c(\tau) d\tau \end{aligned}$$

since $(\tau(i))^2=1$ for all values of i , where L is the number of chips in the pseudorandom sequence. Thus $\gamma_i(t)$ must resemble $\gamma_c(t)$ to an extent sufficient to make the integral relatively large, i.e.,

$$\frac{[\int \gamma_i(\tau) * \gamma_c(\tau) d\tau]^2}{[\int \{\gamma_i(\tau)\}^2 d\tau] * [\int \{\gamma_c(\tau)\}^2 d\tau]}$$

must be on the order of unity, if the pseudo-autocorrelation $\Lambda(t)$ is to have a strong peak.

Values of the pseudo-autocorrelation at a number of discrete times is determined by a time-integrating correlator circuit. Although the correlator output resembles a time sampling of the pseudo-autocorrelation $\Lambda(t)$, it should be noted that the pseudo-autocorrelation as a function of time is never actually determined by the circuit, and therefore it cannot be sampled. The values of pseudo-autocorrelation function at a number of discrete times will be termed the discrete-time pseudo-autocorrelation function, or DTPAC function, and notated as $\Lambda(n)$, where the argument n takes on integer values. The times at which values of the DTPAC function are determined are referred to as the "time bins." Overview of the Doublet Chip Functions

Whereas other radio systems using impulses radiate sequences of single electromagnetic impulses with a minimum of radiation between impulses, the present invention is directed to radio transmissions comprised of sequences of pairs of impulses, termed "doublets." As will be discussed below, switching on a current through the antenna produces a first electromagnetic impulse having an electric field vector in a first direction, and switching off the current produces a second electromagnetic impulse having an electric field vector in a second, opposite direction. As discussed above, the received signal $\Phi_c(t)$ and the internally-generated integration sequence $\Phi_i(t)$ are of the form

$$\sigma[t/\delta t] * \gamma(t \text{ mod } \delta t).$$

In the preferred embodiments of the present invention the doublet chip waveform $\gamma(t)$ has a first section with a first polarity and a second section with a second polarity opposite the first polarity. As before, $\sigma(i)$ is a pseudorandom code sequence of the values plus and minus one, i takes on integer values, δt is the length of the chips, and the square brackets indicates the greatest integer less than or equal to the value of the argument within the brackets.

Applying this doublet chip waveform to the transmitted signal and the impulse sequence provides the advantage that the central positive peak of the pseudo-autocorrelation function is bracketed by two negative peaks, as well as additional positive and negative peaks in the wings of the function. As

will be discussed in the Detailed Description of the Preferred Embodiments, the positive and negative peaks of the pseudo-autocorrelation function make the shape of the discrete-time pseudo-autocorrelation (DTPAC) function particularly sensitive to small time displacements between the received signal $\Phi_c(t)$ and the integration sequence $\Phi_i(t)$ when the time between bins Δt is on the order of half of the chip length. In the preferred embodiment an expert system algorithm, such as a set of neural networks, is used to recognize changes in the shape of the DTPAC function to determine the temporal relationship between the antenna signal $\Phi_c(t)$ and the integration sequence $\Phi_i(t)$ to a time less than the separation between time bins.

Different placements of time bins and different internally-generated chip doublet functions $\gamma_i(t)$ provide different advantages. A general form for the doublet waveform $\gamma_i(t)$ is

$$\begin{aligned} \gamma_i(t) &= +k & 0 < t < h * \delta t \\ \gamma_i(t) &= -k & \delta t/2 < t < \delta t/2 + h * \delta t \\ \gamma_i(t) &= 0 & \text{otherwise,} \end{aligned}$$

where h is a width factor, and k is a constant. When the doublet waveform $\gamma_i(t)$ is normalized, the constant k will be set to one. A general expression for the delay between integration sequences is given by $(\delta t/2 - g * \delta t)$, where g is a shift factor.

In a first preferred embodiment depicted in FIG. 14a, the separation Δt between time bins is $(\delta t/4)$, and the doublet waveform $\gamma_i(t)$ is

$$\begin{aligned} \gamma_i(t) &= +1 & 0 < t < \delta t/2 \\ \gamma_i(t) &= -1 & \delta t/2 < t < \delta t \\ \gamma_i(t) &= 0 & \text{otherwise,} \end{aligned}$$

(i.e., $h=1/2$ and $g=1/4$). Once the integration sequence $\Phi_i(t)$ and the received signal $\Phi_c(t)$ are substantially aligned, this system is useful in determining the exact arrival time of the antenna signal since the shape of the pseudo-autocorrelation function changes substantially for small time shifts between the integration sequence $\Phi_i(t)$ and the received signal $\Phi_c(t)$.

In a second preferred embodiment depicted in FIG. 14b, the separation Δt between time bins is $(\delta t/4)$, and the doublet waveform $\gamma_i(t)$ is

$$\begin{aligned} \gamma_i(t) &= +1 & 0 < t < \delta t/4 \\ \gamma_i(t) &= -1 & \delta t/2 < t < 3\delta t/4 \\ \gamma_i(t) &= 0 & \text{otherwise,} \end{aligned}$$

(i.e., $h=1/4$ and $g=1/4$). This system provides a higher signal-to-noise ratio than the first preferred embodiment since for the peak time bin the integrations are only performed when the received signal $\Phi_c(t)$ is relatively large. This second embodiment is useful for the communication of data once a good time alignment has been achieved between localizers. In a generalization of this second preferred embodiment the doublet waveform $\gamma_i(t)$ is

$$\begin{aligned}\gamma_i(t) &= +1 & 0 < t < h * \delta t \\ \gamma_i(t) &= -1 & \delta t / 2 < t < \delta t / 2 + h * \delta t \\ \gamma_i(t) &= 0 & \text{otherwise,}\end{aligned}$$

where small values of h produce narrow nonzero regions of the doublet waveform $\gamma_i(t)$. The optimum value of h produces peaks of the doublet waveform $\gamma_i(t)$ of approximately the same width as the peaks of the received doublet waveforms $\gamma_c(t)$.

In a third preferred embodiment depicted in FIG. 14c, the separation Δt between time bins is $(\delta t/2)$, and the doublet waveform is $\gamma(t)$ is

$$\begin{aligned}\gamma_i(t) &= +1 & 0 < t < \delta t / 2 \\ \gamma_i(t) &= -1 & \delta t / 2 < t < \delta t \\ \gamma_i(t) &= 0 & \text{otherwise,}\end{aligned}$$

(i.e., $h=1/2$ and $g=0$). This system is useful for scanning for a signal when the time of arrival is uncertain because the reception window is twice as long as either of the two previous techniques. In a generalization of the third preferred embodiment, the shift factor g is a small value to insure that sharp peaks in the received signal are detected. There is a finite time required for the doublet waveform $\gamma_i(t)$ to change values between positive and negative unity and if an impulse in the received signal occurs during a zero crossing of the doublet waveform it may not be detected.

Overview of the Ranging Communications

The distance between two localizers, localizer A and localizer B, is determined by measuring signal propagation times in cooperative ranging transactions. Unless otherwise stated, it will be assumed in the following discussions that localizers A and B have an approximate knowledge of their separation and relative clock rates.

In a first ranging protocol shown in FIG. 2, localizer A sends a first ranging communication to localizer B at a prearranged time. Localizer B listens for the first communication during a time window centered around the time the first communication is expected to arrive. After the time window is over, localizer B processes the reception data to determine the actual time of arrival of the first communication. The processing time at localizer B is on the order of a millisecond. A prearranged delay time after the actual arrival time of the first communication, the delay time being greater than the processing time, localizer B sends a second communication back to localizer A. Localizer A listens for the second communication during a reception time window centered around an estimate of when the second communication should be received. After the reception time window is over, localizer A processes the reception data to determine the arrival time of the second communication. Knowing the time at which the first communication was sent, the time at which the second communication was received, and the agreed upon delay between when localizer B received the first communication and sent the second communication, and having an estimate of the relative clock rate of localizer B, localizer A can calculate the distance between the localizers. A disadvantage of this method is that the actual time for the propagation of the electromagnetic radio communications between the localizers is small compared to the delay time at localizer B and the time difference between transmission and reception at localizer A. The delay time is on the order of a millisecond and the signal propagation time is on

the order of 100 nanoseconds. In this protocol large times must be subtracted to determine a small time, so the calculation is sensitive to inaccuracies in the clocks of localizers A and B.

In a modification of the above method, which increases the accuracy of the estimate of the distance but still suffers from the sensitivity to inaccuracies of the clocks, the localizers perform a second series of ranging communications a prearranged time after the first series of ranging communications. In the second series of ranging communications the center times of the reception windows are adjusted according to the offsets of the reception times from the centers of the reception windows in the first series of communications, so that the transmissions in the second series of communications arrive closer to the center of the reception windows. When the localizers can position the peak in the center of a bin near the center of the reception, this indicates the localizers have achieved the goal of accurately determining the separation distance. Since, as discussed below, features of the DTPAC function $\Lambda(n)$, including the central peak and the peaks in the "wings" of the function, provide information about the time of arrival of a communication, positioning the time of arrival of a communication in the center of a bin near the center of the reception windows increases the accuracy of the estimate of the time of arrival.

To circumvent this disadvantage of the first ranging protocol (and its modification discussed above), a second ranging protocol, shown in FIG. 4, uses a much shorter delay at localizer B. In the second ranging protocol localizer A sends a first ranging communication to localizer B at a prearranged time. Localizer B listens for the first communication during a time window centered around the time the first communication is expected to arrive. After the time window is over, but before processing the reception data to determine when the first communication arrived at localizer B, localizer B sends a second communication back to localizer A a prearranged delay time after the center of localizer B's reception time window. Localizer A listens for the second communication during a reception time window centered around an estimate of when the second communication should be received. Only after the transmission of the second communication does localizer B process the reception data to determine the actual time of arrival of the first communication. After the reception time window of localizer A is over, localizer A processes the reception data to determine the arrival time of the second communication. After localizer B determines the actual reception time of the first communication, localizer B sends a series of correction bits to localizer A. The correction bits communicate the time difference between the actual reception time of the first communication at localizer B and the center of localizer B's reception time window. Knowing the time at which the first communication was sent, the time at which the second communication was received, the agreed upon time delay between the center of localizer B's reception time window and transmission time window, and the correction time between the center of the reception time window and when the first communication was received at localizer B, and having an estimate of the relative clock rate of localizer B, localizer A can calculate the distance between the localizers. Because localizer B sends a signal back to localizer A before processing to determine the actual arrival time of the first communication, the delay time can be much shorter than that of the first protocol, and the accuracy of the calculation is much less sensitive than the first protocol to the inaccuracies of the clock rates of the localizers.

In a modification of the above method, which further increases the accuracy of the estimate of the distance, the

localizers perform a second series of ranging communications at a prearranged time difference from the first series of ranging communications. In the second series of ranging communications the transmission time at localizer A are adjusted according to the offsets of the reception times from the centers of the reception windows in the first series of communications, so that the transmissions in the second series of communications arrive closer to the center of the reception windows. When the localizers can position the peak in the center of a bin near the center of the reception, this indicates the localizers have achieved the goal of accurately determining the separation distance. Since, as discussed below, features of the DTPAC function $\Lambda(n)$, including the central peak and the peaks in the “wings” of the function, provide information about the time of arrival of a communication, positioning the time of arrival of a communication in the center of a bin near the center of the reception windows increases the accuracy of the estimate of the time of arrival.

A third possible ranging protocol shown in FIG. 7a uses a similar approach to the second protocol, but involves a second round-trip communication from localizer B to localizer A and back to localizer B, before localizer B sends a series of correction bits to localizer A. In particular, in the third ranging protocol, localizer A sends a first ranging communication to localizer B at a prearranged time. Localizer B listens for the first communication during a time window centered around the time the first communication is expected to arrive. After the time window is over, but before processing the reception data to determine when the first communication arrived at localizer B, localizer B sends a second communication back to localizer A a prearranged delay time after the center of localizer B’s reception time window. Localizer A listens for the second communication during a reception time window centered around an estimate of when the second communication should be received. After the transmission of the second communication, localizer B processes the reception data to determine the actual time of arrival of the first communication. After the reception time window at localizer A, localizer A processes the reception data to determine the arrival time of the second communication. Then, the roles of localizers A and B in first round of communications are reversed for a second round of communications. Localizer B sends a third ranging communication to localizer A at a prearranged time. Localizer A listens for the third communication during a time window centered around the time the third communication is expected to arrive. After the reception time window is over, but before processing the reception data to determine when the third communication arrived at localizer A, localizer A sends a fourth communication back to localizer B a prearranged delay time after the center of localizer A’s reception time window. Localizer B listens for the fourth communication during a reception time window centered around an estimate of when the fourth communication should be received. After the transmission of the fourth communication, localizer A processes the reception data to determine the actual time of arrival of the third communication. After the reception time window at localizer B, localizer B processes the reception data to determine the arrival time of the fourth communication. After localizer B determines the actual reception time of the fourth communication, localizer B sends a series of correction bits to localizer A. The correction bits communicate the time difference between the actual reception time of the first communication at localizer B and the center of localizer B’s first reception time window, and the time between the

transmission of the third communication and the reception of the fourth communication at localizer B. Knowing the round trip times for the first pair of communications and the second pair of communications, and the prearranged delay times at localizers B and A respectively, localizer A can calculate both the distance between the localizers, and the ratio of the clock rates of the localizers. Because the localizers send signals back to each other in the first pair of communications and the second pair of the communications before processing to determine the actual arrival time of the communications, the delay times are much shorter than in the first method, and the accuracy of the calculation is much less sensitive to the accuracies of the clock rates of the localizers. After localizer B sends the correction bits to localizer A, localizer A may send its results for the separation distance and the ratio of the clock rates explicitly to localizer B. Alternatively, localizer A could send a set of correction bits to localizer B representing the round trip time for the first pair of communications, and the time difference between the center of the reception window and the time of arrival of the third communication at localizer A, so that localizer B may also calculate the separation distance and the ratio of the clock rates. In another alternative of this method the second and third communications from localizer B could be replaced with a single communication, i.e., the time between the second and third communications is effectively reduced to zero. Localizer B would then have to determine the arrival time of the first communication after receiving both the first and third communications from localizer A.

These ranging methods may also be adapted to an iterative procedure where, rather than sending the actual values of time delays between localizers, a localizer only communicates one bit of data per round of communications. This one bit of data could represent the side of a reception window in which a previous communication arrived. For instance, localizer A could send a first communication to localizer B, and localizer B would respond with a second communication back to localizer A after a prearranged time delay which is much shorter than the time it takes for localizer B to determine the actual arrival time of the communication from localizer A. After localizer B responds to localizer A, it would then determine the actual arrival time of the first communication from localizer A. Localizer A would then send a third communication to localizer B after a prearranged wait, and localizer B would again respond with a fourth communication to localizer A after the prearranged time delay. If the first communication arrived in the earlier half of localizer B’s reception window, localizer B’s fourth communication would have a first polarity, and if the first communication arrived in the later half of the reception window, the fourth communication would have a second polarity. (“Polarization” refers to the plane of the electric field in a plane-polarized electromagnetic transmission, and “polarity” refers to the direction of the electric field in the plane of polarization. In other words, the polarization may be controlled by the orientation of the antenna, and the polarity may be controlled by the direction of current through the antenna.) Localizer A would then modify the transmission time of its next communication (the fifth communication) based on the information conveyed from localizer B in the fourth communication by a first amount so that its communication would arrive nearer the center of localizer B’s reception window than previously. Localizer A would also modify the central time of its reception window so that the next communication from localizer B (the sixth communication) would arrive nearer the center of localizer

A's reception window. Similarly, localizer B's next communication (the sixth communication) would reflect the arrival time of the third communication (from localizer A), and localizer A would modify the transmission and reception times of the next pair of communications (the seventh and eighth communications) based on this information by a second amount which is half as large as the first amount. The size of the time corrections made by localizer A decrease by a factor of two in each pair of the communications, and the arrival times of the communications converge rapidly on the centers of the reception windows. Knowing the prearranged delay time at localizer B and the time between a transmission and a reception at localizer A, localizer A may then determine the separation between the localizers.

It may also be desirable to provide protocols where a localizer can determine the locations of other localizers while not divulging its own location. A first localizer may hide its location by offsetting its communications with other localizers with time delays of random sign and magnitude. In this case, it will be apparent to the other localizers that the first localizer is not divulging its location. Alternatively, the first localizer may offset its communications in a controlled manner so that other localizers would determine an incorrect location for the first localizer. For instance in a modification of the third ranging protocol of FIG. 7a, localizer A sends a first communication to localizer B, and after a prearranged delay time localizer B sends a second communication back to localizer A. Then localizer B determines the exact arrival time of the communication from localizer A. Next, after a prearranged waiting time, localizer B sends a third communication to localizer A. Although localizers A and B have agreed on a delay time between receiving and sending communications, localizer A does not hold to this arrangement. Instead, localizer A purposefully modifies the delay time before sending its response (the fourth communication) so that localizer B receives a false impression of the separation distance. Similar modifications of the first ranging protocol of FIG. 2 or the second ranging protocol of FIG. 4 may also be implemented to preserve the location privacy of a localizer.

All of the protocols above require that at least one of the localizers has a first approximation of the distance. Once a distance estimate has been obtained, localizers can use any of the ranging methods described above to update their estimates of the distance and the ratios of the clock rates. To obtain an initial estimate of the separation distance and the ratio of clock rates, the localizers may start out in electrical contact.

In an alternate synchronization protocol not requiring electrical contact, localizer B attempts to initiate contact with other localizers by transmitting a beacon signal on a regular periodic basis. To find this beacon, localizer A must do an exhaustive search of the time period until the beacon is detected. This search could be on the order of 5 to 10 seconds. When localizer A finds the beacon, it begins broadcasting a reply. Localizer B could in turn do an exhaustive search looking for a response from localizer A, doubling the length of time necessary to get into synchronization.

The time for localizer B to do the search could be drastically reduced if localizer A broadcasts the reply at a known time delay after receiving each beacon. Localizer B would only have to search a small time period after the beacon for the reply. This allows localizer B to rapidly find nearby localizers, and to simultaneously acquire an approximate distance to them. Alternately, localizer B could continuously attempt to receive a communication from localizer

A at a small fixed time delay before each beacon. Then localizer A would have to do the fast search backwards from the beacon to find the approximate distance to localizer B. In this case localizer A would acquire an approximate distance. In either case, the localizers indicate the beginning of communication by modifying the beacon or reply communication. Once in synchronization, the localizers can begin to exchange digital messages, requests, and start doing ranging protocols as described above.

Overview of the Hardware

Since electromagnetic radiation travels 1 cm in only about 33 picoseconds, a clock with a period of about 33 picoseconds, i.e., a 30 GHz clock, is required to measure distances as small as 1 cm by measuring the time of propagation of radio waves by counting clock pulses. If this clock was also required to measure times on the order of one day, 2.6×10^{15} of these 30 GHz pulses would have to be counted, requiring a 52-bit counter.

Unfortunately, CMOS logic cannot operate in the tens of gigahertz, though a clock as high as 200 MHz is practicable. (A 200 MHz clock has a period of 5 nanoseconds and can resolve distances down to 1.5 meters.) Therefore, in a first embodiment **2410** shown in FIG. 24a, pulses from a 200 MHz clock **2412** are placed to a resolution of 30 picoseconds by delaying the clock pulses through a programmable delay generator **2050** in stage "S0" of the clock. The delay generator **2050** must select between one of about 150 different delay times, requiring eight bits of binary storage. The remaining 48 bits required for the counter of the clock **2410** are located in a stage S1 counter **2414**. This clock **2410** has the drawback that all 48 bits of the stage S1 counter **2414** must use low-noise circuitry so the S1 counter **2414** can run without producing power line noise and electromagnetic noise during reception and transmission events.

In actuality, the 200 MHz clock **2412** is problematic since it has a high power consumption and produces significant power line noise. So in a second embodiment **2420** shown in FIG. 24b a stage S1 phase-lock loop (PLL) circuit **2010/2020/2030** is used to increase the speed of a readily available crystal oscillator **130** with a frequency of an approximately 6.25 MHz clock to the 200 MHz required. The PLL circuit **2010/2020/2030** has a 5-bit counter to divide the 200 MHz pulses down to phase lock to the 6.25 MHz clock pulses. The output from the 6.25 MHz clock oscillator **130** is also counted by a 43-bit stage S2 counter **2422**. Since the 6.25 MHz crystal oscillator **130** produces many clock pulses during a reception event, the S2 counter **2422** must use low-noise circuitry.

Since the most-significant bits of the S2 counter **2422** do not change very often, a portion of the S2 counter **2422** can be separated into stage S3 counter **2434** implemented in software in a processor **140**, as shown in the third embodiment **2430** depicted in FIG. 24c. This allows the total number bits in the clock **2420** to be arbitrarily large so that periods longer than a day can be counted. The number of bits remaining in the stage S2 counter **2432** should be large enough that the processor **140** does not get interrupted more frequently than it can handle, or during transmission or reception events when only low-noise circuitry can operate. In a preferred embodiment the processor **140** receives an interrupt every 100 microseconds, so the S2 stage **2432** has a 14-bit counter, and the counter in the processor **140** handles the remaining 29 bits. In the preferred embodiment even more bits are implemented in the software counter in the processor **140**, since this is not difficult and allows the processor **140** to schedule events in human time scales such as days and months.

In a fourth embodiment **2440** depicted in FIG. **24d**, the stage **S2** counter **2432** of FIG. **24c** becomes a counter **2442** having two stages, CMOS stage **S3** and low-noise stage **S2**. As before, the crystal oscillator **130** provides a clock with a frequency of approximately 6.25 MHz, the stage **S1** PLL circuit **2010/2020/2030** produces a clock signal of approximately 200 MHz from the 6.25 MHz signal, and the programmable delay unit **2050** provides delays with a placement of 30 picoseconds. The **S3** portion of the counter **2442** counts bits that change infrequently during a single reception or transmission event, and therefore can be implemented in standard CMOS logic. The **S2** stage of the counter **2442**, as well as the **S1** and **S0** stages, count bits which change value during transmission and reception events, and must be implemented in low-noise logic to prevent the production of power supply noise and electromagnetic noise. In the preferred embodiment the chip length is approximately 10 nanoseconds and the number of chips in a code sequence is around **1024**, so the time for one reception event is about 10 microseconds. This requires that the **S2** stage has a 6-bit counter, and the **S3** stage has an 8-bit counter. To allow for longer codes, the **S2** and **S3** stages could both have 8-bit counters.

In a fifth embodiment shown as a block diagram in FIG. **24e**, the **S2** stage uses both low-noise circuitry in a low-noise **S2B** stage and standard logic in a CMOS **S2A** stage. The **S2** clock is only required to use the low-noise **S2B** stage during reception and transmission events, and can use the CMOS **S2A** stage otherwise to conserve power. As before, the crystal oscillator **130** provides a clock with a frequency of approximately 6.25 MHz, the stage **S1** PLL circuit **2010/2020/2030** produces a clock signal of approximately 200 MHz from the 6.25 MHz signal, the programmable delay unit **2050** provides delays with a placement of 30 picoseconds, the processor **140** maintains a count of the most-significant digits of the time, and the low-frequency clock **119** is separated into a CMOS **S3** stage and an **S2** stage.

In summary, the number of stages in which the clock is divided is a function of the power requirements. For instance, if power consumption is not an issue, the **S2** and **S3** counters of the low-frequency clock **119** of the preferred embodiment **100** of FIG. **24e** could be combined and use low-noise circuitry. If power consumption is to be minimized, the timebase has a counter for the most-significant bits in the processor **140**, the low-frequency clock **119** has a CMOS **S3** stage for the next most-significant bits and the **S2** stage for the next most-significant bits is separated into a low-noise **S2B** stage which is active during transmission and reception events and a CMOS **S2A** stage which is active between transmission and reception events. The detailed description below corresponds to the preferred embodiment of FIG. **24e** which is designed to minimize power consumption.

The timebase of the transceivers measures time differences used to calculate locations, and acts as an alarm clock to trigger transmissions and listening periods for receptions. As discussed above, the time base of a localizer of the preferred embodiment is divided into five stages of clocks, the stages being numbered from zero to four in order of increasingly large time graduations between clock ticks (a clock tick is the time between rising edges of a clock signal). The fourth, third and second stages are considered to compose the low-frequency clock. The second stage counts clock impulses directly from a crystal oscillator. The first stage counts clock impulses from a phase-lock loop circuit which increases the frequency of the crystal oscillator clock,

and the zeroth stage is a programmable delay which provides timing control to an accuracy of 30 picoseconds. The first and zeroth stages are considered to compose the high-frequency clock. Between transmissions when low power consumption is required, only the fourth stage, the third stage and a lower-power-consumption portion of the second stage are active. During transmissions when highly accurate time keeping and low-noise emissions are required, the zeroth stage, first stage, and a low-noise portion of the second stage are active. The timebase is designed to insure that in the switching between the low-frequency clock and the high-frequency clock no clock impulses are lost and there is no phase error.

The first, third and fourth stages each have a single counter, while the second stage has two counters: a low-noise counter which operates during transmission and reception, and a low-power standard-circuitry counter which operates between localizer communications. The system is designed so that any transmission or reception impulse sequence is shorter than the time required for the second-stage counters to count from zero to a terminal count. At the terminal count of the second-stage standard-circuitry counter immediately prior to a transmission or reception time window, the second-stage low-noise counter will be activated and the second-stage standard-circuitry counter will be inactivated. The second-stage low-noise counter continues counting until it reaches its terminal count, and at that point there is a check as to whether the transmission or reception time window is over. If the system is still receiving or transmitting, the second-stage low-noise counter will count again to its terminal count, at which point the transmission or reception will be complete and the second-stage standard-circuitry counter will be activated and the second-stage low-noise counter will be inactivated.

When the counter of the first stage reaches its terminal count it resets to zero and at approximately the same time the 6.25 MHz clock causes the counter in the second stage to be incremented by one. When either of the counters of the second stage reaches its terminal count it resets to zero and increments the counter of the third stage by one, and when the counter of the third stage reaches its terminal count it resets to zero and increments the counter of the fourth stage by one. In other words, the counter in the first stage holds a set of least-significant (highest-frequency) clock bits, the counter in the fourth stage holds a set of most-significant (lowest-frequency) clock bits, and the counters in the second and third stages hold clock bits of intermediate significance. Therefore, a triggering clock time C is a concatenation of bit segments, i.e., $C=(C_4, C_3, C_2, C_1, C_0)$, where C_n is the count of the n th stage ($n=1, 2, 3$ and 4) and C_0 is the delay generated by the zeroth stage.

The first, second and third stages each have a transmitter event register, a transmitter event comparator, a receiver event register and a receiver event trigger. (The receiver and transmitter sections of the stages work in exactly the same manner, except where otherwise noted, so the discussion of the receiver section which follows may also be applied to the transmitter section.) To trigger a reception event, bit segments corresponding to the triggering time are loaded in event registers in stages one through three, and a delay is selected for the programmable delay of stage zero. This is referred to as "arming" the event registers. When a comparator determines that there is a correspondence between the event register value and the counter value of that stage a "triggering" of the comparator occurs and it enables the comparator of the next stage (the stage having the next finer time graduations). If a transmission is to occur at a time (C_4 ,

C_3, C_2, C_1, C_0), event registers in the third, second and first stages are armed with the values $C_3-1, C_2-1,$ and $C_1-1,$ respectively. Arming the event registers with the values $C_3-1, C_2-1,$ and $C_1-1,$ rather than $C_3, C_2,$ and $C_1,$ makes the circuit design less demanding by providing additional time for events associated with triggering to occur. When the counter in the third stage reaches the value $C_3-1,$ the comparator in the third stage triggers, and enables the comparator in the second stage. At this point the low-noise components of the second stage are activated and the standard-circuitry components of the second stage are deactivated. Similarly, when the second-stage counter reaches the value $C_2-1,$ the second-stage comparator enables the first-stage comparator, and the low-noise components of the first stage are also activated. When the first-stage comparator determines that the count in the first-stage counter is equal to $C_1-1,$ on the next increment of the first-stage counter the high-frequency clock impulses from the first stage are sent to the programmable delay where they are delayed by $C_0.$ For reception events the high-frequency clock impulses from stage zero are directed to a pseudorandom sequence generator and a time-integrating correlator. For transmission events the high-frequency clock impulses are directed to a transmitter code-sequence generator and a transmitter antenna driver.

The time offsets at which values of the discrete-time pseudo-autocorrelation (DTPAC) function are determined are referred to as the "time bins." The time bins are located at times $(t_0+n \Delta t),$ where t_0 is the time of the central time bin, n is an integer (between negative fifteen and positive sixteen in the preferred embodiment), and Δt is the time difference between neighboring bins. The correlator circuit has an integrator for each time bin. The internally-generated integration sequence $\Phi_i(t)$ may be produced by a linear feedback shift register (and associated circuitry) and delayed by shifting it through a series of flip-flops. (It should be noted that the delay of the analog antenna signal rather than the digital impulse sequence signal would require using an analog delay means such as a surface acoustic wave delay, or lengths of coaxial cable or optical fiber, and would therefore not be compatible with the above-mentioned size and technology requirements of the transceivers.) The flip-flops provide taps for the integrators, and each of the integrators calculates the integral of the product of a delayed integration sequence $\Phi_i(t-t_0-n\Delta t)$ and the received signal $\Phi_c(t),$ so that the value at the n th bin is

$$\Lambda(n) = \int_{\text{mod } \delta t}^{\tau} \int_{\text{mod } \delta t}^{\tau-t-t_0-n\Delta t} \Phi_i(t) \Phi_c(t) dt$$

The time bin which delays the integration sequence $\Phi_i(t)$ so that it overlaps most closely with the received signal $\Phi_c(t)$ is termed the "peak" time bin since it produces the maximum value in the DTPAC function $\Lambda(n).$

In each integrator the product of a delayed internally-generated integration sequence $\Phi_i(t)$ and the received differential voltage signal $\Phi_c(t)$ from the antenna is produced by directly applying the received voltage to the input of a transconductance amplifier when the value of the integration sequence $\Phi_i(t)$ is positive unity, and inverting the polarity of the antenna voltage to the input of the transconductance amplifier when the value of the integration sequence $\Phi_i(t)$ is negative unity. When the delayed integration sequence $\Phi_i(t)$ has a value of zero (prior to the beginning of the sequence, and subsequent to the end of the sequence) the differential inputs to the transconductance amplifier are shorted. The transconductance amplifier provides a very rapid response time since it takes advantage of the natural mode of field

effect transistors, namely the conversion of input voltages to output currents, and does not utilize negative feedback, as do op-amps. However, since the response of the transconductance amplifier is rapid the output impedance of the transconductance amplifier is not large, and the voltage on a capacitor connected across the output of the transconductance amplifier decays ("drips") with a characteristic time on the order of milliseconds (which, as mentioned above, is on the order of the time it takes to calculate the arrival time of an impulse sequence). Therefore, the output of the transconductance amplifier is directed to a switched-capacitor sample-and-hold circuit, i.e., the capacitor across the amplifier output is partially discharged across sampling capacitors, the sampling capacitors are disconnected from the output capacitor, and the voltage across the sampling capacitors is then sampled by a differential amplifier which has a large input impedance. The switched-capacitor sample-and-hold circuit provides a droop time on the order of seconds. However, if the droop time is slow relative to the time required for conversion from analog to digital, a sample-and-hold circuit may not be needed.

In the preferred embodiment, impulse sequences are transmitted and received using a loop antenna. As disclosed in U.S. Pat. No. 4,506,267 issued to Henning F. Harmuth, current-mode loop antennas are well suited to NSS transmissions since their operation is not based on an electromagnetic resonance in the antenna. The far field components of the radiated electric and magnetic fields vary as the product of the length of a single unshielded arm of the loop and the time derivative of the current. Therefore, a device which uses a loop antenna can be made very small since the relatively lower power transmitted by a smaller antenna can be compensated for by producing a larger current derivative. In contrast with the disclosures of Harmuth, it has been found that it is not necessary to shield the loop antenna for it to transmit effectively.

An alternate preferred embodiment of the present invention uses a bi-loop antenna consisting of a substantially square radiating plate with a first pair of leads connected across one pair of opposite sides of the plate, and a second pair of leads connected across the other pair of opposite sides of the plate. Currents across the first pair of leads generate electromagnetic waves with a first electric field polarization, and currents across the second pair of leads generate electromagnetic waves with a second electric field polarization orthogonal to the first. Using the bi-loop antenna, transmissions along both axes can be produced, and the amount of information communicated between localizers can be increased. Another advantage of the bi-loop antenna is that the angular orientation of the plate about its normal vector is irrelevant, the plate need only face the incoming radiation to provide reception when the polarization of the incoming radiation is unknown.

With single-loop transmission and reception antennas there are orientations where the polarization of a transmitted signal is orthogonal to the reception antenna and the signal cannot be detected. However, it should be noted that if both the transmission and reception antennas are bi-loop antennas, it is always possible to communicate between the antennas regardless of their relative position and orientation.

Driving the antenna are a plurality of H-bridge switches, each H-bridge switch being connected to a cascade of pairs of staged-gain CMOS buffers. The cascade allows a large switching current to be developed, ensuring a rapid switching time. Variable delay units are placed at the beginning of each cascade to correct for any inadvertent differences in the

delays of the cascades. The variable delay units can also be used to control the shapes of the transmitted impulses. By varying the number of operating H-bridges, the current, and therefore the power, to the antenna may be controlled to compensate for the distance between localizers.

An H-bridge is a switch configuration which allows the voltage across either lead to be switched from high to low, or low to high, while never creating an open circuit while current is flowing. A current pulse through the antenna generates two electromagnetic impulses—the first electromagnetic impulse corresponding to the beginning of the current pulse has a first polarization, and the second electromagnetic impulse corresponding to the end of the current pulse has an opposite polarization. Terminating current pulses through the antenna by returning both leads to high, both leads to low, or alternating both leads high and both leads low, allows the shapes, and therefore the spectra, of transmitted impulses to be controlled. In the preferred embodiment, all the switches in the H-bridge are opened when the antenna is not in use.

SUMMARY OF THE INVENTION

The present invention is directed to a transceiver for nonsinusoidal spread spectrum (NSS) radio communications. During a time window in which a signal is expected to be received, a code-sequence generator produces an integration sequence which is directed to a correlator circuit. The correlator circuit calculates integrals of the product of the received signal and delayed integration sequences to produce a correlation function. After the time window, a processor determines the time of arrival of the received signal from the correlation function.

The present invention is also directed to a method for determining the distance between a pair of radio transceivers. A first transceiver emits a first communication signal at a prearranged time. The second transceiver emits a second communication signal after a prearranged delay time from the time it expects to receive the first communication signal. After transmitting the second communication signal the second transceiver determines the time it received the first communication signal. After receiving the second communication signal the first transceiver determines the time it received that signal. The two transceivers then determine the distance therebetween based on the transmission and arrival times.

It is therefore an object of the present invention to provide a system of transceivers ("localizers") which can accurately determine their relative positions.

Further objects of the present invention are to provide localizers that are small, inexpensive and have low power consumption, particularly localizers that can be battery powered.

It is another object of the present invention to provide localizers which can operate without a clear view of the sky.

It is another object of the present invention to provide a system of localizers which do not include planetary satellites.

It is another object of the present invention to provide localizers which use nonsinusoidal spread spectrum (NSS) radio transmissions.

It is another object of the present invention to provide localizers which use low-noise logic during transmission and/or reception to increase the signal-to-noise ratio.

It is another object of the present invention to provide a very stable real-time clock counter with low power

consumption, low-noise emissions during reception and transmission, a wide dynamic range and high resolution.

It is another object of the present invention to provide a very stable low-noise high-frequency clock which substitutes for a standard-circuitry low-frequency clock during transmission and/or reception with no loss of phase or clock impulses.

It is another object of the present invention to provide a highly stable and accurate timebase for a system of communicating units generated from a small number of highly accurate clocks or accurately known distances between units, where the majority of the units have low-accuracy clocks.

It is another object of the present invention to provide ranging protocols which determine the separation distances and relative clock rates of localizers, including iterative converging protocols.

It is another object of the present invention to provide protocols for initiating communications between localizers.

It is another object of the present invention to provide antennas compatible with NSS transmissions and receptions.

It is another object of the present invention to provide an NSS antenna which can transmit electromagnetic waves with multiple polarizations.

It is another object of the present invention to provide an antenna which is relatively insensitive to its orientation with respect to incoming NSS radiation.

It is another object of the present invention to provide means for rapid switching of large currents through an NSS antenna.

It is another object of the present invention to provide circuitry for calculating the correlation between extremely rapidly varying signals, particularly the cross-correlation of a received analog signal and an internally-generated digital version of the analog signal.

It is another object of the present invention to determine the location of the maximum of the correlation function between a received analog signal and an internally-generated digital version of the analog signal, by integrating the received analog signal and versions of the internally-generated signal delayed by a number of time offsets.

It is another object of the present invention to provide circuitry for calculating the integral of an extremely rapidly varying analog signal, particularly that of an analog signal formed by the product of an analog signal and a digital signal having values of positive unity, negative unity and zero.

It is another object of the present invention to provide a chip function which causes the pattern of values in the correlation time bins to vary strongly with small time shifts of the received input waveform, i.e., which causes the shape of a pseudo-autocorrelation function examined at a series of discrete time intervals to vary strongly with small shifts of the arrival time of the received input waveform.

It is another object of the present invention to provide internally-generated chip waveforms and time bin locations useful in determining the exact arrival time of an NSS communication over a large span of time, locating the approximate arrival time of an NSS communication, and/or increasing the signal-to-noise ratio.

In addition, other objects, features and advantages of the present invention will become apparent from the following detailed description when taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 shows a schematic diagram of the circuitry of a localizer according to the present invention.

FIG. 2 diagrams a method for cooperative ranging between two localizers.

FIG. 3 is a flow chart depicting an iterative ranging method based on the method depicted in FIG. 2.

FIG. 4 diagrams a method for cooperative ranging between two localizers which is more accurate than the method depicted in FIG. 2.

FIG. 5 is a flow chart depicting an iterative ranging method based on the method depicted in FIG. 4.

FIG. 6 is a flow chart depicting another iterative ranging method based on the method depicted in FIG. 4.

FIG. 7a diagrams a method for cooperative ranging which allows for determination of the separation distance and the ratio of the clock rates of two localizers.

FIG. 7b diagrams a modification of the method for cooperative ranging of FIG. 7a, where a single communication is substituted for the second and third communications of FIG. 7a.

FIG. 8 is a flow chart depicting a method for two localizers to initiate communications.

FIG. 9 diagrams a method for cooperative ranging communications where one localizer provides false information about its location.

FIG. 10 shows a set of waveforms and the absolute value of corresponding Fourier spectra.

FIG. 11 illustrates that the discrete pseudo-autocorrelation (DTFAC) function is equal to the product of a received signal $\Phi_c(t)$ and an internally-generated integration signal $\Phi_i(t)$.

FIG. 12 shows five pairs of graphs illustrating the relationship between a discrete-time pseudo-autocorrelation function $\Lambda(n)$ and time samplings of the analog pseudo-autocorrelation function $\Lambda(t)$, and illustrating the dependence of the shape of the discrete-time pseudo-autocorrelation function $\Lambda(n)$ on shifts in the bin times.

FIG. 13 shows five pairs of graphs illustrating the relationship between a discrete-time pseudo-autocorrelation function $\Lambda(n)$ and a time sampling of the analog pseudo-autocorrelation function $\Lambda(t)$, and illustrating the dependence of the shape of the discrete-time pseudo-autocorrelation function $\Lambda(n)$ on shifts in the bin times, the bin times of FIG. 13 being shifted by smaller amounts than the shifts of FIG. 12.

FIGS. 14a, 14b and 14c show several possible integration sequences $\Phi_i(t)$ and bin times Δt .

FIG. 15 is a schematic diagram of a low-frequency clock portion of the timebase circuitry of a localizer.

FIG. 16 is a schematic diagram of a high-frequency clock portion of the timebase circuitry of a localizer.

FIG. 17a is a schematic diagram of a receiver code-sequence generator of a localizer.

FIG. 17b is a timing diagram of signals in the receiver code-sequence generator of FIG. 17a.

FIG. 18 is a schematic diagram of a time-integrating correlator for providing the discrete-time pseudo-autocorrelation function $\Lambda(n)$.

FIG. 19 is a schematic diagram of one of the integrator circuits used in the time integrating correlator.

FIG. 20 is a timing chart for signals in the integrator circuit.

FIG. 21a is a schematic diagram of a transmitter code-sequence generator. FIGS. 21b–21e show timing charts for the transmitter code-sequence generator for four possible resting state register values.

FIG. 22 is a schematic diagram of a transmitter antenna driver.

FIGS. 23a, 23c and 23e are perspective views of three embodiments of antenna/circuitry systems according to the present invention. FIGS. 23b and 23d are views of metal sheets which may be folded to provide the antennas of FIGS. 23a and 23c, respectively, and FIG. 23f is a front view of the system of FIG. 23e.

FIGS. 24a–24e show five embodiments of a timebase for providing an extremely fast clock with an extended range. The fifth embodiment shown in FIG. 24e corresponds to the preferred embodiment described in detail below.

GLOSSARY

The following symbols are used in the present specification:

α, β	dummy variables for letters
$\gamma(t)$	chip waveform
$\gamma_i(t)$	internally-generated chip waveform
$\gamma_e(t)$	received chip waveform
Δt	delay time between time bins
δt	time length of a chip
θ	phase of a sinusoidal carrier
$\Lambda(n)$	value of discrete-time pseudo-autocorrelation function at the nth bin
$\Lambda(t)$	pseudo-autocorrelation function
ω	angular frequency of a sinusoidal carrier
$\sigma(i)$	pseudorandom code sequence
$\sigma^*(i)$	data modulated pseudorandom code sequence
τ	dummy variable for time
$\Phi(t)$	pseudorandom chip sequence
$\Phi_i(t)$	internally-generated pseudorandom integration sequence
$\Phi_i^{(n)}(t)$	delayed internally-generated pseudorandom integration sequence directed to the n^{th} integrator circuit
$\Phi_e(t)$	transmitted or received chip sequence
$\psi(t)$	communication consisting of a string of pseudorandom sequences $\Phi(t)$
$a(t)$	received or transmitted signal
A, B, D	reference letters for particular localizers
c	speed of light
Code0	low-order bit of two-bit reception command sequence
Code1	high-order bit of a two-bit reception command sequence
C_n	count of the nth clock stage
f	frequency of a sinusoidal carrier ($2\pi\omega$)
G(t)	waveform of a Gaussian impulse
g	shift factor for spacing between bins
h	width factor for pulses in $\gamma_i(t)$
i, n	dummy variables for integers
k_A, k_B	ratio of actual time to clock time for localizers A and B
L	number of chips in a pseudorandom sequence $\Phi(t)$
M	number of pseudorandom sequences $\Phi(t)$ in a communication $\psi(t)$
N	number of integrators in the time-integrating correlator
R_A, R_B	time for round trip communication $A \rightarrow B \rightarrow A$ and $B \rightarrow A \rightarrow B$
t	time
t_0	time of central time bin
t_c	time between ticks of the system clock
t_m	time of peak of Gaussian impulse
t_s	time length of a chip sequence ($=L\delta t$)
ΔT_c	delay time between ranging communications and the transmission of correction bits
ΔT_d	turnaround time between reception and transmission of communications
ΔT_e	time difference between expected and

-continued

	actual arrival times of a communication
ΔT_r	time delay between beacon and reception window
ΔT_s	spoofing time delay
ΔT_x	shift in transmission time T_1
$\Delta T_x(\min)$	minimum shift in transmission time T_1
ΔT_w	length of reception time window ($=N\delta t$)
T_1, T_2, T_3, \dots	central times of reception Windows or beginning times of transmissions
T_{2a}, T_{4a}	arrival times of communications
X	distance between localizers
$X(n)$	nth estimate of distance between localizers

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Detail Overview of Transceiver Circuitry

A schematic of a localizer circuit **100** according to the present invention is shown in FIG. **1** In all the figures, including FIG. **1**, components which utilize low-noise circuitry are shown in shadowed boxes. Such low-noise components include a time-integrating correlator **114**, a low-frequency real time clock **119**, a high-frequency real time clock **120**, a receiver code-sequence generator **117**, a transmitter code-sequence generator **118**, and miscellaneous logic **150**. The miscellaneous logic **150** must operate during transmission and reception and cannot be delegated to a standard-logic processor **140**. The only components which are composed entirely of standard-logic circuitry are the processor and memory unit **140**. Many components are analog in nature, and have no digital logic that produces power supply switching noise or electromagnetic noise. Analog components include: a differential amplifier **105**, a digital-to-analog (D/A) converter **106**, and an analog-to-digital (A/D) converter **107**, and the crystal oscillator **130**. The D/A converter **106** and A/D converter **107** have a logic back end, but this can be constructed of standard-logic since they are only used between reception events. The transmitter antenna driver **116** does not need to use low noise logic, since it only operates when the transmission antenna **101** is generating large noise-like signals. Reception and transmission antennas **102** and **101** are specifically designed to be used for nonsinusoidal spread-spectrum radio communications.

The time base of the circuit **100** is based on a crystal oscillator **130** which, in the preferred embodiment, generates an approximately 6.25 MHz crystal clock signal XClock on crystal clock output line **148**. the crystal clock signal XClock is directed to the XtalClock inputs of the low-frequency and high-frequency real time clocks **119** and **120**. The high-frequency clock **120** is activated only for transmission and reception events to provide additional precision to the time-base. When the counters in the low-frequency clock **119** reach their maxim value a rollover bit is sent from the Rollover output to the Interrupt input of the processor **140** via line **154** to increment a counter in the processor **140**, and the counter in the low-frequency clock **119** resets to zero and continues counting.

The low-frequency clock **119** operates both during and between communications. Since low-noise circuitry uses more power than standard logic circuitry, in applications that must run for long time periods on small portable batteries, the low-frequency clock **119** may be divided into stages that run on standard logic between communications and low-

noise logic during communications. However, when adequate power is available, for example in a permanent installation, the low-frequency clock **119** could be designed using entirely low-noise circuitry. A low-power low-frequency clock **119** is presented as the preferred embodiment in the following discussion. The low-power low-frequency clock **119** has a CMOS-logic stage, termed the "S3 stage," which only operates between communications, since the operation of CMOS logic produces power line noise and electromagnetic radiation which may interfere with communications. The preferred embodiment low-frequency clock **119** also has a stage with a combination of standard and low-noise circuitry, termed the "S2 stage," which holds time bits of less significance than a counter in the S3 stage, and each rollover of the S2 counter increments the S3 counter. The S2 stage switches from operation with the standard circuitry to the low-noise circuitry on the rollover of a standard-circuitry S2 counter before each communication. The S2 stage switches back from operation with the low-noise circuitry to the standard circuitry on the rollover of the low-noise S2 counter after each communication. In an alternate embodiment where low power consumption is not as much an issue, the S2 stage could be composed entirely of low-noise circuitry.

The time accuracy required for accurate ranging necessitates that no clock ticks are lost or gained in switching between the standard and low-noise circuitry of the low-frequency clock **119**. Triggering times for receptions and transmissions are provided by the processor **140** via data bus **190** to the LFC Data input of the low-frequency clock **119**. The triggering times are stored in event registers in the low-frequency clock **119**. The reception triggering circuitry and the transmission triggering circuitry are enabled by signals from the Output1 and Output2 terminals of the processor **140**, which are directed via lines **152** and **153** to the S4RxTrig and S4TxTrig inputs of the low-frequency clock **119**, respectively. When the time of a transmission event is reached to the accuracy of the S3 counter in the low-frequency clock **119**, the transmission triggering circuitry of the S2 stage is activated, and the power of the transmitter code-sequence generator **118** and the transmitter antenna driver **116** is turned on by signals to their TxPower inputs from the TxPower output of the low-frequency clock **119** via a transmission enable line **138**. Because the TxPower output from the S3 stage is asserted prior to the triggering of the S2 stage and the stages in the high-frequency real time clock **120**, this provides the transmitter code-sequence generator **118** and the transmitter antenna driver **116** circuits time to stabilize before beginning a transmission event. Similarly, when the time of a reception event is reached to the accuracy of the S3 counter in the low-frequency clock **119**, the reception triggering circuitry of the S2 stage is activated, and the power to the receiver code-sequence generator **117** is turned on by a signal to its RxPower input from the RxPower output of the low-frequency clock **119** via a reception enable line **155**. Because the RxPower output from the S3 stage is asserted prior to the triggering of the S2 stage and the stages in the high-frequency real time clock **120**, this provides the receiver code-sequence generator **117** time to stabilize before beginning a reception event.

When the time of a transmission event is reached to the accuracy of the S2 counter in the low-frequency clock **119**, a triggering signal is passed from the transmission triggering output S2TxTrig0 of the low-frequency clock **119** to the transmission triggering input S2TxTrig\$ of the high-frequency clock **120** via line **147** to enable transmission

triggering circuitry in the high-frequency clock 120. Similarly, when the time of a reception event is reached to the accuracy of the S2 counter in the low-frequency clock 119, a triggering signal is passed from the reception triggering output S2RxTrig0 of the low-frequency clock 119 to the reception triggering input S2RxTrig\$ of the high-frequency clock 120 on line 146 to enable reception triggering circuitry in the high-frequency clock 120. The high-frequency clock 120 includes a phase-lock loop circuit which uses the crystal clock signal XClock 148 at its XtalClock input to produce a high-frequency clock signal with a clock rate of about 200 MHz. The high-frequency clock signal is delayed by a programmable delay (not shown in FIG. 1) controlled by data provided to the HFC Data input by the processor 140 to generate a delayed high-frequency clock signal DClock, hereinafter referred to as the system clock signal DClock. The system clock signal DClock is supplied via line 160 to the DClock inputs of the time-integrating correlator 114, receiver code-sequence generator 117, and transmitter code-sequence generator 118.

When the time-integrating correlator 114 determines that a reception event is completed, it asserts a signal at its RxStop output which is directed to the RxStop input of the high-frequency clock 120 via reception-stop line 142. Similarly, when the transmitter code-sequence generator 118 determines that a transmission event is completed, it asserts a signal at its TxStop output which is directed to the TxStop input of the high-frequency clock 120 via transmission-stop line 137. Shortly after the high-frequency clock 120 receives a TxStop or RxStop signal, a signal asserted at the WReset output terminal of the high-frequency clock 120 is directed via reset line 170 to the WReset inputs of the time-integrating correlator 114, the receiver code-sequence generator 117, and the transmitter code-sequence generator 118 to reinitialize these components.

The miscellaneous logic block 150 monitors the status of communications to insure that the standard-logic circuitry of the low-frequency clock 119 and the processor 140 are not activated, and thus not creating noise, while communications are in progress. If a communication extends past the rollover time of the S2 counter, the signal asserted at the LFSR Running output of the miscellaneous logic block 150 and directed to the Running inputs of the low-frequency clock 119 and the processor 140 via LFSR running line 145 prevents the standard-logic circuitry from activating until another rollover from the S2 counter occurs. To determine when communications begin, the trigger outputs S2RxTrig0 and S2TxTrig0 from the low-frequency clock 119 are directed via lines 147 and 146 to the S2RxTrig\$ and the S2TxTrig\$ inputs of the miscellaneous logic block 150, respectively. To determine when communications are completed, the RxStop and TxStop outputs from the time-integrating correlator 114 and the transmitter code-sequence generator 118 are directed to the RxStop and TxStop inputs of the miscellaneous logic block 150 via reception-stop line 142 and transmission-stop line 137, respectively.

When an electromagnetic signal is incident on the reception antenna 102, the received signal $\Phi_c(t)$ is directed via reception antenna leads 175 and 176 to the inputs of a differential amplifier 105. The amplification of the analog differential amplifier 105 is controlled by the processor 140 which supplies data via the data bus 190 to the D/A converter 106. The D/A converter 106 converts the digital data to an analog signal at the Out1 terminal of the D/A converter 106 which is directed via voltage gain control line 129 to the VGain input of the differential amplifier 105. The D/A converter 106 also provides a current gain control

signal at its Out2 terminal which is directed to the IGain input of the time-integrating correlator 114 via a current gain control line 131. The voltage gain of the differential amplifier 105 is controlled to compensate for the inverse-square decay in the power of the received signal $\Phi_c(t)$ with distance between the communicating localizers. Differential output lines 125 and 126 from the differential amplifier 105 are directed to inputs $\Phi_c(t)^+$ and $\Phi_c(t)^-$ of the time-integrating correlator 114.

When the receiver code-sequence generator 117 is activated by having the signal to the WReset input go low and receiving a clock signal at the system clock input DClock, it generates a two-bit command sequence, the Code1 and Code0 outputs on lines 132 and 133 each providing one bit of the two-bit sequence to the Code1 and Code0 inputs of the time-integrating correlator 114, respectively. The particular command sequence Code1/Code0 is determined by the data directed from the processor 140 via data bus 190 to the RCSG Data input of the receiver code-sequence generator 117. The system clock DClock provided by the high-frequency clock 120 is directed via system clock line 160 to the clock input DClock of the receiver code-sequence generator 117. A reset signal directed to the WReset input of the receiver code-sequence generator 117 forces the Code1/Code0 outputs to zero between reception events.

The time-integrating correlator 114 provides the discrete-time pseudo-autocorrelation (DTPAC) function $\Lambda(n)$ as a differential analog output at terminals $\Lambda(n)^+$ and $\Lambda(n)^-$. The DTPAC function $\Lambda(n)$ is equal to the integral of the product of the received signal, $\Phi_c(t)$ directed to the $\Phi_c(t)^+$ and $\Phi_c(t)^-$ input terminals and an integration sequence $\Phi_i(t)$ encoded on the two-bit command sequence supplied to the Code1 and Code0 inputs. As shown in FIG. 18, the time-integrating correlator 114 includes a plurality of integrator circuits 1430 (similar components which have the same initial four-digit portion of their reference numerals will be referred to collectively by that portion of the reference numeral). The two-bit command sequence Code1/Code0 is delayed by a chain of flip=flops 1460 which are tapped by the integrators 1430. The rate at which the command sequence Code1/Code0 passes through the delay chain 1460 is controlled by the system clock DClock on line 160. The n^{th} integrator circuit 1430 calculates the integral of the product of the received signal $\Phi_c(t)$ and a delayed integration signal $\Phi_i(t)^{(n)}$, where the delayed integration signal $\Phi_i(t)^{(n)}$ is encoded on the delayed two-bit command sequence Code1/Code0 directed to the Code1 and Code0 inputs of the n^{th} integrator 1430. The preferred embodiment has thirty-two (sixteen pairs) integrators and rising edges of the 200 MHz system clock DClock are separated by 5 nanoseconds, so the delay between the time the command sequence Code1/Code0 is directed to the first pair of integrators 1430 and the last pair of integrators 1430 is 80 nanoseconds, i.e., the reception time window has a length of 80 nanoseconds.

After a reception event the time-integrating correlator 114 sends a signal from its RxStop output via reception-stop line 142 to the RxStop inputs of the high-frequency clock 120 and the miscellaneous logic block 150, as mentioned above. Also, after a reception event the reactivated processor 140 sends selection signals via the data bus 190 to the Select input of the time-integrating correlator 114. The selection signals control the multiplexing of the outputs from the integrators 1430 to the output terminals $\Lambda(n)^+$ and $\Lambda(n)^-$ of the time-integrating correlator 114. Also, after a reception event a reset signal from the high-frequency clock 120 is asserted at the WReset input of the time-integrating correlator 114 to reset the integrators 1430.

The signals at the $\Lambda(n)^+$ and $\Lambda(n)^-$ outputs of the time-integrating correlator **114** are analog signals which are converted to digital by directing them to the IN^+ and IN^- inputs of the A/D converter **107** via lines **127** and **128**. The digital DTPAC function $\Lambda(n)$ from the A/D converter is directed from the A/D data output via data bus **190** to the Data input of the processor **140**. The processor **140** processes the digital DTPAC function $\Lambda(n)$ to determine the arrival time of the received signal $\Phi_c(t)$.

For a transmission event the transmitter code-sequence generator **118** is activated by having the signal via line **170** to the WReset input go low and receiving a clock signal at the system clock input DClock from the high-frequency real time clock **120**. The system clock DClock provided by the high-frequency clock **120** is directed via the system clock line **160** to the clock input DClock of the transmitter code-sequence generator **118**. The transmitter code-sequence generator **118** then produces a two-bit transmission command sequence, the TxAntL and the TxAntR outputs on lines **135** and **136** each providing one bit of the two-bit command sequence to the TxAntL and TxAntR inputs of the transmitter antenna driver **116**. The particular transmission command sequence TxAntL/TxAntR is determined by the data directed from the processor **140** via data bus **190** to the TCSG Data input of the transmitter code-sequence generator **118**. A reset signal directed to the WReset input of the transmitter code-sequence generator **117** from the WReset output of the high-frequency clock **120** forces the command sequence outputs TxAntL and TxAntR to zero after a transmission event.

A signal to the TxPower input of the transmitter antenna driver **116** from the TxPower output of the low-frequency clock **119** via transmission power line **138** turns on the power to the transmitter antenna driver **116** in preparation for transmission events. The two-bit transmission command sequence TxAntL and TxAntR from the transmitter code-sequence generator **118** is directed to the TxAntL and TxAntR inputs of the transmitter antenna driver **116** to control transmissions via lines **135** and **136**. The transmission command sequence TxAntL and TxAntR controls the switching of current through a plurality of H-bridge switches (shown in FIG. **22**) to the transmission antenna **101** via transmission antenna leads **156** and **157**. The particular activated H-bridge switches are controlled by data from the processor **140** directed via data bus **190** to the TAD Data input of the transmitter antenna driver **116** to compensate for the inverse-square decay of signal power with the distance of separation between localizers, and to adjust transmission levels so as not to interfere with other nearby communicating localizers.

Detailed Description of the Ranging Transactions

The distance X between two localizers, A and B, is determined by measuring signal propagation times in cooperative ranging transactions. It will be assumed in the following discussion that the relative velocity of localizer A to localizer B is small enough to be insignificant during the time of a single ranging transaction. Furthermore, for ease of discussion it will initially be assumed that the localizers are synchronized and localizer A has an approximate knowledge of its distance X from localizer B, and the relative clock rate k_B of localizer B. The first approximations to the values X and k_B are determined during synchronization operations when localizers first begin communications. Synchronization operations are described later.

There are a number of communication protocols that can be used to determine the propagation times. In a first ranging

method **200** depicted in FIG. **2**, localizers A and B have previously arranged that localizer A will send a first communication to localizer B at a time T_1 . The transmission by localizer A is represented by the first positive pulse **220** in the timeline **210** of localizer A. Localizer B schedules to receive the first communication **222** during a reception time window **224** that is centered around time T_2 and has width ΔT_w , represented by the first negative pulse **224** in the timeline **212** of localizer B. The reception time window **224** is centered about the time when the first communication **222** is expected to arrive. After the reception time window **224** ends, localizer B analyzes the reception data during a processing period **230** and determines the precise time T_{2a} that the first communication **222** actually arrived.

After a prearranged delay time ΔT_c from the actual reception time T_{2a} , localizer B schedules a transmission event **240**, represented by the positive pulse at time T_3 in the timeline **212** of localizer B, and sends a second communication **242** back to localizer A. The delay ΔT_c is chosen to give localizer B sufficient time to determine the precise arrival time T_{2a} of the first communication **222**. Localizer A arranged to receive the second communication **242** in a reception time window **244**, represented by the negative pulse on the timeline **210** of localizer A, that is centered around a time T_4 , where T_4 is equal to the initial transmission time T_1 plus delay time ΔT_c plus an estimate of the propagation time for a signal to go from localizer A to localizer B and back. Then, localizer A analyzes the reception data during a processing period **250** and determines the precise time T_{4a} that the communication **242** arrived. Localizer A now has all the information necessary to calculate the round trip distance $2*X$, i.e.,

$$2*X=(T_{4a}-T_1-k_B*\Delta T_c)*c,$$

where c is the speed of light and k_B is the ratio of localizer A's clock rate to localizer B's clock rate. (Localizer A's clock rate is assumed to be correct, i.e., $k_A=1$.) This method provides an updated measurement of the separation distance X between the two localizers.

Unfortunately, this first ranging method **200** is sensitive to drifting of the relative clock rates over the long time required to perform the distancing communications. Assuming that a typical microprocessor can execute one million instructions per second, and assuming it will take 1000 instructions to analyze the correlator values to determine the first reception time T_{2a} , the delay time ΔT_c between the first reception **224** and the second transmission **240** will have to be on the order of one millisecond. The propagation time of electromagnetic radiation over a distance of 30 meters is only 100 nanoseconds. Thus, the time period we wish to determine, namely the propagation time of the communication between the localizers, is one hundred parts per million of the time period that is measured, namely $T_{4a}-T_1$.

In a modification of this procedure, localizers A and B could iterate and converge on the correct arrival times of the communications as shown in the iterative procedure **300** in the flowchart of FIG. **3**. In a first step **312** the two localizers perform the ranging protocol as described above for FIG. **2**. In the next step **314** localizer B modifies its value of the central time T_2 of its next reception window **224** by an amount $(T_{2a}-T_2)$ so that the next communication should arrive in the middle of the reception time window **224**. In the step **316** localizer A modifies the central time T_4 of its next reception window **244** so that the next arrival time T_{4a} should occur in the middle of its reception window **244**. In the testing step **318** localizer A tests the accuracy of the most recent ranging transaction by checking to see if the value of

central time T_4 of its reception window **244** was changed in the previous step **316**. If the central time T_4 did need adjusting, then control returns back to the initial step **312** and another iteration of the ranging protocol of FIG. **2** occurs. If the change to time T_4 in step **316** was zero, or some reasonably small prearranged amount, then the iterative procedure **300** is complete. After a few iterations, the actual reception times T_{2a} and T_{4a} will converge to the centers of the reception windows **224** and **250**, and the iterative procedure **300** is complete. Before the iterations converge, localizer A has information concerning the actual arrival time T_{4a} , but does not know localizer B's reception time T_{2a} . After the iterations are complete in step **319**, the value of actual arrival time T_{2a} is assumed to have converged on central time T_2 of localizer B's reception window **224**, and localizer A can calculate the round trip distance $2X$ from the round trip transit time $T_{4a}-T_1-\Delta T_c$.

An improvement on the first ranging method **200** of FIG. **2** is a second ranging method **400** shown in FIG. **4**. In this second method **400** localizer A sends a first communication **421** during a transmission event **420**, represented by the first positive pulse in the timeline **410** of localizer A, beginning at prearranged time T_1 . Localizer B expects the first communication **421** to arrive during a reception time window **422** centered around time T_2 , represented in FIG. **4** by the first negative pulse in the timeline **412** of localizer B. Without waiting to calculate the precise arrival time T_{2a} of the first communication **421**, localizer B sends a second communication **425** back to localizer A in a transmission event **424**, represented by the first positive pulse in the timeline **412** of localizer B. The transmission event **424** begins at time T_3 after a short delay time ΔT_d from the center T_2 of the reception time window **422**. The only limit on the shortness of ΔT_d being that localizer B must have a chance to finish receiving the communication **421** from localizer A, i.e., ΔT_d must be greater than about 10 microseconds. (Alternatively, ΔT_d may be negative and the first and second communications **421** and **425** will cross in the space between the localizers.) Localizer A arranges to receive the second communication **425** during a reception time window **426**, represented by the first negative pulse in the timeline **410** of localizer A, centered around time T_4 . The time T_4 at which localizer A's reception time window **426** is centered takes into account the approximate round trip propagation time of the radio communications and the time delay ΔT_d . After transmission **424**, localizer B then calculates the precise arrival time T_{2a} of the first communication **421** during a processing period **430**. In the figures, such processing periods are represented by shaded boxes **430**, **431**, **443**, **453**, **463**, and **473** along the timelines **410** and **412**. After the second reception window **426**, localizer A calculates the precise arrival time T_{4a} of the second communication **425** during a processing period **431**. After a second prearranged time delay ΔT_c from the beginning of localizer B's transmission time **424**, localizer B sends a set of correction bit communications **441**, **451**, **461**, and **471** during transmission time windows **440**, **450**, **460**, and **470**, beginning at times T_5 , T_7 , T_9 and T_{11} , respectively. The correction bit communications **441**, **451**, **461**, and **471** are received by localizer A during reception time windows **442**, **452**, **462**, and **472**, centered at times T_6 , T_8 , T_{10} and T_{12} , and processes during processing periods **443**, **453**, **463** and **473**, respectively. In the preferred embodiment, there may be more or less than four correction bits sent. The correction bits **441**, **451**, **461**, and **471** communicate the difference ΔT_c between the central time T_2 of localizer B's reception time window **422** and the actual arrival time T_{2a} of the first

communication signal **421** at localizer B. This provides localizer A with enough information to calculate the separation distance X , i.e.,

$$2*X=(T_{4a}-T_1-k_B*(\Delta T_d-\Delta T_c))*c.$$

The accuracy of this calculation is superior to that of the first method **200** since in this case the time $T_{4a}-T_1$ between localizer A's first transmission **420** and localizer A's first reception **426** is on the order of tens of microseconds. Therefore, the value to be ascertained, a propagation time on the order of 100 nanoseconds, is only one part in 100 of the time period measured, an improvement of two orders of magnitude from the first method **200**. This second method **400** is also inherently more accurate than the first method **200** because the time difference ΔT_c between the expected arrival time T_2 and the actual arrival time T_{2a} of the first communication **421** at localizer B is communicated from localizer B to localizer A and taken into account in every round trip time calculation.

an iterative modification of the method **400** of FIG. **4** is shown in the flowchart of FIG. **5** where a series of communications between the two localizers provides a converging estimate of the separation X between the two localizers. In a first step **512**, the two localizers perform the ranging method **400** of FIG. **4** described above. Localizer A has enough information at the next step **514** to modify the initial transmission time T_1 for the next iteration so that the first communication **421** arrives in the center of localizer B's next reception time window **422**. Note that localizer B does not have to change the expected arrival time T_2 ; rather, localizer A shifts the transmission time T_1 by ΔT_c . In the next step **516** localizer A modifies its reception time T_4 so the communication **425** from localizer B arrives in the center of localizer A's reception time window **426**. T_1 and T_4 are modified according to the following formula:

$$T_1'=T_1-k_A*\Delta T_c, T_4'=T_{4a}.$$

In the following step **518**, localizer A determines if another iteration of the method **400** of FIG. **4** is necessary by checking to see if T_1 and T_4 were actually changed in the previous steps **514** and **516**. If the changes were too large, control is returned to the initial step **512** for another iteration. If the changes were sufficiently small, the iterations are terminated **519**. The iterative method **500** of FIG. **5** is superior to that of the iterative method **300** of FIG. **3**, since only one of the localizers (localizer A) modifies its transmit and receive times, thereby decreasing the possibility of losing synchronization by one localizer transmitting at a time such that the transmission arrives outside the reception window of the other localizer.

Another iterative modification of the method **400** of FIG. **4** is shown in FIG. **6**. In this modification **600** the number of correction bits is drastically decreased, at the cost of requiring a number of iterations of the ranging method **400** of FIG. **4** to provide a final distance estimate. In this case the correction bits **441**, **451**, etc. are replaced with a single correction bit which alters the polarity of the communication **425** from localizer B to localizer A to indicate whether the transmission **421** from localizer A arrived in the earlier half or the later half of the reception window in the previous round of communications. Since the communication **425** is part of the ranging transaction and must be sent anyway, none of the correction bits **441**, **451**, etc. are required. As described in detail below, the information in this single-bit return communication **425** allows localizer A to modify the time T_1 of its transmission **420** on successive iterations to

converge on the correct time using an efficient, logarithmic, binary search technique.

In an initial step **610**, a time step variable ΔT_x is initialized to a value of +20 nanoseconds. This value ΔT_x is chosen to be no more than one quarter of the width ΔT_w of the reception window **422**. In a first ranging step **612**, the two localizers perform the ranging protocol **400** of FIG. 4, without sending correction bits **441**, **451**, etc. from localizer B to localizer A. In a second ranging step **614**, the localizers perform the ranging protocol **400** of FIG. 4, with the second communication **425** being modulated by a correction bit value, i.e., if the correction bit is positive the polarity of the return communication **425** is unaffected, and if the correction bit is negative the polarity of the return communication **425** is inverted. As discussed above, the ranging protocol of FIG. 4 consists of: a first communication **421** transmitted from localizer A during a transmission event **420** beginning at a first transmission time T_1 and received by localizer B in a reception window **422** centered at a first reception time T_2 ; a second communication **425** transmitted from localizer B during a transmission event **424** beginning at a second transmission time T_3 and received by localizer A in a reception window **426** centered at a second reception time T_4 ; and computation periods **431** and **430** where localizers A and B determine the actual reception times T_{2a} and T_{4a} of the second and first communications **425** and **421**, respectively. In the method **400** of FIG. 4 there are also a number of correction bits **441**, **451**, etc. sent back to localizer A from localizer B representing the difference between the actual arrival time T_{2a} of the first communication **421** and the central time T_2 of localizer B's reception window **422**. However, in the modification **600** diagrammed in FIG. 6, localizer B calculates only the sign of the correction value, and sends it in communication **425** of the following ranging transaction.

In a first testing step **616** of the method **600**, localizer A tests the sign of the correction bit to see if it matches the sign of the step variable ΔT_x . If the signs match, this means the transmission time T_1 is to be moved in the direction of the sign of the time step ΔT_x , and control passes to a time incrementation step **624** where the time step ΔT_x is added to the first transmission time T_1 . If the signs do not match, control passes to a reverse direction step **618** since the ΔT_x value is assumed to have just been incremented past the correct first transmission T_1 time. In this step **618** the sign of the step variable ΔT_x is reversed and the step variable ΔT_x is also divided in half, so as to converge on the correct first transmission time T_1 in a binary search fashion. After reversing direction in step **618**, a second testing step **620** is performed to see if the absolute value of ΔT_x is less than the smallest possible change in transmission time $\Delta T_x(\text{min})$. In this case the iterative ranging **600** is complete and the value of the first transmission time T_1 is known to within the required accuracy. If the accuracy has reached the desired limit, control passes to a final step **622** where the first transmission time T_1 is updated a final time. Localizer A now uses the round trip time $(T_{4a} - T_1 - \Delta T_d)$ to calculate the distance to the desired accuracy. If the required accuracy was not reached in the second testing step **620**, then control again passes to the time incrementation step **624**, and the time step ΔT_x is added to localizer A's next transmission time T_1 . This will have the effect of moving the next communication **421** of localizer A so that it lands closer to the middle of localizer B's reception window **422**. From this step **624**, control passes back to the ranging step **614**.

Because the correction bit of the n^{th} communication indicates the offset between the arrival time T_{2a} and the

central time T_2 of the reception window **422** of the $(n-1)^{\text{th}}$ communication and affects the first transmission time T_1 of the $(n+1)^{\text{th}}$ communication, the ranging protocol **600** will occasionally step too far in one direction before reversing the sign of the time step variable ΔT_x . The time step ΔT_x is initialized to no more than one quarter of the length of the reception window **422**, since then an extra step past the correct location can never result in stepping out of the reception window **422**. This effect could be circumvented by looping back from the incrementing step **624** to the first ranging step **612** instead of the second ranging step **614**, but this would result in two ranging transactions for every iteration, rather than one.

A third ranging method **700**, illustrated in FIG. 7a, determines the ratio of the clock rates of the two localizers, as well as the distance between the localizers. Let K_a be the ratio of actual time T to the time as measured by localizer A, and k_b be the ratio of the actual time T to the time as measured by localizer B. In this method **700** localizer A does a first ranging transaction with localizer B, as in the first portion of the second method **400** consisting of the first two communications **421** and **425**. Localizer A sends a first communication **721** in a transmission event **720** beginning at prearranged time T_1 . Localizer B expects the first communication **721** to arrive during a reception time window **722** centered around time T_2 . Localizer B sends a second communication **725** back to localizer A in a transmission event **724** which begins at a transmission time T_3 equal to a short delay time ΔT_d from the center T_2 of the reception time window **722**. Localizer A arranges to receive the second communication **725** during a reception time window **726** centered around time T_4 . After transmitting to localizer A, localizer B then determines the precise arrival time T_{2a} of the first communication **721** during a processing period **730**. After receiving the second communication **725** localizer A determines the precise arrival time T_{4a} of the second communication **725** during a processing period **731**. Then localizers A and B switch roles and do a second ranging transaction as in the first portion of the second method **400**, i.e., localizer B sends a third communication **741** in a transmission event **740** beginning at time T_5 , which is at a prearranged time ΔT_c after localizer B's previous transmission event **724**. Localizer A expects the communication **741** to arrive during a reception time window **742** centered at time T_6 . Localizer A then sends a fourth communication **745** back to localizer B in a transmission event **744** at a transmission time T_7 which begins after a short delay time ΔT_d from the center T_6 of localizer A's recent reception time window **742**. Localizer B arranges to receive the communication **745** during a reception time window **746** centered at time T_8 . After transmitting to localizer B, localizer A then calculates the precise arrival time T_{6a} of the previous communication **741** during a processing period **732**. After receiving the communication **745** from localizer A, localizer B calculates the precise arrival time T_{8a} of the communication **745** during a processing period **733**. Then the localizers calculate the following quantities:

$$R_a = T_{4a} - T_1$$

The round trip time of the first transaction on A's clock.

$$D_b = T_3 - T_{2a}$$

The turn-around time of the first transaction on B's clock.

$$R_b = T_{8a} - T_5$$

The round trip time of the second transaction on B's clock.

-continued

$D_a = T_7 - T_{6a}$	The turn-around time of the second transaction on A's clock.
----------------------	--

Localizer B then transmits the values of R_b and D_b to localizer A as a series of correction bits according to a prearranged protocol. For ease of display, only four of the correction-bits are shown and labeled in FIG. 7a. The correction bits **752**, **762**, **772**, and **782** are sent in a series of transmission events **750**, **760**, **770**, and **780** at times T_9 , T_{11} , T_{13} , and T_{15} , respectively. To receive the correction bits **752**, **762**, **772**, and **782**, localizer A schedules reception time windows **754**, **764**, **774**, and **784**, centered around times T_{10} , T_{12} , T_{14} , and T_{16} , and does calculations during computation periods **756**, **766**, **776**, and **786** to detect the values of the bits, respectively. To send the values of R_b and D_b , more than four bits may actually need to be sent. Transmission event **750**, reception window **754**, and calculation **756** comprise the steps necessary to send just one bit starting at time T_9 .

After receiving all the correction bits **752**, **762**, **772** and **782**, localizer A now has the information necessary to solve two equations for two unknowns, the separation distance X, and the ratio of the clock rates k_A/k_B . The two equations are:

$$X = c * (R_a * k_A - D_b * k_B) / 2,$$

and

$$X = c * (R_b * k_B - D_a * k_A) / 2,$$

where c is the speed of light. If localizer A assumes that its clock is the correct one, the value of k_A is assumed to be unity, and the only remaining unknowns are k_B and X. Solving for X and k_B provides:

$$X = c * (R_a * R_b - D_b * D_a) / (2 * (R_b + D_b))$$

and

$$k_B = (R_a + D_a) / (R_b + D_b).$$

At a later pre-arranged time, localizer A can transmit the values of localizer A's roundtrip and turn-around times R_a and D_a to localizer B so that localizer B can calculate the distance X and relative clock rate k_A of localizer A (assuming k_B to be unity). Alternately, localizer A can transmit the computed distance and the ratio of the clock rates and localizer B would then not have to perform the calculations.

FIG. 7b shows a modification **2700** of the third ranging method **700** illustrated in FIG. 7a, where again the ratio of the clock rates of the two localizers, as well as the distance between the localizers is determined. In this modification **2700** the two sequential communications **725** and **741** transmitted by localizer B are combined into a single communication **2725**, the processing periods **731** and **732** of localizer A are combined into a single processing period **2732**, and the majority of the time devoted by localizer B to processing is also combined into a single processing period **2733**. The localizers A and B still have two round trip communications since the first and second transmission may be considered a first round trip pair and the second and third communications may be considered a second round trip pair. From measurements of the two round trip times the ratio of the clock rates k_a/k_b and the distance X between the localizers A and B can be determined. Since the total elapsed time for the ranging communications of FIG. 7b is reduced in

comparison with the method of FIG. 7a, the accuracy of the measurements is improved.

As shown in FIG. 7b, localizer A sends a first communication **2721** in a transmission event **2720** beginning at prearranged time T_1 . Localizer B expects the first communication **2721** to arrive during a first reception time window **2722** centered around time T_2 . Localizer B sends a second communication **2725** back to localizer A in a transmission event **2724** which begins at a transmission time T_3 equal to a short delay time ΔT_d from the center T_2 of the first reception time window **2722**. Localizer A arranges to receive the second communication **2725** during a second reception time window **2726** centered around time T_4 .

After the first transmission to localizer B, localizer B then prepares to receive a third communication **2745** from localizer A by either A/D converting the values in the correlator bins and storing them in memory, or initializing a second correlator circuit, during a processing period **2730**. Localizer A then sends a third communication **2745** to localizer B beginning at a transmission time T_7 equal to a short delay time ΔT_d from the center T_4 of the second reception time window **2725**. Localizer B arranges to receive the third communication **2745** during a third reception time window **2746** centered around time T_8 .

After transmitting to localizer B, localizer A then calculates the precise arrival time T_{4a} of the second communication **2725** during a processing period **2732**. After receiving the third communication **2745** from localizer A, localizer B calculates the precise arrival times T_{2a} and T_{8a} of both the first and third communications **2721** and **2745** during a processing period **2733**. Then, the localizers determine the following quantities:

$R_a = T_{4a} - T_1$	The round trip time of the first pair of communications on A's clock.
$D_b = T_3 - T_{2a}$	The turn-around time of the first pair of communications on B's clock.
$R_b = T_{8a} - T_3$	The round trip time of the second pair of communications on B's clock.
$D_a = T_7 - T_{4a}$	The turn-around time of the second pair of communications on A's clock.

Localizer B then transmits the values of R_b and D_b to localizer A as a series of correction bits according to a prearranged protocol. For ease of display, only four of the correction-bits are shown and labeled in FIG. 7b. The correction bits **2752**, **2762**, **2772**, and **2782** are sent in a series of transmission events **2750**, **2760**, **2770**, and **2780** at times T_9 , T_{11} , T_{13} , and T_{15} , respectively. To receive the correction bits **2752**, **2762**, **2772**, and **2782**, localizer A schedules reception time windows **2754**, **2764**, **2774**, and **2784**, centered around times T_{10} , T_{12} , T_{14} , and T_{16} , and does calculations during computation periods **2756**, **2766**, **2776**, and **2786** to determine the values of the bits, respectively. To send the values of R_b and D_b , more than four bits may actually need to be sent. Transmission event **2750**, reception window **2754**, and calculation **2756** comprise the steps necessary to send just one bit starting at time T_9 .

After receiving all the correction bits **2752**, **2762**, **2772** and **2782**, localizer A now has the information necessary to solve two equations for two unknowns, the separation distance X, and the ratio of the clock rates k_A/k_B . As before,

$$X = c * (R_a * R_b - D_b * D_a) / (2 * (R_b + D_b))$$

and

$$k_B = (R_a + D_a) / (R_b + D_b).$$

At a later pre-arranged time, localizer A can transmit the values of localizer A's roundtrip and turn-around times R_A and D_a to localizer B so that localizer B can calculate the distance X and relative clock rate K_A of localizer A (assuming k_B to be unity). Alternately, localizer A can transmit the computed distance and the ratio of the clock rates and localizer B would then not have to perform the calculations.

Detailed Description of Synchronization Protocols

Before two localizers can begin any of the above ranging algorithms, it is assumed that the pair of localizers are synchronized, i.e., that each localizer has determined a time when it can send a communication that the other localizer will be able to detect, and a time when it can listen and receive a communication from the other localizer. Once synchronized, these transmission and reception times are repeated on a regular or pseudorandom basis. In the process described below, one of the localizers acquires an approximate distance in the process of developing the synchronization. However, it is possible for two localizers to become synchronized, and even to exchange digital information, without either localizer determining the distance to the other localizer.

In a synchronization procedure **800** according to the preferred embodiment shown in FIG. **8**, localizer A executes the procedure **800** while localizer B produces a beacon for localizer A to find. This beacon could be a unique communication code produced on a regular or pseudorandom time basis. For the purpose of discussion it will be assumed that the beacon will be regularly broadcast once every millisecond.

In the first step **810** of the synchronization procedure **800**, localizer A locates one of these communications. There are a number of algorithms localizer A could use to find the beacon, such as a linear search or a random search of all times (modulo the one millisecond re-broadcast time). If localizer A does a linear search, each of localizer A's reception windows are separated by one millisecond plus a small offset. The offset must be no larger than the width of a reception window in order to guarantee that every time slot is checked, and should be less than the width of a reception window to prevent the beacon escaping noticing by arriving too near the edge of a reception window. Localizer A continues listening at different offsets until a beacon communication is received. With a one millisecond re-broadcast time and a 100 nanosecond reception window, this search takes an average of 5 seconds. It would be noted that if the clocks drift by 100 parts per million, the drift per beacon is on the order of the length of a reception window and a linear search may be unsuccessful. This problem can be reduced by intermixing a forward and backward linear search, or by searching in a pseudorandom pattern.

In the second step **812** of the synchronization algorithm **800**, localizer A determines the relative clock rate of localizer B. The ratio of the time measured by localizer A between beacons to the expected one millisecond time generates a first approximation to the clock rate ratio $k_B k_A$. If the clocks have a constant ratio, this ratio can be determined by measuring the time between a pair of beacons; if the clock rate ratio varies this behavior must be determined by sampling more than two beacons. When localizer A has determined the relative clock rate of localizer B, localizer A can then receive beacons indefinitely.

To complete the synchronization process, localizer A must now determine times at which return transmissions from

localizer A will be receivable by localizer B. Localizer B listens for return transmissions a predetermined fixed delay time before or after each beacon transmission. (In this example it will be assumed that localizer B listens for a return transmission a fixed delay time ΔT_r after the beacon signal.) When a communication is successfully received in one of these reception events, localizer B acknowledges the reception by inverting the polarity of the next beacon transmission a millisecond later. So in the next step **814** of the synchronization procedure **800**, localizer A initializes a counting integer n to one and a first estimate X_1 of the separation distance to zero, in preparation for an iterative search for a transmission time such that the communication will arrive while localizer B is listening. This first estimate X_1 of the separation distance is used in the ranging step **816** to determine the delay between the reception of a beacon at localizer A and a return transmission by localizer A. In particular, the delay is equal to $(\Delta T_r - X_1/c)$. If the distance estimate X_1 is close to correct then the return transmission by localizer A will arrive during the reception window of localizer B, and localizer B will invert the polarity of the next beacon to localizer A. (In the preferred embodiment the reception windows are approximately 80 nanoseconds long, and so distance estimates must be correct to within plus or minus approximately ten meters, and the distance estimates are incremented by twenty meters.) If in the test step **818** localizer A determines that the polarity of the beacon has been inverted, then an approximate separation distance has been determined and the synchronization process is complete **822**.

However, if in the test step **818** localizer A determines that the polarity of the beacon has not been inverted, then in update step **820** the estimated distance X_n of the recently transmitted communication is assumed to be too small, a new estimate X_{n+1} of the separation distance is set equal to the previous estimate X_n plus twenty meters, the counting integer n is incremented by one, and control is returned back to the ranging step **816**. Because localizer A alters its distance estimates X_n in twenty meter increments, it will rapidly find the correct distance in a small number of attempts since the range of the localizers is on the order of one thousand meters. Finally, when the distance estimate X_n is correct to within plus or minus ten meters, the inverted beacon is received by localizer A and control passes to the final step **822** where the distance estimate X_n is saved for future ranging transactions. Once the two localizers A and B are in synchronization, they may wish to exchange digital information or perform ranging transactions as described in FIGS. **4** through **7** to determine their separation distance to greater accuracy.

The synchronization procedure of FIG. **8** allows localizer A to calculate initial approximations to the distance and relative clock rate of localizer B. In an alternate method, localizer A transmits a return communication at a fixed time after receiving the beacon, and localizer B searches for localizer A's return communication. Although synchronization using this method takes longer than in the method previously described, this allows localizer B to determine the approximate separation distance, while localizer A can only determine the relative clock ratio. In another alternate method, the fixed delays used by localizers A and B would be unknown to the other localizer, and the approximate distance X_n would be incorrect. But this technique allows the two localizers to get into synchronization without divulging their relative locations.

Detailed Description of Protocols which Permit Privacy

There are several techniques a first localizer can use to find its distance from a second localizer without giving such

information away. This ability may be required in situations where divulging the precise location of a localizer would be considered an invasion of privacy. It may also be required in, for example, a military situation where giving away a localizer's precise location would be dangerous. In the methods **200** and **400** transactions described in FIGS. **2** and **4**, localizer A determines its distance from localizer B without giving any information away. Unfortunately these methods **200** and **400** are not as accurate as the method **700** diagrammed in FIG. **7a**, since in that method **700** both the distance and the ratio of the clock rates k_A/k_B are determined. The method **900** diagrammed in FIG. **9** is a modification of the method **700** described by FIG. **7a** which provides localizer A with accurate distance information, but gives localizer B an erroneous or obviously wrong distance.

This ranging method **900** is similar to the ranging protocol **700** diagrammed described in FIG. **7a**, but in the method **900** diagrammed in FIG. **9** a spoofing delay ΔT_s is chosen by localizer A to give the appearance that it is farther away or closer to localizer B than it actually is. Localizer A may choose the values of the spoofing delay ΔT_s randomly to cause its position to appear in random positions over a large area. Or, localizer A can choose the spoofing delay ΔT_s to give a fixed, but incorrect, location. If the spoofing delays ΔT_s are randomly chosen then it will be obvious that localizer A is hiding its location. If the spoofing delays ΔT_s are chosen to give a fixed but incorrect location, a different spoofing delay ΔT_s would have to be chosen and used for each localizer that localizer A is in communication with, and the network of surrounding localizers will not know that it does not have the correct location of localizer A.

In the protocol shown in FIG. **9**, events occurring at localizer B are shown on the bottom time line **910**, events occurring at localizer A are shown on the middle timeline **912**, and the events at localizer A as they are made to appear to localizer B are shown on the top timeline **914**. As shown in FIG. **9**, in this method **900** localizer A sends a first communication **721** during a transmission event **720** beginning at prearranged time T_1 . Localizer B expects the first communication **721** to arrive during a reception time window **722** centered around time T_2 . Localizer B sends a second communication **725** back to localizer A in a transmission event **724** which begins at a transmission time T_3 equal to a short delay time ΔT_d from the center T_2 of the reception time window **722**. Localizer A arranges to receive the second communication **725** during a reception time window **726** centered around time T_4 . After transmitting to localizer A, localizer B then calculates the precise arrival time T_{2a} of the first communication **721** during a processing period **730**. After receiving the second communication **725** localizer A calculates the precise arrival time T_{4a} of the second communication **725** during a processing period **731**.

Then localizers A and B switch roles and do a second ranging transaction. Localizer B sends a third communication **741** during a transmission event **740** beginning at time T_5 , which is at a prearranged time ΔT_c after localizer B's previous transmission event **724**. Localizer A expects the communication **741** to arrive during a reception time window **742** centered around time T_6 . Localizer A then sends a fourth communication **745** back to localizer B in a transmission event **744** which begins at a transmission time T_7 equal to the short delay time ΔT_d plus the spoofing delay ΔT_s from the center T_6 of localizer A's recent reception time window **742**. Localizer B arranges to receive the communication **745** during a reception time window **746** centered around time T_8 . After transmitting to localizer B, localizer A then calculates the precise arrival time T_{6a} of the previous

communication **741** during a processing period **732**. After receiving the communication **745** from localizer A, localizer B calculates the precise arrival time T_{8a} of the communication **745** during a processing period **733**.

Dashed lines **946** and **948** show how the reception and transmission windows **742** and **744** appear as reception and transmission windows **942** and **944** to localizer B since localizer B expects localizer A to only wait a delay time ΔT_d after the center of its reception window **942** to begin the transmission **944**. Therefore, localizer B also expects that the initial transmission **720** occurred as an earlier transmission **922**, and that localizer A received the second communication **725** at a reception event **924** which occurred later than the actual reception event **726**. Next, the localizers calculate the following quantities:

$R_a = T_{4a} - T_1$	The round trip time of the first pair of communications on A's clock.
$D_b = T_3 - T_{2a}$	The turn-around time of the first pair of communications on B's clock.
$R_b = T_{8a} - T_5$	The round trip time of the second pair of communications on B's clock.
$D_a = T_7 - T_{6a}$	The turn-around time of the second transaction on A's clock.

Localizer B then transmits the values of R_b and D_b to localizer A as a series of correction bits **752**, **762**, **772**, and **782** in transmission events **750**, **760**, **770**, and **780** at transmission times T_9 , T_{11} , T_{13} , and T_{15} , respectively, according to a prearranged protocol. For ease of display, only four correction-bit communications are shown and labeled in FIG. **9**. To send the values of R_b and D_b , more than four bits may actually need to be sent. To receive the communications **752**, **762**, **772**, and **782**, localizer A schedules reception time windows **754**, **764**, **774**, and **784**, centered around times T_{10} , T_{12} , T_{14} , and T_{16} , and does calculations during computation periods **756**, **766**, **776**, and **786** to detect the values of the bits, respectively.

After receiving all the correction bits **752**, **762**, **772**, and **782**, localizer A now has the information necessary to solve two equations for two unknowns, the separation distance X and the ratio of the clock rates k_A/k_B . The two equations are:

$$X = c * (R_a * k_A - D_b * k_B) / 2,$$

and

$$X = c * (R_b * k_B - D_a * k_A) / 2,$$

where c is the speed of light. If localizer A assumes that its clock rate is correct, the value of k_A is unity, and the only remaining unknowns are k_B and X. Solving for X provides:

$$X = c * (R_a * R_b - D_b * D_a) / (2 * (R_b + D_b));$$

and solving for k_B provides:

$$k_B = (D_a + R_a) / (D_b + R_b).$$

Localizer A now has an accurate measure of the distance to localizer B, while localizer B has an incorrect value equal to $X + (\Delta T_s / C)$. If localizer A communicates round trip and turn-around times R_a and D_a to localizer B, localizer A must correct the values to be consistent with the spoofing delay ΔT_s it used. Although localizer B uses R_a and D_a to calculate an incorrect X value, when localizer B calculates the value of k_A , it gets the accurate result:

$$X = c * (R_a * R_b - D_b * D_a) / (2 * (R_b + D_b));$$

and solving for k_B provides:

$$k_A = (D_b + R_b) / (D_a + R_a).$$

Dashed line **926** shows how adding ΔT_s to R_a makes the time and distance of transmission event **720** appear in the position shown by transmission event **922**. Similarly, dotted line **928** shows how adding ΔT_s to R_s makes the time and distance of reception window **726** appear in the position shown by reception window **924**.

Although localizer **A** can use a different random spoofing delay ΔT_s value with every localizer it communicates with, once communication is initiated, the value of the spoofing delay ΔT_s cannot change by more than about 40 nanoseconds between communications to the same localizer. This is because the reception window **746** is only about 80 nanoseconds wide. If the ΔT_s value caused communication **745** to miss reception window **746**, the localizers would loose contact with each other, and have to re-synchronize.

Detailed Description of Spectra of Nonsinusoidal Transmissions

In contrast with sinusoidal-carrier spread spectrum techniques, the transceivers of the present invention generate transmissions whose spectra cover a broad range of frequencies by transmitting sequences of short impulses. In general, the width of the Fourier spectrum of the impulse sequence is inversely proportional to the width of the individual impulses in an impulse sequence.

Consider a single Gaussian impulse $G(t)$, as, is shown in FIG. **10a.1**, described by the equation

$$G(t) = G_0 \exp[-4\pi((t-t_m)/d)^2].$$

For simplicity, we will set the amplitude G_0 to one. Then, the Fourier transform of the impulse $G(t)$ is

$$\begin{aligned} F[G] &= \int \exp[-4\pi((t-t_m)/d)^2] * \exp[i\omega t] dt \\ &= \exp[-\omega^2 d^2 / 16\pi] * \exp[i\omega t_m] * \\ &\quad \int \exp[-(4\pi/d^2)t - (i\omega d^2/8\pi)^2] dt \\ &\propto \exp[-\omega^2 d^2 / 16\pi] * \exp[i\omega t_m], \end{aligned}$$

and the magnitude of $F[G]$ is $\exp[-\omega^2 d^2 / 16\pi]$. Therefore, as shown in FIG. **10a.2**, the $1/e^x$ width, d , of the Gaussian impulse $G(t)$ is inversely proportional to the $1/e^x$ width $\omega = 4\pi/d$ ($f = 2/d$) of the Fourier spectrum $F[G]$ of the impulse.

The shape of the Fourier spectrum of a transmitted code sequence $\Phi_c(t)$ can be manipulated by controlling the placement of the impulses in the chips $\gamma_c(t)$. In particular, the location of zeroes in the magnitude of the spectrum can be controlled so that localizer transmissions provide a minimum of noise in particular frequency bands. For instance, it is desirable to minimize the interference provided by localizers to the commercial AM and FM radio frequency bands at 0.525–1.7 MHz and 88–108 MHz, respectively.

The chip function $\gamma_c(t)$ of the preferred embodiment is a doublet function consisting of a positive impulse $G(t)$ and a delayed negative impulse $-G(t-t_0)$, where t_0 is the delay time, as shown in FIG. **10b.1**. The Fourier transform of the chip function is

$$\begin{aligned} F[\gamma_c] &= F[G(t)] - F[G(t-t_0)] \\ &= \int \exp[-4\pi(t/d)^2] * \exp[i\omega t] dt - \\ &\quad \int \exp[-4\pi(t-t_0/d)^2] * \exp[i\omega t] dt \\ &\propto \exp[-\omega^2 d^2 / 16\pi] * \{1 - \exp(i\omega t_0)\}. \end{aligned}$$

As shown in FIG. **10b.2**, the magnitude of the Fourier transform, $|F[\gamma_c]|$, has an envelope equal to the Fourier transform of a single impulse $F[G]$, and has zeroes at multiples of $\omega = 2\pi/t_0$ ($f = 1/t_0$). The zeroes in the spectrum include one at zero frequency (DC) since the integral of the pair of impulses is zero. If the spacing between the impulses is reduced to t_1 as shown in FIG. **10e.1**, then the distance between zeroes in the magnitude of the Fourier spectrum is increased to $\omega = 2\pi/t_1$ ($f = 1/t_1$) as shown in FIG. **10e.2**.

The simplest transmitted impulse sequence $\Phi_c(t)$ larger than a single chip $\gamma_c(t)$ is a pair of chips. As shown in FIG. **10c.1**, one possibility or a pair of chips is a positive polarity chip $\gamma_c(t)$ followed by a negative polarity chip delayed by the time length δt of a chip, i.e., $-\gamma_c(t-\delta t)$. The Fourier transform of this pair of chips is

$$\begin{aligned} F[\gamma_c(t) - \gamma_c(t-\delta t)] &= F[\gamma_c(t)] - F[\gamma_c(t-\delta t)] \propto \\ &\quad \exp[-\omega^2 d^2 / 16\pi] * \{1 - \exp(i\omega t_0)\} * \{1 - \exp(i\omega \delta t)\}. \end{aligned}$$

The magnitude of the spectrum F is equal to the product of the magnitudes of the factors $\exp[-\omega^2 d^2 / 16\pi]$, $\{1 - \exp(i\omega t_0)\}$, and $\{1 - \exp(i\omega \delta t)\}$. Therefore the magnitude of a spectrum of the pair of chips is equal to the magnitude of the spectrum of a single chip $\gamma_c(t)$ modulated by the factor $\{1 - \exp(i\omega \delta t)\}$. As shown in FIG. **10c.2**, the magnitude of the spectrum of the pair of chips has an envelope equal to that of a single impulse $G(t)$, zeroes at multiples of $\omega = 2\pi/t_0$ ($f = 1/t_0$), and zeroes at multiples of $\omega = 2\pi/\delta t$ ($f = 1/\delta t$).

In general, a transmitted impulse sequence $\Phi_c(t)$ consists of a string of L chips with polarities determined by a pseudorandom (or some other type of) code sequence $\sigma(i)$ as shown in FIG. **10d.1**, i.e.,

$$\Phi_c(t) = \gamma_c(t \bmod \delta t) * \sigma(t/\delta t)$$

or equivalently,

$$\Phi_c(t) = \sum_{0 \leq j \leq L} \gamma_c(t - j\delta t) * \sigma(j),$$

where the square brackets around the argument of the pseudorandom code sequence σ indicates the largest integer less than or equal to the argument. Assuming that $\delta t = 2t_0$, the Fourier transform of the transmitted impulse sequence $\Phi_c(t)$ is then given by

$$\begin{aligned} F[\Phi_c(t)] &= \sum_{0 \leq j \leq L} F[\gamma_c(t - j\delta t)] * \sigma(j) \propto \\ &\quad \exp[-\omega^2 d^2 / 16\pi] * \{1 - \exp(i\omega t_0)\} * \left\{ \sum_{0 \leq j \leq L} \sigma(j) \exp(i\omega j\delta t) \right\}. \end{aligned}$$

Therefore, the amplitude of the spectrum of an impulse sequence Φ_c is equal to the amplitude of the spectrum for a single chip γ_c , as shown in FIG. **10b.2**, modulated by the

function $|\Sigma\sigma(j) * \exp(i\omega j\delta t)|$, as shown in FIG. 10d.2. Although the modulation by $|\Sigma \sigma(j) \mathbf{8} \exp(i\omega j\delta t)|$ provides additional structure to the spectrum, the spectrum still has zeroes at multiples of $\omega=2\pi/t_0$ ($f=1/t_0$). As mentioned above, the envelope of the spectrum of the impulse sequence Φ_c is equal to the spectrum of a single impulse $G(t)$, so narrow impulses create an impulse sequence spectrum which is “spread.”

Similarly, if the transmitted impulse sequence $\Phi_c(t)$ consists of a string of chips with impulses separated by t_1 , as shown in FIG. 10f. 1, then the Fourier spectrum is proportional to

$$\exp[-\omega^2 d^2 / 16\pi] * \{1 - \exp(i\omega t_1)\} * \left\{ \sum_{0 \leq j \leq L} \sigma(j) \exp(i\omega j\delta t) \right\}.$$

Therefore, the amplitude of the spectrum of an impulse sequence Φ_c is equal to the amplitude of the spectrum for a single chip γ_{cs} , as shown in FIG. 10e.2, again modulated by the function $|\Sigma \sigma(j) \mathbf{8} \exp(i\omega j\delta t)|$, as shown in FIG. 10f.2. Although the modulation by $|\Sigma \sigma(j) \mathbf{8} \exp(i\omega j\delta t)|$ provides additional structure to the spectrum, the spectrum still has zeroes at multiples of $\omega=2\pi/t_1$ ($f=1/t_1$) and an envelope equal to the spectrum of a single impulse $G(t)$.

Detailed Description of the Discrete-Time Pseudo-Autocorrelation Function

FIG. 11 is a graphical illustration of the discrete-time pseudo-autocorrelation (DTPAC) function of an internally-generated integration sequence $\Phi_i(t)$ and a received impulse sequence $\Phi_c(t)$. For ease of discussion and display, the impulse sequences $\Phi_i(t)$ and $\Phi_c(t)$ each consist of two doublets and the DTPAC function has seventeen bins. As shown in the top graph, from left to right the internally-generated integration sequence $\Phi_i(t)$ consists of a first positive rectangular impulse **1014**, followed immediately by two negative rectangular impulses **1012** and **1016**, following finally by a second positive rectangular impulse **1018**. The rectangular impulses **1012**, **1014**, **1016** and **1018** each have the same shape, i.e., the same width and magnitude. For convenience it will be assumed in the following discussion of FIG. 11 that the absolute value of the magnitude of the impulses **1014**, **1012**, **1016** and **1018** is unity. The internally-generated integration sequence $\Phi_i(t)$ may be viewed as a pair of doublets—the first doublet **1013** consisting of the first positive and negative impulses **1014** and **1012**, and the second doublet **1017** consisting of the second negative and positive impulses **1016** and **1018**. The second doublet **1017** has a polarity opposite that of the first doublet **1013**, i.e., $\sigma_f(1)=+1$ and $\sigma_f(2)=-1$.

Similarly, as shown in the second graph from the top, from left to right the received signal $\Phi_c(t)$ consists of four equally spaced Gaussian impulses: a first positive Gaussian impulse **1024**, followed by two negative Gaussian impulses **1022** and **1026**, following finally by a second positive Gaussian impulse **1028**. The received signal impulses **1022**, **1024**, **1026** and **1028** each have the same shape, i.e., the same width and magnitude. The received impulse sequence $\Phi_c(t)$ may also be viewed as a pair of doublets, the first doublet **1023** consisting of the first positive and negative impulses **1024** and **1022**, and the second doublet **1027** consisting of the second negative and positive impulses **1026** and **1028**. The second doublet **1027** has a polarity opposite the first doublet **1023**, i.e., $\sigma_r(1)=+1$ and $\sigma_r(2)=-1$. For convenience it will be assumed in the following discussion of FIG. 11 that the absolute value of the area under each of the impulses **1024**, **1022**, **1026** and **1028** is unity.

As discussed above (and in detail below), the internally-generated integration sequence $\Phi_i(t)$ is delayed by a chain of flip-flops **1460** in the time-integrating correlator **114** to provide a time-delayed integration sequence $\Phi_i^{(n)}(t)$ to the n^{th} integrator **1430**. The received signal $\Phi_c(t)$ is not delayed. The n^{th} bin value of the DTPAC function $\Lambda(n)$ shown in the top right graph of FIG. 11 is equal to the integral of the product of received signal $\Phi_c(t)$ and the n^{th} time-delayed integration sequence $\Phi_i^{(n)}(t)$. The zeroth bin ($n=0$) value of the DTPAC function, $\Lambda(0)$, is shown as zero, and corresponds to the product of a delayed internally-generated integration sequence $\Phi_i(t)$ and a received signal $\Phi_c(t)$ where there is no overlap of nonzero portions of the signals $\Phi_i(t)$ and $\Phi_c(t)$. The $n=1$ bin of the DTPAC function, $\Lambda(1)$, has a small positive value and corresponds to the product of the delayed internally-generated integration sequence $\Phi_i^{(1)}(t)$ and the received signal $\Phi_c(t)$ where there is a partial overlap of the last positive impulse **1018** of the delayed integration sequence $\Phi_i^{(1)}(t)$ and the first positive impulse **1024** of the received signal $\Phi_c(t)$. Similarly, the $n=2$ bin of the DTPAC function, $\Lambda(2)$, has a positive value of unity since it is equal to the product of a delayed integration sequence $\Phi_i^{(2)}(t)$ and the received signal $\Phi_c(t)$ where there is a complete overlap of the last positive impulse **1018** of the delayed integration sequence $\Phi_i^{(2)}(t)$ and the first positive impulse **1024** of the received signal $\Phi_c(t)$. The DTPAC function Λ changes sign in the $n=3$ bin, since it is equal to the product of the delayed integration sequence $\Phi_i^{(3)}(t)$ and the received signal $\Phi_c(t)$ where there is a partial overlap of the last positive impulse **1018** of the delayed integration sequence $\Phi_i^{(3)}(t)$ with the first negative impulse **1022** of the received signal $\Phi_c(t)$, and the first positive impulse **1024** of the received signal $\Phi_c(t)$ overlaps equally with both the last positive impulse **1018** and the last negative impulse **1016** of the delayed integration sequence $\Phi_i^{(3)}(t)$.

The DTPAC function $\Lambda(n)$ again changes sign between the sixth and seventh bins and reaches a maximum value of four in the eighth bin. In the eighth bin the value of the DTPAC function $\Lambda(8)$ corresponds to the product of the delayed integration sequence $\Phi_i^{(8)}(t)$ and the received signal $\Phi_c(t)$ where both positive impulses **1014** and **1018** of the delayed integration sequence $\Phi_i^{(8)}(t)$ overlap completely with both positive impulses **1024** and **1028** of the received signal $\Phi_c(t)$, and both negative impulses **1012** and **1016** of the delayed integration sequence $\Phi_i(t)$ overlap completely with both negative impulses **1022** and **1026** of the received signal $\Phi_c(t)$. When the received signal $\Phi_c(t)$ and the integration sequence $\Phi_i(t)$ are based on the same pseudorandom code sequence $\sigma(i)$, as is the case in FIG. 11, then the maximum value of the DTPAC function Λ is equal to the number of impulses in the signals (again assuming that the absolute values of the magnitude of the impulses in the integration sequence $\Phi_i(t)$ and the area of the impulses in the received signal $\Phi_c(t)$ are equal to unity). As discussed in the Overview, the pseudo-autocorrelation function $\Lambda(t)$ is symmetric about the maximum value when the received signal $\Phi_c(t)$ and the integration sequence $\Phi_i(t)$ are based on the same pseudorandom code sequence $\sigma(i)$. Therefore, if the central bin of the DTPAC function $\Lambda(n)$ is perfectly centered to coincide with the maximum of the pseudo-autocorrelation function $\Lambda(t)$, as appears to be the case in the top righthand graph of FIG. 11, then the DTPAC function $\Lambda(n)$ is symmetric about the central bin ($n=8$). In general, for longer code sequences the DTPAC function $\Lambda(n)$ will exhibit characteristics similar to the DTPAC function $\Lambda(n)$ of FIG. 11. For instance, all DTPAC functions $\Lambda(n)$ have a central maximum value, and oscillate in sign and decay to zero away from the maximum.

FIGS. 12 and 13 illustrate the sensitivity of the DTPAC function $\Lambda(n)$ to small shifts in the bins relative to the received signal $\Phi_c(t)$, when the time spacing between bins is of the order of one quarter of the chip length δt , i.e., half the width of central peak of the pseudo-autocorrelation function. (As mentioned in the Overview, although the DTPAC function $\Lambda(n)$ resembles a time sampling of the pseudo-autocorrelation function $\Lambda(t)$, the pseudo-autocorrelation function $\Lambda(t)$ is actually never produced by the circuitry and so it therefore cannot be sampled. However, some insight is provided by viewing the DTPAC function $\Lambda(n)$ as equivalent to a sampling of the pseudo-autocorrelation function $\Lambda(t)$ in the discussion that follows.) Top left graph 1100 of FIG. 12 shows a simple pseudo-autocorrelation function $\Lambda(t)$ (in general, a pseudo-autocorrelation function will have other minima and maxima, though there will always be a large central peak) and a series of equally spaced bin times 1101, 1102, . . . 1109, represented as sharp impulses, separated by 2.5 nanoseconds. The pseudo-autocorrelation function $\Lambda(t)$ has a central positive peak 2198 with surrounding negative peaks 2197 and 2196 of a smaller magnitude. In the top left graph 1100 the central bin 1105 is centered in the central peak 2198—this is termed a 0-phase delay.

The sampling by the central bin 1105 of the center of the central peak 2198 of the pseudo-autocorrelation function $\Lambda(t)$ provides a large positive value 1115 in the DTPAC function $\Lambda(n)$ 2110 shown in the top right graph 1110. The samplings by the bins 1104 and 1106 surrounding the central bin 1105 at times of -2.5 nanoseconds and $+2.5$ nanoseconds where the pseudo-autocorrelation function $\Lambda(t)$ has small positive values (and large positive and negative derivatives), provides small positive values of the DTPAC function $\Lambda(n)$ 2110 in the bins 1114 and 1116 on both sides of the central bin 1115. The samplings by the bins 1103 and 1107 at times of -5.0 nanoseconds and $+5.0$ nanoseconds well-centered in the negative peaks 2196 and 2197 of the pseudo-autocorrelation function $\Lambda(t)$, respectively, provides negative values of the DTPAC function 2110 in the bins 1113 and 1117. Similarly, the other time bins 1101, 1102, 1108 and 1109 sample the pseudo-autocorrelation function $\Lambda(t)$ at time positions farther from the central peak 2198 and provide bin values 1111, 1112, 1118 and 1119 corresponding to the values of the pseudo-autocorrelation function $\Lambda(t)$.

The lefthand graph in the second row from the top 1120 shows the pseudo-autocorrelation function $\Lambda(t)$, and the bins 1121 through 1128 shifted by 0.5 nanoseconds from the positions of the bins 1101 through 1109 shown in the preceding lefthand graph 1100. Because the spacing between bins is 2.5 nanoseconds, this is termed a $1/5$ -phase delay. The position of the central bin 1125 is offset by 0.5 nanoseconds from the center of the central peak 2198 of the pseudo-autocorrelation function $\Lambda(t)$. However, since the central peak 2198 is substantially flat at the top, the central value 1135 of the DTPAC function $\Lambda(n)$ 2130 in the second righthand graph is approximately the same as the central value 1115 of the DTPAC function $\Lambda(n)$ 1115 when the central bin 1105 is exactly centered in the central peak 2198. The bin 1126 immediately to the right of the central bin 1125 is now located in the righthand negative peak 2197, to the right of the zero-crossing of the pseudo-autocorrelation function $\Lambda(t)$. Therefore, the value of the DTPAC function $\Lambda(n)$ 2130 in the bin 1136 immediately to the right of the central bin 1135 is now negative. Furthermore, the bin 1124 immediately to the left of the central bin 1125 is now located well within the central peak 2198 of the pseudo-autocorrelation function $\Lambda(t)$. Therefore, the value of the DTPAC function $\Lambda(n)$ 2130 in the bin 1134 immediately to

the left of the central bin 1135 is now large and positive. A comparison of the DTPAC function $\Lambda(n)$ 2130 of graph 1130 and the DTPAC function $\Lambda(n)$ 2110 of the preceding graph 1110 shows that a substantial change in the shape of the functions occurs. In general, when the time between bins Δt is on the order of one-quarter of a chip length δt the values of the DTPAC function in bins of a first parity (e.g., odd bins) change significantly while the values of the DTPAC function in bins of a second parity (e.g., even bins) remain relatively stable for small time shifts from when a bin is centered at the peak of the pseudo-autocorrelation functions. Thus, the even bins describe the stable shape of the DTPAC function, while the sensitivity of the odd bins can be used to determine slight changes in the arrival time. Because the even bins are relatively stable, they can be used to calculate the gain of the input amplifier 105.

Similarly, the subsequent graphs 1140, 1160, and 1180 show $2/5$ -, $3/5$ -, and $4/5$ -phase delays, i.e., the bins are shifted by 1.0 nanoseconds, 1.5 nanoseconds and 2.0 nanoseconds from the case shown in the first graph 1100 where the central bin 1105 is centered in the central peak 2198 of the pseudo-autocorrelation function $\Lambda(t)$ respectively. Because the pseudo-autocorrelation function $\Lambda(t)$ is evenly symmetric and the bins are uniformly spaced, the DTPAC function $\Lambda(n)$ 2130 for a $1/5$ -phase delay is equal to the time-reversed DTPAC function $\Lambda(n)$ 2190 for a $4/5$ -phase delay. Similarly, the DTPAC $\Lambda(n)$ function 2150 for a $2/5$ -phase delay is equal to the time-reversed DTPAC function $\Lambda(n)$ 2170 for a $3/5$ -phase delay. In general, if a pseudo-autocorrelation function $\Lambda(t)$ is evenly symmetric and the bins are uniformly spaced, then the DTPAC function $\Lambda(n)$ for a θ -phase delay is equal to the time-reversed DTPAC function $\Lambda(n)$ for a $(1-\theta)$ -phase delay.

FIG. 13 illustrates that the central region of the DTPAC function $\Lambda(n)$ near the 0-phase delay is highly sensitive to small shifts in the locations of the bins since the bins 1104 and 1106 surrounding the central bin 1105 are located where the pseudo-autocorrelation function $\Lambda(t)$ has small values and large magnitude derivatives. For clarity, graphs 1100 and 1110 from FIG. 12 are reproduced in FIG. 13. The lefthand graph in the second row 1220 shows the pseudo-autocorrelation function $\Lambda(t)$ with the bins 1221 through 1228 shifted by 0.1 nanoseconds from the positions of the bins 1101 through 1109 shown in the top lefthand graph 1100. Because the spacing between bins is 2.5 nanoseconds, this is a $1/25$ -phase delay. The position of the central bin 1225 is offset by 0.1 nanoseconds from the center of the central peak 2198 of the pseudo-autocorrelation function $\Lambda(t)$. However, since the central peak 2198 is substantially flat at the top, the central value 1235 of the DTPAC function $\Lambda(n)$ 2230 is approximately the same as the central value 1115 of the DTPAC function $\Lambda(n)$ 1110 when the central bin 1105 is exactly centered in the central peak 2198. Also, the bin 1126 immediately to the right of the central bin 1125 is now located where the central peak 2198 has a small positive value. Therefore, the value of the DTPAC function $\Lambda(n)$ 2230 in the bin 1236 immediately to the right of the central bin 1235 is smaller than in the previous figure 1110. Furthermore, the bin 1224 immediately to the left of the central bin 1225 is located closer to the center of the central peak 2198 of the pseudo-autocorrelation function $\Lambda(t)$. Therefore, the value of the DTPAC function $\Lambda(n)$ 2230 in the bin 1234 immediately to the left of the central bin 1235 is larger than in the previous figure 1110. A comparison of the DTPAC function $\Lambda(n)$ 2230 of the second-from-the-top-righthand graph 1230 and the DTPAC function $\Lambda(n)$ 2110 of the top right graph 1110 shows that a substantial change in

the shape of the DTPAC functions $\Lambda(n)$ **2110** and **2230** occurs for a small change in the positions of the bins **1101–1109** and **1221–1229**.

Similarly, the lefthand graph in the middle row **1240** of FIG. **13** shows the pseudo-autocorrelation function $\Lambda(t)$ with the bins shifted by 0.2 nanoseconds from the positions of the bins **1101** through **1109** shown in the top graph **1100**. Because the spacing between bins is 2.5 nanoseconds, this is a $\frac{2}{25}$ -phase delay. Since the central peak **2198** is flat at the top, the central value **1255** of the DTPAC function $\Lambda(n)$ **2250** is approximately the same as the central value **1115** of the DTPAC function $\Lambda(n)$ **2110** when the central bin **1105** is exactly centered in the central peak **2198**. However, the bin **1246** immediately to the right of the central bin **1245** is now located just within the righthand negative peak **2197**, and therefore the value of the DTPAC function $\Lambda(n)$ **2250** in the bin **1256** immediately to the right of the central bin **1255** is small and negative. The bin **1244** immediately to the left of the central bin **1245** is located still closer to the center of the central peak **2198** of the pseudo-autocorrelation function $\Lambda(t)$. Therefore, the value of the DTPAC function $\Lambda(n)$ **2250** in the bin **1254** immediately to the left of the central bin **1255** is larger than in the graph **1230** immediately above. Again, a comparison of the DTPAC function $\Lambda(n)$ **2250** of the middle-row righthand graph **1250** and 0-phase delay DTPAC function $\Lambda(n)$ **2110** in the top righthand graph **1110** shows that a substantial change in the shape of the DTPAC functions $\Lambda(n)$ **2110** and **2250** occurs for a small change in the positions of the bins **1101–1109** and **1241–1249**.

The subsequent graphs **1240** and **1260** show $\frac{3}{25}$ - and $\frac{4}{25}$ -phase delays, i.e., the bins are shifted by 0.3 and 0.4 nanoseconds from the case shown in the first graph **1100** where the central bin **1105** is centered in the central peak **2198** of the pseudo-autocorrelation function $\Lambda(t)$. The bottom lefthand graph **1280** shown in FIG. **13** is a $\frac{1}{5}$ -phase delay, and is equivalent to the lefthand second-from-the-top graph **1120** in FIG. **12**.

In the preferred embodiment a neural network included in software in the processor **140** or in hardware (not shown) is utilized to differentiate between different patterns formed by the DTPAC function $\Lambda(n)$, to thereby determine the time of arrival of received communications $\Phi_c(t)$. The sensitivity of the shape of the DTPAC function $\Lambda(n)$ to small time shifts of the bins has been discussed in relation to the sampling of the central peak **2198** of the pseudo-autocorrelation function $\Lambda(t)$. However, it should be noted that the same type of argument may be applied to all of the peaks in the pseudo-autocorrelation function $\Lambda(t)$, since all of the peaks have similar shapes and approximately the same width as the central peak **2198**. As mentioned above, it should also be noted that when the spacing between bins Δt is approximately equal to one-quarter of a chip length δt then DTPAC values for bins of a first parity will change much faster than DTPAC values $\Lambda(n)$ for bins of a second parity when a bin of the first parity is well-centered in the peak of the pseudo-autocorrelation function $\Lambda(t)$.

Detailed Description of Bin Times and Integration Functions

As mentioned above, different relationships between the internally-generated doublet functions $\gamma_i(t)$ and the bin time Δt provide different advantages. The relationship between the bin time Δt and the internally-generated doublets $\gamma_i(t)$ for the preferred embodiment of the time-integrating correlator **114** and the receiver code-sequence generator **118** is depicted in the timing chart of FIG. **14a**. As shown in FIG. **14a**, and as will be mentioned in the detailed discussion of the receiver code generator **117** of FIG. **17**, a divide-by-two counter **1712** produces a half-speed clock signal HSClock

with a time between clock ticks equal to twice the time between clock ticks t_c of the system clock signal DClock. Also, the value of the integration sequence $\Phi_i(t)$ can change once per tick of the system clock DClock, i.e., on the rising edge of the DClock signal. The internally-generated doublet function $\gamma_i(t)$ consists of a series of doublets, the second value of each doublet being different from the first value. Ignoring the transient features of the signal, i.e., the time for the signal to change in value, the doublet waveform $\gamma_i(t)$ is

$$\gamma_i(t) = +1 \quad 0 < t < t_c$$

$$\gamma_i(t) = -1 \quad t_c < t < 2t_c.$$

An exemplary integration sequence $\Phi_i(t)$ depicted in FIG. **14a** consists of a first doublet of positive polarity (having a positive impulse followed by a negative impulse), followed by another doublet of positive polarity, and then a doublet of negative polarity. However, the actual values of the integration sequence $\Phi_i(t)$ are immaterial; only the times at which the values of the integration sequence $\Phi_i(t)$ change are relevant to the present discussion.

The system described above is designed for reception of a received signal $\Phi_c(t)$ consisting of a string of chips $\gamma_c(t)$ having a chip length δt equal to the chip length of the internally-generated chips $\gamma_i(t)$, as shown in FIG. **14a**. The received signal $\Phi_c(t)$ always consists of a sequence of impulse doublets; the second impulse of each doublet having an opposite polarity to that of the first impulse. The exemplary received signal $\Phi_c(t)$ shown in FIG. **14a** also consists of a first doublet of positive polarity (having a positive impulse followed by a negative impulse), followed by another doublet of positive polarity, and then a doublet of negative polarity (having a negative pulse followed by a positive pulse). However, the actual values of the exemplary received signal $\Phi_c(t)$ are immaterial; only the separation between the impulses is relevant to the present discussion. The length of time between the midpoints of impulses in the received signal $\Phi_c(t)$ and the integration sequence $\Phi_i(t)$ is the same. As discussed above, this insures a nonzero correlation between the received signal $\Phi_c(t)$ and the integration sequence $\Phi_i(t)$ when they are based on the same pseudorandom code sequence $\sigma(i)$. The integral as a function of time for the product of the integration sequence $\Phi_i(t)$ at the n th correlator and the received signal $\Phi_c(t)$ is also shown in FIG. **14a**, where

$$\text{Integral} = \int_0^T \Phi_c(\tau) * \Phi_i(\tau) d\tau.$$

Because the pseudorandom code sequence $\sigma(i)$ is the same for both signals $\Phi_i(t)$ and $\Phi_c(t)$ in FIG. **14a**, the integral exhibits an increase in value when the received signal $\Phi_c(t)$ is nonzero, and is constant when the received signal $\Phi_c(t)$ is zero.

As will be discussed below in the discussion of the time-integrating correlator **114**, in general the integration sequence $\Phi_i^{(n+1)}(t)$ directed to the $(n+1)^{\text{th}}$ integrator **1430** is delayed by $t_c/2$ (half a tick of the system clock DClock) from the integration sequence $\Phi_i^{(n)}(t)$ directed to the n^{th} integrator **1430**, as shown in FIG. **14a**, i.e., the bin time Δt is $t_c/2$. Since the length of the reception window ΔT_w is equal to the bin time Δt times the number N of integrators, in this case $\Delta T_w = N t_c/2$.

The relation between the bin time Δt and the functional form of the internally-generated chips $\gamma_i(t)$ of the preferred

embodiment, as shown in FIG. 14a, is well-suited for the accurate determination of the arrival time of communications once an approximate arrival time has been determined. The integrator 1430 which receives a delayed integration sequence $\Phi_i(t)$ which begins closest to the time of arrival of the received chip sequence $\Phi_c(t)$ produces the largest output signal. This integrator 1430 is termed the “peak integrator.” In FIG. 14a the n^{th} integrator is the peak integrator since the polarity of each peak in the received chip sequence $\Phi_c(t)$ is the same as the polarity of each impulse in the integration sequence $\Phi_i^{(n)}(t)$ which occurs at the same time. The integration sequence $\Phi_i^{(n+1)}(t)$ from the $(n+1)^{\text{th}}$ integrator 1430 is shifted forward by one quarter of a chip length δt (which in this case is equal to half the time t_c between ticks from the system clock DClock) from that of the peak integrator 1430, producing a significant change in the overlap of the impulses in the integration sequence $\Phi_i(t)$ and the received chip sequence $\Phi_c(t)$. Therefore, the width of the peak of the pseudo-autocorrelation function is approximately equal to the bin time $\Delta t (= \delta t/4)$. As discussed above, when this is the case the bin values on either side of the peak value change extremely rapidly, with time shifts between the received chip sequence $\Phi_c(t)$ and the integration sequence $\Phi_i(t)$, providing a sensitive indicator of the displacement between the beginning times of the received sequence $\Phi_c(t)$ and the integration sequence $\Phi_i(t)$. Therefore, the bin time Δt of $\delta t/4$ in this embodiment provides a means for accurately determining the arrival time of communications.

A first alternate embodiment of the relationship between the internally-generated chip function $\gamma_i(t)$ and the bin times Δt (i.e., the time delays of the integration sequence $\Phi_i(t)$ to the integrators 1430) is depicted in FIG. 14b. It should be noted that the circuitry necessary to implement these relationships, although not explicitly depicted by the circuitry figures and discussed in the present specification, would be apparent to one skilled in the art as modifications of the circuitry presented herein. As in the previous embodiment, in this alternate embodiment the time delay between the integration sequence $\Phi_i^{(n)}(t)$ directed to the n^{th} integrator 1430 and the integration sequence $\Phi_i^{(n+1)}(t)$ directed to $(n+1)^{\text{th}}$ integrator 1430 is one quarter of the time length δt of a chip, i.e., one half of the time t_c between ticks of the system clock DClock. Ignoring transients, in this alternate embodiment the internally-generated chip waveform $\gamma_i(t)$ is

$$\begin{aligned} \gamma_i(t) &= +1 & 0 < t < \delta t/4 \\ \gamma_i(t) &= -1 & \delta t/2 < t < 3\delta t/4 \\ \gamma_i(t) &= 0 & \text{otherwise.} \end{aligned}$$

The internally-generated chip function $\gamma_i(t)$ consists of two square pulses and resembles a clipped version of the externally-generated chip function $\gamma_c(t)$. The received externally-generated chip sequence $\Phi_c(t)$ and the integration sequences $\Phi_i^{(n)}$ and $\Phi_i^{(n+1)}$ are depicted in FIG. 14b as a sequence of three chips, the first two chips having a positive polarity and the third chip having a negative polarity. In addition, the received chip sequence $\Phi_c(t)$ is depicted as having noise superimposed on the signal. The integral as a function of time for the product of the integration sequence $\Phi_i(t)$ at the n^{th} correlator and the received signal $\Phi_c(t)$ is also shown in FIG. 14b, where

$$\text{Integral} = \int_0^n \Phi_c(\tau) * \Phi_i(\tau) d\tau.$$

The integral changes in value when the integration sequence $\Phi_i(t)$ is nonzero. However, the integral is constant when the integration sequence $\Phi_i(t)$ is zero so that noise from the received signal $\Phi_c(t)$ during these periods does not perturb the value of the integral. Because the pseudorandom code sequence $\alpha(i)$ is the same for both the integration sequence $\Phi_i(t)$ and the received signal $\Phi_c(t)$ in FIG. 14b, each impulse in the received signal $\Phi_c(t)$ produces an increase in the value of the integral.

An advantage of the internally-generated chip function $\gamma_i(t)$ of FIG. 14b is that this alternate embodiment provides a higher signal-to-noise ratio than the embodiment of FIG. 14a. This is due to the fact that for the peak integrator the relatively noisy regions between the impulses of the received chip sequence $\Phi_c(t)$ do not contribute to the integral since the integration signal $\Phi_i(t)$ is zero over most of these regions.

As is shown in FIG. 14b, the n^{th} integrator 1430 is the peak integrator since the locations of the positive and negative pulses of the integration sequence $\Phi_i^{(n)}(t)$ and the externally-generated chip sequence $\Phi_c(t)$ coincide. The integration sequence $\Phi_i^{(n+1)}(t)$ supplied to the $(n+1)^{\text{th}}$ integrator 1430 is shifted forward by one quarter of a chip length δt (which in this case is equal to half the time t_c between ticks from the system clock DClock) from that of the peak integrator 1430, i.e., the bin time Δt is $\Delta t/4$. The output from the $(n+1)^{\text{th}}$ integrator 1430 will be small since the pulses of the integration signal $\Phi_i^{(n+1)}(t)$ occur in-between the impulses of the externally-generated chip sequence $\Phi_c(t)$. Therefore, the width of the peak of the pseudo-autocorrelation function is again approximately twice the bin time Δt . In contrast with the previous embodiment, in this case the outputs of the $(n+1)^{\text{th}}$ and $(n-1)^{\text{th}}$ integrators 1430 to either side of the peak integrator 1430 (the n^{th} integrator) are near zero and are relatively insensitive to a shift in the arrival time of the externally-generated chip sequence $\Phi_c(t)$. This embodiment is therefore less useful for accurate ranging than the previous embodiment. However, because this embodiment is less susceptible to noise, it is well-suited for the transmission of binary information between localizers. (In alternate embodiments the bin spacing Δt is not fixed at a value exactly equal to one quarter of a chip length δt . For instance, the bin spacing Δt could vary between a value approximately equal to the width of an impulse and less than one quarter of the chip length δt).

A second alternate embodiment of the relationship between the internally-generated chip function $\gamma_i(t)$ and the time delays of the integration sequence $\Phi_i(t)$ to the integrators 1430 is depicted in FIG. 14c. It should again be noted that the circuitry necessary to implement these relationships, although not explicitly depicted by the circuitry figures and discussed in the present specification, would be apparent to one skilled in the art as modifications of the circuitry presented herein. Ignoring transients, in this alternate embodiment the internally-generated chip function $\gamma_i(t)$ is the same as in the preferred embodiment, i.e.,

$$\begin{aligned} \gamma_i(t) &= +1 & 0 < t < \delta t/2 \\ \gamma_i(t) &= -1 & \delta t/2 < t < \delta t. \end{aligned}$$

The externally-generated chip sequence $\Phi_c(t)$ and the integration sequences $\Phi_i^{(n)}(t)$ and $\Phi_i^{(n+1)}(t)$ are depicted in FIG.

14c as a sequence of three chips γ_c , the first two chips having a positive polarity and the third chip having a negative polarity.

The n^{th} integrator 1430 is the peak integrator since the locations of the positive and negative impulses of the integration sequence $\Phi_i^{(n)}(t)$ and the externally-generated chip sequence $\Phi_c(t)$ coincide. The integral as a function of time for the product of the integration sequence $\Phi_i(t)$ at the n th correlator and the received signal $\Phi_r(t)$ is shown in FIG. 14c, where

$$\text{Integral} = \int_0^{\tau} \Phi_c(\tau) * \Phi_i(\tau) d\tau.$$

Because the pseudorandom code sequence $\sigma(i)$ is the same for both signals $\Phi_i(t)$ and $\Phi_c(t)$ in FIG. 14c, the integral exhibits an increase in value when the received signal $\Phi_r(t)$ is nonzero, and is constant when the received signal $\Phi_r(t)$ is zero. The integration sequence $\Phi_i^{(n+1)}(t)$ form the $(n+1)^{\text{th}}$ integrator 1430 is shifted forward by the time t_c between ticks of the system clock DClock (i.e., one half of a chip length δt) from that of the peak integrator 1430, and the output from the $(n+1)^{\text{th}}$ integrator 1430 will be small since there will generally be no correlation between the impulses of the received externally-generated chip sequence $\Phi_c(t)$ and the shifted integration sequence $\Phi_i^{(n+1)}(t)$. As discussed above in reference to the embodiment of FIG. 14a, even a shift of the integration sequence $\Phi_i(t)$ of one quarter of a chip length δt from the peak alignment produces a substantial drop in the correlation of the two signals $\Phi_c(t)$ and $\Phi_i(t)$. As also discussed above, the optimal bin time Δt is approximately half the width of the peak of the pseudo-autocorrelation function. Therefore, this second alternate embodiment cannot determine the actual arrival time of the received chip sequence $\Phi_c(t)$ to the accuracy of the embodiment of FIG. 14a due to the increase in the bin size Δt . However, this alternate embodiment is useful in locating the approximate arrival time of communications, such as the beacon signal of FIG. 8, since the length ΔT_w of the reception window is twice as long as in the embodiment of FIG. 14a. The length of the reception window ΔT_w of this embodiment is equal to the bin time Δt times the number N of integrators, in this case $\Delta T_w = Nt_c$, whereas the length ΔT_w of the reception window for the embodiment of FIG. 14b is $Nt_c/2$.

In alternate embodiments the bin spacing Δt is not fixed at exactly half of a chip length δt , as in FIG. 14c. For instance, the bin spacing Δt could be equal to half the chip length δt minus the rise time (fall time) of the square pulses in the internally-generated chip function $\gamma_c(t)$ to insure that received impulses do not escape detection, since when the bin spacing Δt is exactly equal to half the chip length δt a sharp impulse occurring during the rise time of one internally-generated integration sequence $\Phi_i(t)$ and the fall time of an internally-generated integration sequence $\Phi_i(t)$ form an adjacent bin may escape detection. Detailed Description of the Low-Frequency Real Time Clock

As mentioned above, the real time clock 119 and 120 of the present invention may have as many as five separate stages so as to provide a high-speed low-power clock and an extended timebase. The most-significant bits of the clock are stored and managed by software in an "S4-stage" implemented in the processor 140. The second-most-significant bits of the clock are stored and managed by the low-frequency real time clock 119 shown in detail in FIG. 15. In the preferred embodiment presented in FIG. 15 and dis-

cussed in detail below, the low-frequency real time clock 119 is split into two stages, S3 and S2, and the S2 stage is further split into a standard-logic stage S2A and a low-noise stage S2B. However, in applications where power consumption is not an issue, the S2A and S2B stages may be combined into a single low-noise S2 stage. Furthermore, the S3 and S2 stages may also be combined into a single low-noise stage, though this alternative produces even greater power consumption.

The low-frequency real time clock 119 is responsible for triggering the high-frequency real time clock 120 shortly before a transmission or reception event, and for notifying the processor 140 when a counter 1910 in the S3 stage overflows. To allow the low-frequency real time clock 119 to run continuously, the S2 stage has two counters, an S2A static-CMOS counter 1960 and an S2B low-noise counter 1970. The S2B counter 1970 is designed using low-noise circuitry to produce very little power supply line noise or radio frequency radiation so as to minimize interference with other components of the circuit during transmission and reception events. The S2A counter 1960 is designed using standard CMOS logic, and so the S2A static-CMOS counter 1960 is noisier, but consumes much less power, than the low-noise S2B counter 1970. A selection logic block 1950 in the low-frequency clock 119 determines which of the S2 counters 1960 or 1970 to use, and switches back and forth between the two. The selection logic 1950 uses the signal XtalClock on line 148 from the crystal oscillator 130 for its timing. If one of the linear feedback shift registers 1716 or 1826 in the receiver or transmitter code-sequence generators 117 or 118 is running, the miscellaneous logic block 150 notifies the low-frequency real time clock 119 via a signal on the LSFR-running line 145. The selection logic 1950 supplies the clock signals via output terminals S2AClock and S2BClock on lines 1961 and 1971 to run the S2A and S2B counters 1960 and 1970, respectively. The S2 counters 1960 or 1970 send their terminal count TC signals to the static TC and low-noise TC inputs of the selection logic 1950 on lines 1962 and 1972, respectively. The TC signals are used by the selection logic 1950 to time-switch between the two S2 counters 1960 and 1970, and also to generate the signal on the S3Clock line 1901. The signal on the S3Clock line 1901 goes high for one XtalClock tick whenever one of the S2 clocks 1960 or 1970 produces a terminal count, incrementing an S3 static-CMOS counter 1910 by one. The S3 counter 1910 contains the second most-significant portion of the bits of the real time clock. The CMOS logic of the S3 static counter 1910 only generates power supply line noise and radio frequency noise when it is switching, so selection logic 1950 delays sending the S3Clock signal to the S3 counter 1910 during a transmission or reception event. This allows the S3 counter 1910 to be designed using standard low-power CMOS circuitry. When the S3 counter 1910 overflows, it interrupts the processor 140 via rollover line 154 to inform the processor 140 that it is time to increment the S4 stage of the counter.

A receiver triggering circuit 1930 is used to detect when it is time to trigger the high-frequency clock 120 to start a reception event. Before the reception event, the processor 140 loads an S3 receiver event register 1932 and an S2 receiver event register 1935 via data bus 190 with the appropriate components of the time that the reception event will happen. When the most-significant S4 portion of the reception event time matches the most-significant S4 portion of the counter (not shown) in the processor 140, the processor 140 generates a pulse on the S4RxTrig line 152. At this time, the processor 140 is disabled to prevent it from

producing radio frequency noise. The S4RxTrig signal is directed via line 152 to the S3REnable input of an S3 receiver comparator 1931 and enables the S3 receiver comparator 1931. This comparator 1931 waits until the value from the S3 counter 1910 on an S3 data bus 1902 matches the value in the S3 receiver event register 1932, and then produces a pulse on the S3RxTrig\$ line 1936. This S3RxTrig\$ trigger pulse is latched into a reception flip-flop 1933 to delay the trigger until the next overflow of the S2 static counter 1960 which induces the selection logic 1950 to produce a pulse at the S3 clock output. This delay produced by the flip-flop 1933 gives the selection logic circuit 1950 time to switch to the S2B low-noise counter 1970 before the reception event starts. The software in the processor 140 takes this delay into account when determining the values to load into the S3 receiver event register 1932 and the S2 receiver event register 1935, and loads values that are one count less than the actual times required. For instance, if a reception event is supposed to be triggered when the counters in stages S3 and S2 have values C_3 and C_2 , then the S3 and S2 event registers 1932 and 1935 are loaded with the values (C_3-1) and (C_2-1) . To give the selection logic 1950 ample warning that a switch to the low-noise circuitry will be necessary, the un-delayed S3RxTrig\$ signal from the S3 receiver comparator 1931 is fed to the S3Rx/TxTrig\$ input of the selection logic 1950 via an OR gate 1920. The Q output from the reception flip-flop 1933 then enables an S2 receiver comparator 1934 via line 155. When the value in the S2B low-noise counter 1970 provided on an S2 data bus 1903 matches the value in the S2 receiver event register 1935, the S2 receiver comparator 1934 triggers, generating a pulse on the S2RxTrig\$ line 146 which enables a portion of the high-frequency real time clock 120, as described below. The Q output from the reception flip-flop 1933 is also passed on to the receiver code-sequence generator 117 via RxPower line 155. This gives the receiver code-sequence generator 117 time to turn on low-noise circuits that are currently disabled to conserve power.

A transmitter triggering circuit 1940 operates in a similar fashion to the receiver triggering circuit 1930. This transmitter triggering circuit 1940 is used to detect when it is time to trigger the high-frequency clock 120 to start a transmission event. Before the transmission event, the processor 140 loads an S3 transmitter event register 1942 and an S2 transmitter event register 1945 via data bus 190 with the appropriate components of the time that a transmission event will happen. When the most-significant S4 portion of the transmission event time matches the most-significant S4 portion of the counter (not shown) in the processor 140, the processor 140 generates a pulse on the S4TxTrig line 153. At this time, the processor 140 will be disabled to prevent it from producing power line and radio frequency noise. The S4TxTrig signal enables an S3 transmitter comparator 1941 via its S3TEnable input. The S3 transmitter comparator 1941 produces a pulse on the S3TxTrig\$ line 1946 when the value from the S3 counter 1910 on the S3 data bus 1902 matches the value in the S3 transmitter event register 1942. This S3TxTrig\$ trigger pulse is latched into a reception flip-flop 1943 to delay the trigger until the next overflow of the S2A static counter 1960, which induces the selection logic 1950 to produce a pulse at the S3 clock output. This delay gives the selection logic circuit 1950 time to switch to the S2B low-noise counter 1970 before the transmission event starts. The software in the processor 140 takes this delay into account when determining the values to load into the S3 transmitter event register 1942 and the S2 transmitter event

register 1945, and loads values that are one cycle earlier than the actual times required. For instance, if a transmission event is to be triggered when the counters in stages S3 and S2 have values C_3 and C_2 , then the S3 and S2 event registers 1942 and 1945 are loaded with the values (C_3-1) and (C_2-1) . To give the selection logic 1950 ample warning that a switch to the low-noise circuitry will be necessary, the un-delayed S3TxTrig\$ signal is sent to the S3Rx/TxTrig\$ input of the selection logic 1950 via OR gate 1920. The Q output from the transmission flip-flop 1943 in turn enables an S2 transmitter comparator 1944 via line 138. When the value in the S2B counter 1970 provided on the S2 data bus 1903 matches the value in the S2 transmitter event register 1945, the S2 transmitter comparator 1944 triggers, generating a pulse on the S2TxTrig\$ line 147 which enables a portion of the high-frequency real time clock 120, as described below. The Q output from the transmission flip-flop 1943 is also passed on to the transmitter code-sequence generator 118 via the TxPower line 138. This gives the transmitter code-sequence generator 118 time to turn on low-noise circuits that are currently disabled to conserve power.

Detailed Description of the High-Frequency Real Time Clock

As mentioned above, the real time clock of the present invention has five separate components so as to provide high clock speed and an extended time base. The most-significant bits of the clock are stored and managed by an S4 stage which is implemented as software in the processor 140. The second most-significant bits of the clock are stored and managed in stages S3 and S2 by the low-frequency real time clock 119 described above. The lowest-significant bits of the real time clock are stored and managed in stages S1 and S0 of a high frequency real time clock 120 shown in detail in FIG. 16. During transmission and reception events, this high-frequency real time clock 120 generates the high-speed system clock DClock signal on line 160 that is utilized by the transmitter code-sequence generator 118, the receiver code-sequence generator 117, and the time-integrating correlator 114. The high-frequency real time clock 120 utilizes the low bits of the receiver and transmitter trigger times supplied by the processor 140, trigger transmission and reception events, as described in detail below.

The high-frequency real time clock 120 of FIG. 16 uses a phase-lock loop circuit 2010 to convert the low-speed crystal clock signal XtalClock on line 148 into a high-speed clock signal HClock on line 2099. The high-speed clock HClock only runs internally to the high-frequency clock 120. The components of the phase-lock loop 2010 are activated by the processor 140 via the data bus 190 to the Enable inputs of the components. Because the phase-lock loop circuit 2010 requires a number of cycles to stabilize, the circuit 2010 is enabled by the processor 140 via the processor data bus 190, rather than by the triggering signals S2RxTrig\$ or S2TxTrig\$ from the low-frequency real time clock 119. To maximize the accuracy of the high-frequency clock 120 while minimizing power consumption, the phase-lock loop 2010 is maintained active during the communications in each ranging interaction (lasting on the order of milliseconds), but deactivated between ranging interactions (periods on the order of seconds). The approximately 6.25 MHz crystal clock XtalClock is multiplied by a number, which in the preferred embodiment is thirty-two, by the phase-lock loop 2010 to generate the 200 MHz internal HClock signal. In the phase-lock loop 2010, the HClock signal is divided back down by thirty-two in an S1 low-noise counter 2016 to produce a low-speed clock signal on line

2097. This S1 counter **2016** contains the second-least-significant bits of the real time clock. The low-speed clock signal from the Q-Bar output of the S1 counter **2016** on line **2097** is compared with the crystal clock signal XtalClock in a phase/frequency detector **2012**. If the low-speed clock on line **2097** is too slow, the phase/frequency detector **2012** produces a pulse on its UP output. The length of this pulse will be equal to the time difference between when a transition happens on the crystal clock XtalClock on line **148** and when the late transition occurs on the low-speed clock on line **2097**. If the low-speed clock on line **2097** is too fast, the phase/frequency detector **2012** produces an impulse on its DOWN output. In this case, the length of the impulse is equal to the time difference between a transition on the early low-speed clock on line **2097** and a transition on the crystal clock XtalClock on line **148**. The UP/DOWN error signals are used by a type-II operation charge pump and loop filter **2014** to produce a voltage on output line **2015** proportional to the integral of the UP/DOWN error signals from the phase/frequency detector **2012**. This voltage on line **2015** is used in turn by a voltage controlled oscillator **2018** to generate the internal high-speed clock signal HClock on line **2099**. This HClock signal feeds back into the S1 counter **2016** to complete the loop.

An S1 receiver triggering circuit **2020** generates reset and clock signals for a receive event. This receiver trigger **2020** is enabled by the S2RxTrig\$ signal on line **146** from the low-frequency real time clock **119**. The S2RxTrig\$ signal is synchronous with the crystal clock XtalClock (since the crystal clock XtalClock is also the clock signal for the low-frequency clock **119**), but may arrive slightly early or late with respect to the low-speed clock from the S1 counter **2016** due to phase shifts produced by the phase-lock loop **2010**. To correct for any phase error between the S2RxTrig\$ signal and the low-speed clock signal on line **2097**, a first receiver flip-flop **2022** samples S2RxTrig\$ half way through a cycle by using the inverted low-speed clock signal from the Q output of the S1 counter **2016** on line **2096**. The output from the first receiver flip-flop **2022** is then sampled with the low-speed clock signal from the Q-bar output of the S1 counter **2016** by a second receiver flip-flop **2024**. The output from the second receiver flip-flop **2024** is used to enable an S1 receiver comparator **2026**. Before a reception event, the processor **140** loads an S1 event register **2028** via data bus **190** with the second-least-significant bits of the reception event time. The receiver comparator **2026** compares the output from the S1 counter **2016** with the value in the S1 event register **2028**, and produces a high signal at its RecEqual output when the two values match. A third receiver flip-flop **2023** latches the RecEqual output of the S1 comparator **2028** to produce a clean pulse as the S1RxTrig signal on line **2095**. The S1RxTrig signal causes a receiver SR flip-flop **2027** to be set. This receiver SR flip-flop **2027** will stay on for the duration of the reception event.

When a reception event is complete, the time-integrating correlator **114** sends a RxStop signal on line **142** to the high frequency clock **120**. This signal is synchronous with the system clock DClock, but may not be in phase with the internal clock HClock. To bring the RxStop signal into synchronization with the internal clock HClock, a receiver synchronizing flip-flop **2025** latches the RxStop signal to produce a pulse at its Q output synchronized with one of the HClock pulses. The output from receiver synchronizing flip-flop **2025** is directed to the reset input R of the receiver SR flip-flop **2027** to reset it, producing a low value at the Q output. Since the Q output from the transmitter SR flip-flop **2037** is also low (as will be discussed below), the output of

the NOR gate **2044** goes high, so as to turn on the WReset signal on line **170** when the receiver event is done. When the output of the NOR gate **2044** goes high, this forces the output of the OR gate **2049** directed to the programmable delay **2050** to also go high, thereby preventing any transitions of the system clock DClock. The asserted S1RxTrig signal on line **2095** is also used to set a selection flip-flop **2042**. The output of this selection flip-flop **2042** on line **2092** is used to select one of the S0 event registers **2046** and **2047**, as described below.

An S1 transmitter triggering circuit **2030** operates in a similar fashion to the S1 receiver triggering circuit **2020**. This transmitter trigger **2030** is enabled by the S2TxTrig\$ signal on line **147** from the low-frequency real time clock **119**. The S2TxTrig\$ signal is synchronous with the crystal clock XtalClock, but may arrive slightly early or late with respect to the low-speed clock signal on line **2097** from the S1 counter **2016** due to phase shifts produced by the phase-lock loop **2010**. To allow for any phase error between the S2TxTrig\$ signal and the low-speed clock signal on line **2097**, a first transmitter flip-flop **2032** samples S2TxTrig\$ half way through a cycle by using the inverted low-speed clock from the Q output of the S1 counter **2016** on line **2096**. The output from the first transmitter flip-flop **2032** is then sampled with the low-speed clock signal on line **2097** by a second transmitter flip-flop **2034**. The output from the second transmitter trigger flip-flop **2034** is used to enable an S1 transmitter comparator **2036**. Before a transmission event, the processor **140** loads a transmitter S1 event register **2038** with the second-least-significant bits of the transmission event time. The transmitter comparator **2036** compares the output from the S1 counter **2016** with the value in the S1 Event register **2038**, and produces a high signal at its TrnEqual output when the two values match. A third transmitter flip-flop **2033** latches the TrnEqual output of the S1 comparator **2036** to produce a clean pulse as the S1RxTrig signal on line **2094**. The S1TxTrig signal causes a transmitter SR flip-flop **2037** to be set. This transmitter SR flip-flop **2037** will stay on for the duration of the transmission event.

When the transmission event is complete, the transmitter code-sequence generator **118** sends a TxStop signal on line **137** to the high-frequency clock **120**. The TxStop signal is synchronous with the system clock DClock, but may not be in phase with the internal clock HClock. To bring the TxStop signal into synchronization with the internal clock HClock, transmitter synchronizing flip-flop **2035** latches the TxStop signal to produce a pulse at its Q output synchronized to one of the HClock pulses. The output from transmitter synchronizing flip-flop **2035** is directed to the reset input R of the transmitter SR flip-flop **2037** to reset it, producing a low value at the Q output. Since the Q output from the receiver SR flip-flop **2027** is also low (as discussed above), the output of the NOR gate **2044** goes high, so as to turn on the WReset signal on line **170** when the transmitter event is done. When the output of the NOR gate **2044** goes high, this forces the output of the OR gate **2049** directed to the programmable delay **2050** to also go high, thereby preventing any transitions of the system clock DClock. The asserted S1TxTrig signal on line **2094** is also used to reset a selection flip-flop **2042**. The output of this selection flip-flop **2042** on line **2092** is used to select one of the S0 event registers **2046** and **2047**, as described below.

The outputs from the receiver SR flip-flop **2027** and the transmitter SR flip-flop **2037** are combined in a NOR gate **2044** to produce the WReset signal on line **170**. The WReset signal remains high between transmitter and receiver events, and goes low only for the duration of a transmission or

reception event. The RxStop signal on line 142 from the time-integrating correlator 114 and the TxStop signal on line 137 from the transmitter code-sequence generator 117 are used by the high-frequency real time clock 120 to terminate a reception or transmission event, respectively, and assert the WReset signal on line 170. As discussed above, OR gate 2049 uses the WReset signal to enable or disable the HClock signal into an S0 programmable delay generator 2050. Between transmission and reception events, the WReset signal is high, causing the OR gate 2049 to produce a continuous high signal, masking out the HClock signal to the IN input of the S0 programmable delay generator 2050. During a transmitter or receiver event, the WReset signal on line 170 goes low, and OR gate 2049 allows the internal clock HClock signal to pass through to the S0 programmable delay generator 2050.

The S0 programmable delay generator 2050 implements a time shift smaller than the time between the ticks of the internal clock HClock, and so is equivalent to the least-significant bits of the real time clock. Because the internal clock HClock is a 200 MHz signal, the S1 counter 2016 can only time events to the nearest 5 nanoseconds, and this only allows the measurement of distances to the nearest 1.5 meters. To achieve a greater time accuracy, the S0 delay generator 2050 shifts the phase of the internal clock HClock to produce a system clock signal DClock on line 160 aligned to the nearest 30 picoseconds. This level of time accuracy allows for distance measurements to the nearest centimeter. The processor 140 loads a delay via data bus 190 into an S0 transmitter delay unit 2046 or an S0 receiver delay unit 2047 before each transmission or reception event, respectively. The signal on line 2092 from select flip-flop 2042 is directed to the select input of a multiplexer 2048 to select which delay the multiplexer 2048 will pass through to the S0 delay generator 2050. During a receiver event when the signal on line 2092 is high, the multiplexer 2048 selects the value in the S0 receiver delay 2047. During a transmitter event when the signal on line 2092 is low, the multiplexer 2048 selects the value in the S0 transmitter delay 2046.

FIG. 16 shows the S0 Programmable delay generator 2050 as a separate component from the phased locked loop 2010. However, there are other ways to implement the programmable delay, including implementing the voltage controlled oscillator 2019 in the phased lock loop 2010 as a ring oscillator. In this case, an S0 delay generator could be implemented as a multiplexer that selects one of the taps off of the ring oscillator.

Detailed Description of the Receiver Code-Sequence Generator

A receiver code-sequence generator 117 according to the present invention is shown in detail in FIG. 17a. During a receiver event, this circuit generates a code sequence $\sigma(i)$ from parameters initialized by the processor 140 via data bus 190. The code sequence $\sigma(i)$, a string of single bits, is converted into a two-bit reception command sequence consisting of Code0 on output line 132 and Code1 on output line 133. These commands provide a series of instructions to the integrators 1430 of the time-integrating correlator 114. The following table shows the meanings of the two-bit commands:

Code1,Code0	Name	Meaning
0,0	HOLD	Integrators hold their integral values and ignore received input signal $\Phi_c(t)$ - - -

-continued

Code1,Code0	Name	Meaning
1,1	INT+	equivalent to multiplying input $\Phi_c(t)$ by zero. Integrators add received signal $\Phi_c(t)$ to integral value - - - equivalent to multiplying input $\Phi_c(t)$ by one.
1,0	INT-	Integrators subtract received signal $\Phi_c(t)$ from integral value - - - equivalent to multiplying input $\Phi_c(t)$ by, negative one.
0,1	SAMPLE	Integrators transfer integral value to sample-and-hold circuit.

For each reception event the two-bit commands will consist of a string of pairs of INT+ and INT- commands, followed by a single SAMPLE command, and a string of HOLD commands.

To prevent the receiver code-sequence generator 117 from generating radio-frequency noise as a byproduct of its operation, the receiver code-sequence generator 117 is designed using low-noise current-steering logic. This type of logic consumes more power than standard CMOS logic, so it is disabled to conserve power when not in use by the power control circuitry 1714 which is switched by the RxPower signal on line 155 from the low-frequency real time clock 119. For clarity, the power lines running from power control circuitry 1714 to the other components in FIG. 17a are not shown.

For every bit generated in the code sequence $\sigma(i)$ by a linear feedback shift register 1716, two two-bit commands Code1/Code0 are sent to the time-integrating correlator 114, corresponding to one INT+ command and one INT- command. For this reason, the divide-by-two counter 1712 produces a half-speed clock signal, HSClock, on line 1741 that runs the linear feedback shift register 1716 at half the speed of the system clock signal DClock on the clock line 160. As shown in the timing chart of FIG. 17b, every time the linear feedback shift register 1716 produces one output bit of the code sequence $\sigma(i)$ on line 1742, a two-bit code generation state machine circuit 1730 produces the two commands of a doublet consisting of an INT+ and an INT- command. The order of the INT+ and INT- commands is determined by the values of the bits in the code sequence $\sigma(i)$ on line 1742 from the linear feedback shift register 1716. FIG. 17b shows a sample code sequence $\sigma(i)$ that begins with a first code value $\sigma(1)$ of positive unity, a second code value $\sigma(2)$ of negative unity, and a third code value $\sigma(3)$ of positive unity, etc. By means discussed below, the first three code values σ are converted to the three pairs of commands: INT+ (Code1=1, Code0=1), INT- (Code1=1, Code0=0), INT-, INT+, INT+ and INT-. The reception command sequence Code1/Code0 lags the code sequence σ by a clock tick t_c . As shown in FIG. 17b, the reception command sequence Code1/Code0 ends with a SAMPLE command and a string of HOLD commands.

The particular code that the linear feedback shift register 1716 produces is determined by initial seed and coefficient values provided by the processor 140 on data bus 190 before each reception event. Although the code sequence $\sigma(i)$ is shown to be generated by a linear feedback shift register 1716 in FIG. 17a, there are many other ways that the code sequence $\sigma(i)$ could be generated, including a random access memory or a shift register that contains the entire code. The linear feedback shift register 1716 can generate maximal sequences, Gold codes, Kasami-large codes, Kasami-small

codes, BCH codes, and others. The processor 140 also loads the run length counter 1718 via data bus 190 prior to each reception event with the number of bits in the code sequence $\sigma(i)$. When the reception event is complete, a terminal count signal from the TC output of the run length counter 1718 is asserted on line 1749 into a terminal count flip-flop 1724 via an OR gate 1722. The Q output from the terminal count flip-flop 1724 feeds back into the OR gate 1722 via a feedback line 1748 to force the terminal count flip-flop 1724 to stay high after the terminal count is complete. Therefore, the inverted terminal count signal, ITCL, on line 1743 from the Q-Bar output of terminal count flip-flop 1724 stays high during the generation of the code sequence $\sigma(i)$, and goes low on the rising edge of the system clock DClock after the last value of the code sequence $\sigma(i)$ is generated by the linear feedback shift register 1716.

While the code generation state machine circuit 1730 receives a WReset signal on the reset line 170, Code1 and Code0 are forced to zero to produce a HOLD command. An asserted reset signal WReset also causes the ITCL signal at the Q-Bar output of the terminal count flip-flop 1724 to be high. This ITCL signal on line 1743 is latched serially through the two lower state machine flip-flops 1735 and 1736. As shown in FIG. 17b, two ticks of the clock signal DClock after the WReset signal goes low, the Code1 output from the lower right state machine flip-flop 1736 goes high, and remains there until two DClock ticks after the ITCL signal from the terminal count flip-flop 1724 goes low. Since a high value of Code1 assures that the output Code1/Code0 command is either the INT+ command or the INT- command, depending on the value of Code0, the ITCL signal controls the number of ticks of the system clock DClock for which integrations occur in the integrators 1430.

Because the output of a first multiplexer 1731 in the state machine 1730 is selected by the half-speed clock signal HSClock on line 1741 from the divide-by-two clock 1712, its output will switch from the value at the 0 input to the value at the 1 input during each chip of the code sequence $\sigma(i)$, producing a pair of INT commands, INT+ and INT-. As shown in FIG. 17b, during the first half of each chip, the first multiplexer 1731 passes the value from the linear feedback shift register 1716 to the upper left flip-flop 1732, which latches it and outputs the chip value on its Q terminal. During the second half of each chip, the upper left flip-flop 1732 produces at the Q output the inversion of the value from the first half of the chip by feeding the inverted output from its Q-Bar terminal back into the 1 input of the first multiplexer 1731 via a feedback line 1744. As shown in FIG. 17b, the Y output of the first multiplexer 1731 therefore changes in the middle of each value of the code sequence $\sigma(i)$. The output of the second multiplexer 1733 is selected by the signal from the Q output of the lower left flip-flop 1735 via line 1750. Since the lower left flip-flop 1735 is high during a reception event until the terminal count, the second multiplexer 1733 passes the values from the upper left flip-flop 1732 through to the upper right flip-flop 1734 until two system clock DClock ticks after the terminal count from the TC output of the run length counter 1718 is asserted. The upper right flip-flop 1734 holds the Y output values from the second multiplexer 1733 for each tick of the DClock. The diagonal arrows between the code sequence $\sigma(i)$ trace and the Code0 trace in FIG. 17b highlight the delay of one tick of the system clock DClock of the Code0 signal from the corresponding section in the code sequence $\sigma(i)$.

One tick of the system clock DClock on line 160 after the ITCL signal on line 1743 from the Q-Bar output of the terminal count latch 1724 goes low, the Q output from the

lower left flip-flop 1735 also goes low on line 1750, as shown in FIG. 17b. This causes the second multiplexer 1733 to select the high signal on the Q output of the lower right flip-flop 1736 which is directed into the 0 input of the multiplexer 1733, and to pass this on to the upper right flip-flop 1734. The output of the lower right flip-flop 1736 then goes to zero and the output of the upper right flip-flop 1734 goes to one on the next DClock tick on line 160, producing a SAMPLE command (Code0=1, Code1=0), as shown in FIG. 17b. Then the low signal input to the lower right flip-flop 1736 propagates through the second multiplexer 1733 to the Q output of the upper right flip-flop 1734 on the next tick of the system clock DClock on line 160 to provide a HOLD command (Code1=0 Code0=0). HOLD commands continue to be provided (until the next receiver event is triggered) since zeros are output from the lower flip-flops 1736 and 1736, the second multiplexer 1733 and the upper right flip-flop 1734 as long as the ITCL signal from the terminal count flip-flop 1724 continues to be low.

Detailed Description of the Time-Integrating Correlator

A time-integrating correlator according to the present invention is shown in FIG. 18. As is described in detail below, the integrators 1430 provide differential analog signals at their outputs IntOut+ and IntOut- equal to the integral of the product of the differential externally-generated signal $\Phi_c(t)^+$ and $\Phi_c(t)^-$ received at the antenna 102 and the internally-generated integration sequence $\Phi_r(t)$ delayed by the chain of D flip-flops 1460 (in the form of a two-bit reception command sequence Code1/Code0). As shown in FIG. 18, the received differential antenna signals $\Phi_c(t)^+$ and $\Phi_c(t)^-$ on the input differential signal lines 125 and 126 are directed to input terminals IntIn+ and IntIn- of the sixteen rising-edge integrators 1430r.1 through 1430r.16 (of which only the first two rising-edge integrators 1430r.1 and 1430r.2 and the last rising-edge integrator 1430r.16 are explicitly shown) and sixteen falling-edge integrators 1430f.1 through 1430f.16 (of which only the first two falling-edge integrators 1430f.1 and 1430f.2 and the last falling-edge integrator 1430f.16 are explicitly shown). For notational convenience similar components which share a first portion of their reference numerals will be referred to generally or collectively using only that first portion of the reference numeral. For example, the rising-edge integrators 1430r.1 through 1430r.16 may be referred to as "rising-edge integrators 1430r;" or the rising-edge and falling-edge integrators 1430r and 1430f may be referred to as "integrators 1430." Similarly, when the particular integrator is immaterial, it will be referred to as "the integrator 1430." As discussed below, the rising-edge integrators 1430r and the falling-edge integrators 1430f are so named because the input to the rising-edge integrators 1430r changes on the rising-edge of the system clock signal DClock and the input to the falling-edge integrators 1430f changes on the falling-edge of the system clock signal DClock.

A reference voltage line 1422 provides supply voltage Vmid to the reference voltage inputs Vmid of the integrators 1430. (The ground and power buses are not shown in the figure.) The Reset inputs of the integrators 1430 are connected to a reset line 170 which carries the WReset signal. When the WReset signal goes high the voltages stored in the capacitors in the integrators 1430 are cleared to zero (as will be discussed in detail below). A gain control signal IGain on gain control line 136 supplied to the Gain inputs of the integrators 1430 controls the gain of the integrators 1430 according to the expected length of the received code sequence $\Phi_c(t)$ so that the peak output voltage across the output terminals IntOut+ and IntOut- can be maintained at an approximately constant level.

The reception command sequence Code1/Code0 on lines 132 and 133 is directed to a delay line of flip-flops 1460 as a two-bit signal, having first bit Code1 on line 133 and second bit Code0 on line 132. The system clock signal DClock is supplied via a clock line 160 to the clock inputs (represented by triangles on the left edges of the flip-flops) of the rising-edge flip-flops 1460r. The rising-edge flip-flop 1460r trigger on the rising edge of the system clock signal DClock. The clock inputs of the falling-edge flip-flops 1460f are inverted (represented by the small circles next to the clock inputs), so they trigger on the falling edges of the system clock signal DClock.

The Q outputs of the first pair of rising-edge flip-flops 1460r.1.1 and 1460r.1.2 are connected to the D inputs of the second pair of rising-edge flip-flops 1460r.2.1 and 1460r.2.2, and to the D inputs of a first pair of falling-edge flip-flops 1460f.1.1 and 1460f.1.2, respectively. In general, the Q outputs of the n^{th} pair of rising-edge flip-flops 1460r.n.1 and 1460r.n.2 are connected to the D inputs of the $(n+1)^{\text{th}}$ pair of rising-edge flip-flops 1460r.(n+1).1 and 1460r.(n+1).2, and to the D inputs of the n^{th} pair of falling-edge flip-flops 1460f.n.1 and 1460f.n.2, respectively. However, the Q outputs of the sixteenth pair of rising-edge flip-flops 1460r.16 are connected to the D inputs of a pair of terminating flip-flops 1461. The rising-edge flip-flops 1460r act as a shift array, shifting the two-bit command sequence Code1 and Code0 through the rising-edge flip-flops 1460r by one flip-flop per rising edge of the system clock Dclock. On the falling edges of the system clock Delock the output of the n th rising-edge flip-flop 1460r.n is shifted through the n th falling-edge flip-flop 1460f.n. Therefore, the falling-edge flip-flops 1460f act as another shift array, effectively shifting the two-bit command sequence Code1 and Code0 through by one flip-flop per falling edge of the system clock Delock. (It should be noted that there are other ways of constructing chains of flip-flops to produce the same result, such as connecting the outputs of the n th stage of falling-edge flip-flops to the inputs of the $(n+1)$ th stage of rising-edge flip-flops.)

The Q outputs of the rising-edge flip-flops 1460r.n.1 and 1460r.n.2 are directed to the command sequence inputs Code1 and Code0 of the rising-edge integrators 1430r.n, respectively, thereby providing taps of the shift array produced by the rising-edge flip-flops 1460r. Similarly, the Q outputs of the falling-edge flip-flops 1460f.n.1 and 1460f.n.2 are directed to the command sequence inputs Code1 and Code0 of the falling-edge integrators 1430f.n, respectively, thereby providing taps of the shift array produced by the falling-edge flip-flop 1460f. As discussed earlier, when the command sequence Code1 and Code0 at the Code1/Code0 input of an integrator 1430 has a binary value of "11" the externally-generated signal $\Phi_c(t)$ is multiplied by +1 and integrated, and the integration signal $\Phi_i(t)$ is said to have a value of positive one; when the command sequence Code1 and Code0 at the Code1/Code0 input of an integrator 1430 has a binary value of "10" the externally-generated signal $\Phi_c(t)$ is multiplied by -1 and integrated, and the integration signal $\Phi_i(t)$ is said to have a value of negative one; when the command sequence Code1 and Code0 at the Code1/Code0 input of an integrator 1430 has a binary value of "01" the value of the integral calculated by the integrator 1430 is transferred to the output terminals IntOut+ and IntOut- of the integrator 1430; and when the command sequence Code1 and Code0 at the Code1/Code0 input of an integrator 1430 has a binary value of "00," the integrator circuit 1430 holds its internal value constant, and the integration sequence $\Phi_i(t)$ is said to have a value of zero. When the

command sequence Code1/Code0 value of "01" reaches the terminal flip-flops 1461, the AND gate 1453 activates the RxStop signal on receive stop line 142.

The output terminals IntOut+ and IntOut- of the rising-edge integrators 1430r.1 through 1430r.16 are connected to the input terminals MuxIn+ and MuxIn- of analog rising-edge multiplexers 1450r.1 through 1450r.16, and the output terminals IntOut+ and IntOut- of the falling-edge integrators 1430f.1 through 1430f.16 are connected to the input terminals MuxIn+ and MuxIn- of analog falling-edge multiplexers 1450f.1 through 1450f.16, respectively. When the n^{th} multiplexer 1450 is selected by the processor 140 via the data bus 190, the input to the n^{th} multiplexer 1450 at input terminals MuxIn+ and MuxIn- is individually transferred to the output terminals MuxOut+ and MuxOut- where it is amplified by an amplifier 1452 to provide differential outputs $\Lambda(n)^+$ and $\Lambda(n)^-$ at the correlator output terminals 127 and 128. The difference of the differential outputs $\Lambda(n)^+$ and $\Lambda(n)^-$ is equal to the n^{th} bin value of the discrete-time pseudo-autocorrelation (DTPAC) function $\Lambda(n)$.

The circuitry of the rising-edge and falling-edge integrators 1430 is the same, and is shown in detail in FIG. 19. Integrators are often implemented using an operational amplifier with a capacitor in the feedback path to the inverting input node. A resistor is connected from the same node to the voltage signal to be integrated. Because the op-amp maintains the inverting input node at a constant virtual ground voltage, the current through the resistor is proportional to the signal voltage. The op-amp balances the current through the resistor against the current into the capacitor. Integrators implemented in this fashion are highly accurate, but limited by the compensated frequency response of the amplifier. In contrast, in the preferred embodiment of the present invention the integrator uses a transconductance amplifier which does not rely on the features of high voltage gain and feedback which create the response limitations of an op-amp integrator. Furthermore, FETs in the transconductance amplifier of the preferred embodiment naturally convert input voltages to output currents, so by taking advantage of this natural mode of operation of CMOS devices the transconductance amplifier operates with times on the order of one nanosecond. This is to be compared with the operation time of operational amplifiers which is typically on the order of a hundred nanoseconds. Operation times on the order of a nanosecond are necessary since the system clock DClock changes its value every 2.5 nanoseconds.

As shown in FIG. 19, in each integrator 1430 the delayed command signals Code1 and Code0 are directed via code input lines 133 and 132 to a decoder 1560. Code1 and Code0 are binary signals and therefore the pair of signals represents four states. When Code1=1 and Code0=0, the integration sequence $\Phi_i(t)$ is considered to have a value of negative unity and this value is multiplied with the received externally-generated signal $\Phi_c(t)$ by inverting the polarity of the signal prior to integration. When Code1=1 and Code0=1, the integration sequence $\Phi_i(t)$ is considered to have a value of positive unity, and by leaving the received externally-generated signal $\Phi_c(t)$ unaltered the signal $\Phi_c(t)$ is multiplied by unity prior to integration. When Code1=0 and Code0=1, the integrator circuit 1430 produces as an output across output terminals IntOut+ and IntOut- the value of the integral of the product of the integration sequence $\Phi_i(t)$ and the externally-generated received signal $\Phi_c(t)$ by sampling the amount of charge on an internal capacitor (as explained below). Between integration and sampling operations (and in some doublets as discussed below) the values Code1=0

and Code0=0 are directed to the integrators 1430, causing them to hold their output values without sampling and therefore being equivalent to the multiplication of the externally-generated received signal $\Phi_c(t)$ by zero and summing, i.e., the integration sequence $\Phi_i(t)$ is considered to have a value of zero.

When the integration sequence $\Phi_i(t)$ has a value of positive unity (Code1=1 and Code0=1), the decoder 1560 sends a signal from an Int⁺ output terminal via a lead 1561 to a noninverting switch 1582 which directs the positive component of the differential received signal $\Phi_c(t)^+$ on input lead 125 to the positive input terminal TransIn⁺ of a transconductance amplifier 1570, and directs the negative component of the differential received signal $\Phi_c(t)^-$ on input lead 126 to the negative input terminal TransIn⁻ of the transconductance amplifier 1570. Similarly, when the integration sequence $\Phi_i(t)$ has a value of negative unity (Code1=1 and Code0=0), the decoder 1560 sends a signal from an Int⁻ output terminal via a lead 1562 to an inverting switch 1581 which directs the positive component of the differential received signal $\Phi_c(t)^+$ on input lead 125 to the negative input terminal TransIn⁻ of the transconductance amplifier 1570, and directs the negative component of the differential received signal $\Phi_c(t)^-$ on input lead 126 to the positive input terminal TransIn⁺ of the transconductance amplifier 1570. Whether the internally-generated integration sequence $\Phi_i(t)$ has a value of positive unity or negative unity, the value of Code1 is unity, so after passing through inverter 1579, the signal to a hold switch 1580 is low and the hold switch 1580 remains open and does not affect the input to the transconductance amplifier 1570.

The transconductance amplifier 1570 converts a differential input voltage across inputs TransIn⁺ and TransIn⁻ to a proportional output current across output TransOut⁺ and TransOut⁻. The amplification provided by the transconductance amplifier 1570 is controlled by signal IGain directed via an input line 131 to the IGain input of the amplifier 1570. The reference voltage Vmid, directed via a lead 1422 to the Vmid input of the transconductance amplifier 1570, is a reference voltage with a value equal to the ideal average of the differential received signals $\Phi_c(t)^+$ and $\Phi_c(t)^-$.

The current from the output terminals TransOut⁺ and TransOut⁻ of the amplifier 1570 charges an integration capacitor 1572 connected across the output terminals TransOut⁺ and TransOut⁻ of the amplifier 1570, so the voltage across integration capacitor 1572 is proportional to the integral of the voltage across the input terminals TransIn⁺ and TransIn⁻ of the amplifier 1570. Ideally the transconductance amplifier 1570 would have infinite (Norton equivalent) output impedance, so that the output current is independent of the voltage across the output terminals TransOut⁺ and TransOut⁻. In practice, the output impedance is finite, and when a voltage appears across the integration capacitor 1572 some of the charge on the integration capacitor 1572 is drained off through the outputs TransOut of the transconductance amplifier 1570. During the period of approximately ten microseconds when an externally-generated code sequence $\Phi_c(t)$ is received, the voltage drain is only a few percent. However, if steps were not taken to prevent such voltage losses, significant charge would drain from the integration capacitor 1572 during the time on the order of 100 microseconds that it takes for the processor 140 to digitize the correlation results from all the integrators 1430.

When the input to the decoder 1560 is a Hold signal (Code1=0, Code0=0), the low value of Code1 is inverted by inverter 1579 to provide a high value to close the hold switch

1580. With the hold switch 1580 closed, the voltage applied to both inputs TransIn⁺ and TransIn⁻ of the transconductance amplifier 1570 is the reference voltage Vmid. Since the same voltage is applied to both inputs TransIn of the transconductance amplifier 1570, the amplifier 1570 does not produce an output current, the charge across the integration capacitor 1572 is unaffected, and the integration sequence $\Phi_i(t)$ is considered to have a value of zero.

When the input to the decoder 1560 corresponds to a Sample signal (Code0=1, Code1=0), again the Code1 value is low and the hold switch 1580 provides the voltage Vmid to both the inputs TransIn⁺ and TransIn⁻ of the transconductance amplifier 1570, so the charge across the output capacitor 1572 is unaffected. Also, the decoder 1560 switches the Sample output to high. The Sample output is directed to a delay unit 1590, a first input of a NOR gate 1591, and two feedback-capacitor shorting switches 1585 and 1586. The output of the delay 1590 is directed to the Grab input of a charge transfer switch 1584. When closed, the charge transfer switch 1584 connects the integration capacitor 1572 in series with two sampling capacitors 1592 and 1593. The output of the delay 1590 is also directed to a second input of the NOR gate 1591, and the output of the NOR gate 1591 is directed to a sampling-capacitors connection switch 1587 which connects the two sampling capacitors 1592 and 1593 in series.

Because the output impedance of the transconductance amplifier 1570 is finite and the charge across the integration capacitor 1572 decays by leaking through the transconductance amplifier 1570, the integrator circuit 1430 must determine the voltage across the integration capacitor 1572 on a time scale fast relative to this decay. (In the preferred embodiment the integrator circuit 1430 determines the charge across the integration capacitor 1572 in approximately five nanoseconds.)

As shown in the timing chart of FIG. 20, when the Sample output of the decoder 1560 is asserted, the Grab signal on line 1565 also goes high after a delay induced by the delay unit 1590. Also, the output Xfer of the NOR gate 1591 on line 1566 goes from high to low shortly after the Sample signal goes from low to high, but before the Grab signal goes from low to high. Therefore, prior to the Sample signal going high the feedback-capacitor shorting switches 1585 and 1586 are open, the charge transfer switch 1584 is open, and the sampling-capacitors connection switch 1587 is closed. When the Sample signal first goes high the feedback-capacitor shorting switches 1585 and 1586 close, connecting the positive input DifIn⁺ to the negative output DifOut⁻, and the negative input DifIn⁻ to the positive output DifOut⁺ of the differential amplifier 1595, forcing a virtual connection of DifIn⁺ and DifIn⁻ (i.e., a differential voltage of zero). After the high Sample signal passes through the NOR gate 1591 the sampling-capacitors connection switch 1587 opens. Then, after a delay induced by the delay unit 1590 the signal to the Grab input of the charge transfer switch 1584 goes high and the charge transfer switch 1584 closes so that a precise portion of the charge on the integration capacitor 1572 (determined by the ratio of the capacitance of the integration capacitor 1572 to the sum of the capacitances of the sampling capacitors 1592 and 1593) is transferred to the sampling capacitors 1592 and 1593 which are effectively in series. Because the inputs DifIn⁺ and DifIn⁻ of the differential amplifier 1595 are shorted to the outputs DifOut⁻ and DifOut⁺, respectively, the voltage differential across the inputs DifIn is held at zero. When the Sample signal returns low the feedback-capacitor shorting switches 1585 and 1586 open. Then, after a delay induced by the delay unit 1590 the

Grab signal goes low causing the charge transfer switch **1584** to open and the sampling-capacitors connection switch **1587** to close. Now a charge on sampling capacitors **1592** and **1593** proportional to the charge that had accumulated on the integration capacitor **1572** is present across the inputs DifIn of the differential amplifier **1595**. The voltage at the outputs DifOut of the differential amplifier **1595** will change to place an equal and opposite charge on the feedback capacitors **1596** and **1597**, and bring the differential voltage at the inputs DifIn of the differential amplifier **1595** to zero. The voltage change required to do this is equal to the charge on the sampling capacitors **1592** and **1593** times the ratio of the values of the capacitances of the sampling capacitors **1592** and **1593** to the capacitances of the feedback capacitors **1596** and **1597**. This ratio is selected to provide the desired amplification factor. The resulting voltages on the outputs DifOut of the differential amplifier **1595** are connected to the outputs IntOut⁺ and IntOut⁻ of the integrator circuit **1430** on lines **1598** and **1599** to provide an amplified value of the integral of the product of the internally-generated integration sequence $\Phi_i(t)$ and the received externally-generated signal $\Phi_c(t)$.

After a receive event is completed, the outputs of the integrators **1430** are selected by the multiplexers **1450**, and the WReset signal on the reset bus **170** is asserted, causing an integration-capacitor shorting switch **1583** connected across the integration capacitor **1572** to close, thereby zeroing the charge on the integration capacitor **1572**. When the WReset signal is asserted, the Code1 bit is held low so that hold switch **1580** is closed and the transconductance amplifier **1570** does not produce an output current. As discussed above, the WReset signal is unasserted just before a reception command sequence Code1 and Code0 is shifted into the first integrator **1430**.

Detailed Description of the Transmitter Code-sequence Generator

The transmitter code-sequence generator **118** is shown in detail in FIG. **21a**, and timing charts FIGS. **21b–e** show the values of WReset, DClock, LClock, TxStop, the code sequence $\sigma(i)$, the output from multiplexer **1808**, TxAntL, TxAntR and the transmitted signal $\Phi_c(t)$ for four different values in a resting state register **1804** of the transmitter code-sequence generator **118**. During a transmission event, this circuit **118** generates a code sequence $\sigma(i)$ from parameters initialized by the processor **140** via data bus **190**. The code sequence $\sigma(i)$, a string of ones and zeroes, is converted into a two-bit transmission command sequence, TxAntL on line **135** and TxAntR on line **136**, that causes the transmitter driver circuit **116** (which is discussed in detail below) to produce the transmitted signal. Although the code sequence $\sigma(i)$ can be generated by a linear feedback shift register **1826** as shown in FIG. **21a**, there are many other ways that the code sequence $\sigma(i)$ could be generated, including a shift register or a random access memory. The switching elements of the transmitter code-sequence generator **118** (i.e., every element except a power control unit **1802**, the modulation latch **1822**, and the resting state register **1804**) utilize low-noise current-steering logic to prevent them from generating power supply and radio frequency noise while in operation. Because this low-noise logic has a large power consumption, the transmitter code-sequence generator **118** is disabled when not in use by power control circuitry **1802** according to the TxPower signal on line **138**. For clarity, the power lines from the power control circuit **1802** are not shown.

For every bit in the code sequence $\sigma(i)$ the transmitter driver **116** produces the two Gaussian impulses of a doublet.

A first divide-by-two counter **1820** reduces the frequency of clock pulses on line **160** by two to produce a half-speed clock signal LClock on line **1841**. As shown in FIGS. **21b–21e**, the half-speed clock signal LClock changes value for each rising edge of the system clock DClock. The half-speed clock signal LClock clocks the linear feedback shift register **1826** to produce one code value $\sigma(i)$ for every two ticks of the system clock DClock. As an example, in FIGS. **21b–21e** the code values $\sigma(i)$ are shown to be +1, -1, +1, +1, -1, -1 and +1, and it is assumed that the code values $\sigma(i)$ are not modulated by the modulation latch **1822**, i.e., the value in the modulation latch **1822** is zero.

Modulation latch **1822** and XOR gate **1824** are used to encode a message onto a string of pseudorandom sequences $\sigma(i)$ generated by the linear feedback shift register **1826**, using a technique called “antipodal modulation.” Before each transmission event, the processor **140** loads the modulation latch **1822** via data bus **190** with a single bit value. If the bit supplied by the modulation latch **1822** is zero, the XOR gate **1824** does not invert the code sequence $\sigma(i)$, and the unchanged code sequence $\sigma(i)$ is passed through as the modulated code sequence $\sigma(i)$ on line **1842**, as shown in FIGS. **21b–e**. However, when a bit supplied by modulation latch **1822** is one, the XOR gate **1824** causes the code sequence $\sigma(i)$ passed through as the modulated code sequence $\sigma(i)$ on line **1842** to be inverted. Other modulation techniques, such as phase modulation, can be used alone or in conjunction with antipodal modulation in the current invention. For ease of presentation, in the following discussions of the transmitter code-sequence generator **118** it will be assumed that the code sequence $\sigma(i)$ is unmodulated, i.e., $\sigma(i)=\sigma(i)$.

The length of the code sequence $\sigma(i)$ is controlled by run length counter **1828**. The processor **140** loads this counter **1828** via data bus **190** with the length of the code sequence $\sigma(i)$ before a transmission event begins. A counter OR gate **1830** located at the terminal count output TC directs its output to the D input of a counter flip-flop **1832**. The Q output of the counter flip-flop **1832** is directed via TxStop line **137** to the other input of the counter OR gate **1830**. This insures that the TxStop signal on transmission stop line **137** stays high after the run length counter **1828** reaches its terminal count and the terminal count output TC is asserted, until the WReset signal on line **170** is asserted to set the output of the counter flip-flop **1832** to zero.

As discussed below, the shape of the transmitted chip signals $\Phi_c(t)$ can be affected by the resting state of the transmission command sequence values TxAntL and TxAntR on lines **135** and **136**. The resting state is determined by the bits which are loaded by processor **140** via the data bus **190** into the resting-state register **1804** before a transmission event. These two bits are passed via resting state select lines **1846** and **1847** to the A0 and A1 inputs of a resting state multiplexer **1808** to select one of four different resting state options and outputs. The resting state multiplexer **1808** produces a resting state signal at its Y output on line **1848** based on its inputs.

When the signal to the A1 input is one and the signal to the A0 input is zero, the signal at the Y output of the resting-state multiplexer **1808** is zero, as shown in FIG. **21b**, and in every other $\delta t/2$ period the values of both TxAntL and TxAntR are low. When the signals to the A1 and A0 inputs of the resting state multiplexer **1808** are both one, the signal at the Y output is one, as shown in FIG. **21c**, and in every other $\delta t/2$ period the values of both TxAntL and TxAntR are high. But since asymmetries and resistive losses in the circuit cause a small residual field in the antenna **101** after

very doublet, if the same resting state is used after each doublet this residual field may accumulate. This effect can be minimized by alternating between the two resting states within the same code sequence $\sigma(i)$. A first method of alternating resting states is implemented when the signal to the A1 input is zero and the signal to the A0 input is one. In this case the output from a second divide-by-two counter **1806** is selected by the resting-state multiplexer **1808**. The second divide-by-two counter **1806** has as its input the output LClock of the first divide-by-two counter **1820**, so that the output of the multiplexer **1808** alternates between zero on odd chips and one on even chips, as shown in FIG. **21d**. A second way of alternating resting states is implemented when the signals to the A1 and A0 inputs of the resting state multiplexer **1808** are both zero. This selection causes the resting state to be data dependent since the code sequence $\sigma(i)$ (assuming the value in the modulation latch **1822** is zero) output from the XOR gate **1824** is directed to the 00 input of the resting-state multiplexer **1808**, so the output of the resting-state multiplexer **1808** is the same as the code sequence $\sigma(i)$ as shown in FIG. **21d**. In the preferred embodiment of the invention, the linear feedback shift register **1826** produces balanced codes, i.e., codes which have an almost equal number of one and zero bits, (such as maximal sequences, Gold codes, Kasami-large codes, Kasami-small codes and BCH codes) so the average time spent in the high resting state is equal to the average time spent in the low resting state when A1 and A0 are zero.

A transmitter-enable OR gate **1834** forces the transmitter multiplexers **1812** and **1816** to output the resting state provided at their 1 inputs when the transmitter is stopped by a high signal at the terminal count output TC of the run length counter **1828**. During a transmission event, the transmitter-enable OR gate **1834** allows the transmitter multiplexers **1812** and **1816** to alternate between the rest state and the code sequence states by passing the half-speed clock signal LClock on line **1841** through the transmitter-enable OR gate **1834** and directing it to the Select inputs of the transmitter multiplexers **1812** and **1816**. The half-speed clock signal LClock is high for the first half of each chip, so the transmitter multiplexers **1812** and **1816** pass a resting state through to the output flip-flops **1814** and **1818** to be latched as the TxAntL and TxAntR signals on lines **135** and **136**, respectively.

When the half-speed clock signal LClock is low for the second half of each chip, the transmitter multiplexers **1812** and **1816** select the inverted and non-inverted code sequence values $\sigma(i)$ at the 0 inputs to provide antenna signals TxAntL and TxAntR on lines **135** and **136**, respectively. The bottom transmitter multiplexer **1816** uses the code sequence $\sigma(i)$ directly. The top transmitter multiplexer **1812** receives a code sequence $\sigma(i)$ which is inverted by the left antenna inverter **1810** so that the values to the 0 inputs of the output multiplexers **1812** and **1816** are always different. Therefore during the first half of each chip one of TxAntL and TxAntR values will always be equal to the resting state when the other one is not.

FIG. **21b** shows a timing chart for the transmitter code-sequence generator **118** when the resting state register **1804** values are A1=1 and A0=0. As shown in FIG. **21b**, the antenna signals TxAntL and TxAntR are low prior to time zero since WReset is asserted until shortly before time zero. At the beginning of the first chip (at time zero) when the code sequence value $\sigma(1)$ is high, the antenna signals TxAntL and TxAntR remain low since the high value of the half-speed clock LClock causes the output multiplexers **1812** and **1816** to select the values provided at their 1 inputs.

When the half-speed clock LClock goes low at the beginning of the second half of the first chip (at time $\delta t/2$), the output multiplexers **1812** and **1816** then select the inverted and non-inverted values of the code sequence $\sigma(1)$ at their 0 inputs, so the right antenna signal TxAntR goes high. This causes current to flow from right to left in the antenna, producing an impulse of a first polarity (which will henceforth be considered to be a positive polarity), as shown in FIG. **21a**, in the transmitted signal $\Phi_c(t)$ shortly after time $\delta t/2$. At the beginning of the next chip (at time δt) the half-speed clock LClock goes from low to high, again selecting the resting state at the 1 inputs of the output multiplexers **1812** and **1816**. This causes the right antenna signal TxAntR to again go low, producing no voltage differential across the antenna **101**, so that the current which had previously flowed from right to left stops and the transmitted signal $\Phi_c(t)$ has an impulse of negative polarity shortly after time δt . At time $1.5*\delta t$ the half-speed clock LClock again goes low, so that the output multiplexers **1812** and **1816** select the inverted and non-inverted code sequence value $\sigma(2)$ of the second chip. This causes the left antenna signal TxAntL to go high, generating current from left to right in the antenna **101** to produce an impulse of negative polarity shortly after time $1.5*\delta t$. The selection of the resting state followed by the code sequence values $\sigma(i)$ continues until the end of the code sequence $\sigma(i)$ when the TxStop signal on line **137** is asserted. Subsequent to this the WReset signal is asserted and the DClock signal goes high.

FIG. **21c** shows a timing chart for the transmitter code-sequence generator **118** when the resting state register **1804** values are A1=1 and A0=1. As shown in FIG. **21c**, the antenna signals TxAntL and TxAntR are low prior to time zero since WReset is asserted (i.e., high). When WReset goes low, the antenna signals TxAntL and TxAntR go high since the Y output of the resting-state multiplexer **1808** is high. Since both antenna signal TxAntL and TxAntR change value at the same time, no impulses are generated in the transmitted signal $\Phi_c(t)$ at this point. When the half-speed clock LClock goes low midway through the first chip (at time $\delta t/2$), the output from the OR gate **1834** causes the output multiplexers **1812** and **1816** to select the inverted and non-inverted values of the code sequence $\sigma(1)$ provided at their 0 inputs so the left antenna signal TxAntL goes low. This causes current to flow from right to left in the antenna (as was the case in FIG. **21b**), producing an impulse of positive polarity in the transmitted signal $\Phi_c(t)$ shortly after time $\delta t/2$ (again, as in FIG. **21b**). At the beginning of the next chip (at time δt) the half-speed clock LClock goes from low to high, again selecting the resting state provided at the 0 inputs of the output multiplexers **1812** and **1816** by the resting-state multiplexer **1808**. This causes the left antenna signal TxAntL to again go high, producing an impulse of negative polarity in the transmitted signal $\Phi_c(t)$ shortly after time δt . At time $1.5*\delta t$ the half-speed clock LClock again goes low, so that the output multiplexers **1812** and **1816** select the inverted and non-inverted code sequence value $\sigma(2)=-1$ of the second chip. This causes the right antenna signal TxAntR to go low, generating current from left to right in the antenna **101** to produce an impulse of negative polarity shortly after time $1.5*\delta t$ (as was the case in FIG. **21b**). The selection of the resting state followed by the code sequence values $\sigma(i)$ continues until the end of the code sequence $\sigma(i)$ when the TxStop signal on line **137** is asserted. Subsequent to this the WReset signal is asserted and DClock signal goes high.

FIG. **21d** shows a timing chart for the transmitter code-sequence generator **118** when the resting state register **1804**

values are $A1=0$ and $A0=1$. As shown in FIG. 21d, the antenna signals TxAntL and TxAntR are low prior to time zero since WReset is asserted until shortly before time zero. At the beginning of the first chip (at time zero) when the code sequence value $\sigma(1)$ is high, the antenna signals TxAntL and TxAntR remain low since the second divide-by-two unit 1806 provides a low value which is output from the resting-state multiplexer 1808, and the high value of the half-speed clock LClock causes the output multiplexers 1812 and 1816 to select the values provided at their 1 inputs. When the half-speed clock LClock goes low at the beginning of the second half of the first chip (at time $\delta t/2$), the output multiplexers 1812 and 1816 then select the inverted and non-inverted values of the code sequence $\sigma(1)$ at their 0 inputs, so the right antenna signal TxAntR goes high. This causes current to flow from right to left in the antenna, producing an impulse of a first polarity in the transmitted signal $\Phi_c(t)$ shortly after time $\delta t/2$, as shown in FIG. 21d (and as was the case in FIGS. 21b and 21c). At the beginning of the next chip (at time δt) the half-speed clock LClock goes from low to high, again selecting the resting state at the 1 inputs of the output multiplexers 1812 and 1816. Since the divide-by-two counter 1806 now provides a high value to the resting-state multiplexer 1808, this causes the left antenna signal TxAntL to go high, producing no voltage differential across the antenna 101, so that the current which had previously flowed from right to left stops and the transmitted signal $\Phi_c(t)$ has an impulse of negative polarity shortly after time δt . At time $1.5*\delta t$ the half-speed clock LClock again goes low, so that the output multiplexers 1812 and 1816 select the inverted and non-inverted code sequence value $\sigma(2)$ of the second chip, respectively. This causes the right antenna signal TxAntR to go low, generating current from left to right in the antenna 101 to produce an impulse of negative polarity shortly after time $1.5*\delta t$. The selection of the resting state followed by the code sequence values $\sigma(i)$ continues until the end of the code sequence $\sigma(i)$ when the TxStop signal on line 137 is asserted. Subsequent to this the WReset signal is asserted and the DClock signal goes high.

FIG. 21e shows a timing chart for the transmitter code-sequence generator 118 when the resting state register 1804 values are $A1=0$ and $A0=0$. As shown in FIG. 21e, the antenna signals TxAntL and TxAntR are low prior to time zero since WReset is asserted until shortly before time zero. At the beginning of the first chip (at time zero) when the code sequence value $\sigma(1)$ is high, the antenna signals TxAntL and TxAntR go high since the value provided to the 00 input of the resting-state multiplexer 1808 is the value of the code sequence $\sigma(1)$, and the high value of the half-speed clock LClock causes the output multiplexers 1812 and 1816 to select the values provided at their 1 inputs. Since both antenna signals TxAntL and TxAntR go high simultaneously, no current is produced across the antenna and the transmitted signal $\Phi_c(t)$ is unaffected. When the half-speed clock LClock goes low at the beginning of the second half of the first chip at time $\delta t/2$, the output multiplexers 1812 and 1816 then select the inverted and non-inverted values of the code sequence $\sigma(1)$ at their 0 inputs, so the left antenna signal TxAntL goes low. This causes current to flow from right to left in the antenna, producing an impulse of positive polarity in the transmitted signal $\Phi_c(t)$ shortly after time $\delta t/2$, as shown in FIG. 21e (and as was the case in FIGS. 21b, 21c and 21d). At the beginning of the next chip at time δt the half-speed clock LClock goes from low to high, again selecting the resting state at the 1 inputs of the output multiplexers 1812 and 1816. Since the 00 input to the

resting-state multiplexer 1808 now receives the low value of the second chip of the code sequence ($\sigma(2)=-1$), this causes the right antenna signal TxAntR to go low, producing no voltage differential across the antenna 101, so that the current which had previously flowed from right to left stops and the transmitted signal $\Phi_c(t)$ has an impulse of negative polarity shortly after time δt . At time $1.5*\delta t$ the half-speed clock LClock again goes low, so that the output multiplexers 1812 and 1816 select the inverted and non-inverted code sequence value $\sigma(2)$ of the second chip, respectively. This cause the left antenna signal TxAntL to go high, generating current from left to right in the antenna 101 to produce an impulse of negative polarity shortly after time $1.5*\delta t$. The selection of the resting state followed by the code sequence values $\sigma(i)$ continues until the end of the code sequence $\sigma(i)$ when the TxStop signal on line 137 is asserted. Subsequent to this the DClock signal goes high and the WReset signal is asserted.

The transmitter output flip-flops 1814 and 1818 are forced to zero by the WReset signal on line 170 between transmission events. The same WReset signal is used to reset the terminal count flip-flop 1832 and both the divide-by-two counters 1806 and 1820. Holding the divide-by-two counters 1820 and 1806 low until a transmission even starts insures that these counters 1820 and 1806 start up in phase with the system clock DClock on line 160.

Detailed Description of the Transmitter Antenna Driver

The transmitter antenna drive 116 of the present invention, shown in detail in FIG. 22, consists of a series of driver circuits 1680. In the preferred embodiment, there are eight identical driver circuits 1680.0 through 1680.7 (only three driver circuits 1680.0, 1680.1, and 1680.7 are shown for clarity, and only one 1680.0 is shown in detail). Under control of the processor 140 via data bus 190, a power control latch 1691 selects which driver circuits 1680 are enabled during a transmission. Enable signals from the active-low power enable outputs Y0 through Y7 are directed via lines 1670 through 1677 to transmitter driver circuits 1680.0 through 1680.7, respectively. The strength of the transmitted signal is proportional to the number of enabled driver circuits 1680, and the signal strength is increased for transmission to distant localizers or decreased to prevent overpowering nearby localizers. The power control latch 1691 is enabled by the TxPower signal directed to its Enable input via line 138. When the TxPower signal at the Enable input to the power control latch 1691 is low, all the power enable outputs Y0 through Y7 are high, disabling all the transmitter driver circuits 1680, thereby conserving power, and preventing the driver circuits 1680 from switching and generating noise during receiving or processing operations.

The transmitter code-sequence generator 118 generates a transmission command sequence TxAntL and TxAntR on lines 135 and 136 which controls the transmitter antenna drivers 1680. The transmission command sequence TxAntL and TxAntR is delayed through digitally-controlled delay units 1692 and 1693 and 1694 and 1695. The processor 140 controls the delays of these delay units 1692, 1693, 1694, and 1695 via the data bus 190 to compensate for timing variations in the delays induced by the antenna driver buffers (discussed below) in each transmitter driver circuit 1680.

The transmitter driver circuit 1680 includes an H-Bridge switch 1640 comprised of two upper p-channel MOSFET transistors 1641 and 1642, and two lower n-channel MOSFET transistors 1643 and 1644. As discussed above, when

the H-bridge switch **1640** switches the current on or off across the antenna **101**, an electromagnetic Gaussian impulse is radiated. The switching of MOSFET transistors is controlled by the voltage between the gate and the source. A p-channel transistor switches from off to on when its base voltage drops a threshold (approximately 1 to 2 volts) below its source voltage. Therefore, the upper left H-Bridge transistor **1641** switches on when a voltage below V_{DD} arrives at its gate via the left OR gate **1610** and the top left series of buffers **1621–1624**. The top left OR gate **1610** provides a low output when the power enable signal **Y0** is low and the delayed transmission command value TxAntL on line **1665** is low. An n-channel transistor switches from off to on when its base voltage rises a threshold (approximately 1–2 volts) above its source voltage. Therefore, the lower left H-bridge transistor **1643** switches on when it receives a voltage greater than V_{SS} at its gate via the left AND gate **1611** and the bottom left series of buffers **1625–1628**. The left AND gate **1611** supplies a high signal when the transmission command value TxAntL is high, and a low signal from the **Y0** output of the power control latch **1691** is inverted high by a left inverter **1612**. Therefore, one of the left transistors **1641** or **1643** is turned on when the other is turned off. An advantage of using this combination of a p-channel and an n-channel transistor is that the switching is independent of the voltages on the antenna **101** since the antenna is connected to the drains of the transistors, and due to inductive effects the voltage across the antenna **101** may vary with time and even rise above V_{DD} or below V_{SS} .

However, in an alternate embodiment the two upper MOSFET transistors **1641** and **1642** are replaced with n-channel MOSFET transistors. Advantages of n-channel MOSFET transistors is that they are smaller, have lower resistances, and better gain than equivalent p-channel transistors. To guarantee that the upper transistors turn off, a voltage greater than V_{DD} must be provided, possibly by voltage multiplier circuits. It should be noted that voltages less than V_{SS} are difficult to provide for chips fabricated using the N-Well process since the substrate voltage is V_{SS} , and therefore it is problematic to use p-channel MOSFET transistors in the lower portion of the H-bridge switch.

The right side of the H-bridge is controlled by the transmission command sequence TxAntR on line **136** and works in an identical manner. The upper right H-bridge transistor **1642** is a p-channel MOSFET which switches on when a low signal is directed to its gate via the right OR gate **1613** and the top right series of buffers **1631–1634**. The right OR gate **1613** provides a low output when the power enable signal **Y0** is low and the delayed transmission command sequence value TxAntR on line **1666** is low. The lower right H-bridge transistor **1644** is an n-channel MOSFET which switches on when it receives a high signal at its gate via the right AND gate **1614** and the bottom right series of drivers **1635–1638**. The right AND gate **1614** only supplies a high signal when the delayed value TxAntR is high, and a low signal from the **Y0** output of the power control latch **1691** is inverted high by a right inverter **1615**.

The upper left staged buffers **1621**, **1622**, **1623** and **1624** are used to increase the current from the output of the left OR gate **1610** so that the upper left H-bridge transistor **1641** can be switched off and on quickly. Since the radiated signal is a function of the first derivative of the antenna current, the faster the transistors **1641**, **1642**, **1643** and **1644** switch, the greater the radiated signal strength. For clarity, four upper left staged buffers are shown in FIG. **22**, though more or fewer may be employed. The required number of buffer stages is a function of the size of the H-bridge transistor

1641 and the CMOS process parameters. The actual value of the delay introduced by the upper left buffers **1621** through **1624** is not important, if this delay is identical to the delay of the buffers on all the other branches of the H-bridge. Slight differences in the characteristics of the semiconductor from which the upper left buffers are manufactured may however result in different delays for each chain of buffers. To counteract this, the digitally controlled delay **1692** is controlled by the processor **140** via data bus **190** to insure that the delay to the upper left H-bridge transistor **1641** is identical to the delays to all the other transistors **1642**, **1643** and **1644**. The resulting total delay between the arrival of a transmission command sequence value TxAntL at the upper left delay **1692** and the time that the upper left H-bridge transistor **1641** switches on is then a constant that can be subtracted out by the software during ranging calculations.

Similarly, the upper right staged buffers **1631–1634**, the lower left staged buffers **1625–1628**, and the lower right staged buffers **1635–1638** increase the current from the right OR gate **1613**, and the left and right AND gates **1611** and **1614** to cause upper right and bottom left and right H-bridge transistors **1642**, **1643** and **1644**, respectively, to be switched on and off rapidly. Digitally controlled delays **1694**, **1693**, and **1695** allow the total delay through the upper right staged buffers **1631–1634**, the lower left staged buffers **1625–1628**, and the lower right staged buffers **1635–1638** to be adjusted, respectively, until the total delays are all equal.

Two vertical H-bridge lines **1653** and **1654** connect the upper H-bridge transistors **1641** and **1642** to the lower H-bridge transistors **1643** and **1644**, respectively. Lead **157** connects the left H-bridge line **1653** to the left side of the external antenna **101**, and lead **158** connects the right H-bridge line **1654** to the right side of the external antenna **101**.

To produce a doublet, the H-bridge transistors may be turned on and off in any of several different patterns. In a first case, in the resting state the upper H-bridge transistors **1641** and **1642** are held on, while the lower H-bridge transistors **1643** and **1644** are held off. To start the transmission of a positive doublet, the command sequence value TxAntR goes high, causing upper right H-bridge transistor **1642** to switch off and lower right H-bridge transistor **1644** to switch on, so current flows through upper left H-bridge transistor **1641**, down the upper half of the left vertical line **1653**, out the left lead **157**, across the antenna **101**, back into the transmitter driver **116** through right lead **158**, down the lower half of the right vertical line **1654**, and through lower right H-bridge transistor **1644**. During the time that the current is changing (1 or 2 nanoseconds), the antenna **101** will broadcast a single positive Gaussian electromagnetic impulse. After the current reaches the steady state, no signal is produced since the signal is proportional to the change in current. Next, the command sequence value TxAntR goes back to low, causing upper right transistor **1642** to switch on while lower right transistor **1644** switches back off again. This will cause the current across the antenna to change from maximum to zero, producing a second Gaussian electromagnetic impulse with a polarity of the electric vector opposite to that of the first Gaussian impulse. An impulse with a polarity of the electric vector in a first direction (caused by current flowing from left to right) followed by an impulse with a polarity of the electric vector in a direction opposite to the first one, is called a positive doublet. A negative doublet has impulses whose polarities of the electric vectors are opposite to that of a positive impulse. A negative impulse can be produced by raising and lowering the command sequence value TxAntL instead of the command sequence

value TxAntR as outlined previously. In this case, the resulting current first goes from right to left through the antenna **101**, producing a first Gaussian impulse with a polarity of the electric vector opposite to the polarity of the first impulse in a positive doublet. Then, when the current is turned off an impulse of the opposite polarity to the first pulse in the doublet is produced.

Doublets can also be produced by a starting state where the bottom two H-bridge transistors **1643** and **1644** are held on, while the upper two H-bridge transistors **1641** and **1642** are held off. This is called a low resting state. When in the low resting state, lowering and then raising the command sequence value TxAntL will produce a positive doublet, and lowering and then raising the command sequence value TxAntR produces a negative doublet. Asymmetries and resistive losses in the circuit cause a small residual field in the antenna after every doublet. Switching between different resting states helps to balance this current out to zero. There is a slight difference in the switching speed of the two upper p-channel transistors **1641** and **1642** and the switching speed of the two lower n-channel transistors **1643** and **1644** which can effect the shape of the Gaussian impulses and the spectrum of the resulting signal. Alternating between resting states helps to balance out these effects also.

The physical orientation of a receiving localizer can result in a positive doublet being detected as a negative doublet if the antenna is rotated by 180°. When a string of digital bits, such as correction bits **451**, **461**, etc., are sent with antipodal modulation, having an incorrect polarity can result in an incorrect value being received. Several protocols can be used to determine the true polarity of a doublet. In a first protocol, all the ranging transactions are performed with positive doublets. If the polarity of these doublets appears to be negative, then the orientation of the transmitting antenna is assumed to be backwards, and the polarity of all transactions is assumed to be backwards. In a second protocol, strings of correction bits are always prefaced by a short prearranged code. If this code is received inverted, then the orientation of the antenna is assumed to be opposite, and all the digital bits are inverted.

Detailed Description of the Antennas

As shown in FIG. **23a** and the flattened view of the antenna **101** of FIG. **23b**, the transmitter antenna **101** of the present invention is a modification of a frequency-independent current-mode shielded loop antenna developed by Dr. Henning Harmuth and disclosed in U.S. Pat. No. 4,506,267. The transmitter antenna **101** is an ultra-wideband large-current radiator (LCR) antenna which radiates outwards from the surface of a flat rectangular conducting plate **2330**. In the preferred embodiment the conducting plate is rectangular **2330**. A first triangular section **2321** extends from the top edge **2320** of the plate **2330**, and a second triangular section **2323** extends from the bottom edge **2322** of the plate **2330**. At the apexes of the triangular sections **2321** and **2323** opposite the edges adjacent the plate **2330** extend connection tabs **2311** and **2313**, respectively. Leads **157** and **156** connect the circuit block **2300** to the conducting plate **2330** via connection tabs **2311** and **2313** and triangular sections **2321** and **2323**, respectively. The circuit block **2300** contains a power source (not shown in the Figures) and all the circuitry of FIG. **1** (except the antennas **101** and **102**). In contrast to the disclosures of Harmuth, it has been found that it is not necessary to shield the circuit block **2300** and the leads **156** and **157** to the LCR antenna **101** with high-permittivity or high-permeability materials. FIG. **23b** shows a flattened view of the antenna **101** to illustrate how a planar

sheet of metal foil can be folded to provide the transmitter antenna **101** of FIG. **23a** by bending the two attachment tabs **2311** and **2313** up 90° along a first pair of dotted lines **2310** and **2312**, then bending the two triangular sections **2321** and **2323** up 90° along a second pair of dotted lines **2320** and **2322**, respectively.

An alternate preferred embodiment of the present invention uses a bi-loop LCR antenna **2350**, as shown in FIG. **23c**, to produce a signal with polarizations on two axes separated by 90°. This antenna **2350** has a square radiating plate **2380** with a triangular section **2371**, **2373**, **2375** and **2377** extending from each side of the antenna **2350**. Each triangular section **2371**, **2373**, **2375** and **2377** has a connection tab **2361**, **2363**, **2365** and **2367** extending from the apex of the triangular section **2371**, **2373**, **2375** and **2377**, respectively, opposite the side adjacent the square radiating plate **2380**. The antenna **2350** is attached to the circuit block **2300** by a first pair of leads **2352** and **2354** which are connected across one pair of opposite connection tabs **2361** and **2365** of the antenna **2350**, and a second pair of leads **2356** and **2358** which are connected across the other pair of opposite connection tabs **2367** and **2363** of the antenna **2350**. FIG. **23d** shows a flattened configuration of the antenna **2350** of FIG. **23c**. The antenna **2350** can be manufactured from a piece of planar metal foil by bending the four attachment tabs **2361**, **2363**, **2365**, and **2367** up 90° along dotted lines **2360**, **2362**, **2364**, and **2366**, then bending the four triangular sections **2371**, **2373**, **2375**, and **2377** up 90° along dotted lines **2370**, **2372**, **2374**, and **2376**.

By sending the same code on each transmission axis of the antenna **2350**, separated by a short time interval, one or the other transmission will be received by a single loop antenna whose normal vector is substantially aligned with that of the plane of the bi-loop antenna **2350**. If the receiver is also a bi-loop antenna **2350**, then reception can occur regardless of the relative orientation of the antennas **2350**. Another advantage of the bi-loop antenna **2350** is that it can be used, with sufficient extra circuitry, to transmit different codes on each axis and double the amount of information communicated between localizers, or increase the signal-to-noise ratio. Sending double codes would, however, put restrictions on the relative orientation of the two localizers.

In the preferred embodiment, the transmitter antenna **101** or **2350** is used for both transmitting and receiving impulse sequences $\Phi_c(t)$. However, in some applications it is advantageous to have a separate receiver antenna **102**. To switch a single antenna from connection between the transmission and reception circuitry, the required switch must be faster than standard mechanical switches and have less capacitance than a sufficiently large CMOS transistor. Switches of sufficiently high speed and low capacitance are difficult to construct with CMOS technology. It is often easier and less expensive to manufacture a localizer with a separate receiver antenna for applications where the bulk of a second antenna is not objectionable. As shown in the rear perspective view of FIG. **23e** and the front view of FIG. **23f**, the separate receiver antenna **102** is a closed loop sensor (see "Antennas and Wave Guide for Nonsinusoidal Waves," by Dr. Henning Harmuth, Academic Press, Inc., 1984) consisting of a U-shaped strip of metal **2392**, backed by a ferrite plate **2390** or some other other high-permeability material, to increase the strength of the received signal $\Phi_c(t)$. (The transmitter antenna **101** is not shown in FIG. **23e** for clarity.) A strip of metal **2392** is used rather than a wire, to achieve a lower impedance of the receiver antenna **102**. Two leads **175** and **176** connect the circuit block **2300** to the receiver antenna **102**.

The size of the antennas **101** and **102** is limited to less than 30 centimeters by the propagation time of current impulses through the antennas **101** and **102**; when impulses as short as one nanosecond propagate through an antenna with a length greater than 30 centimeters, the current across the antenna is sufficiently nonuniform to substantially reduce the transmission and reception efficiencies. The lower bounds on the size of the transmitter and receiver antennas **101** and **102**/circuit block **2300** system is determined only by the minimum sizes of the battery, the crystal oscillator **130**, and the rest of the circuitry. In the preferred embodiment, all the circuitry resides on a single CMOS or BiCMOS VLSI chip. The power source is a small battery (such as the zinc-air batteries under development by Driesbach ElectroMotor Inc. of Santa Barbara, Calif.), a thin-film fuel cell (such as those under development by K. Dyer of Bell Communications Research, N.J.), or a rechargeable thin-film lithium microbattery (such as those under development at Oak Ridge National Laboratory, Tennessee, by John B. Bates) on the back of the chip. In an alternate embodiment which allows for further miniaturization, the crystal oscillator **130** is replaced with a micro-machined mechanical resonator integrally formed from the VLSI chip, and the entire localizer is only about the size of a coin, i.e., one or two centimeters square.

The foregoing descriptions of specific embodiments of the present invention have been presented for purposes of illustration and description. They are not intended to be exhaustive or to limit the invention to the precise forms disclosed, and it should be understood that many modifications and variations are possible in light of the above teaching. The embodiments were chosen and described in order to best explain the principles of the invention and its practical application, to thereby enable others skilled in the art to best utilize the invention and various embodiments with various modifications as are suited to the particular use contemplated. Many variations are within the scope of the present invention, for instance: the transmitted impulse sequences may be encoded to carry information using other forms of encoding; other means may be used to provide low-noise circuitry; the transmission code sequence circuitry need not be low-noise logic; other ranging protocols may be used; other means for privacy protection may be implemented; other methods for synchronization of localizers may be used; the time base may be decomposed into stages other than those described in the discussion of the low- and high-frequency clocks, for instance, the low-frequency clock may have more or fewer stages, or the high-frequency clock may have more or fewer stages; the clock rate of the crystal oscillator may be greater than or less than 6.25 MHz; the phase-lock loop circuit may increase the clock rate by more than or less than a factor of thirty-two; the antenna may have another configuration; the impulses may have larger or smaller widths; the transmitted impulses may be separated by other time intervals; the number of correlator bins may be different than described above; the linear feedback shift register may generate other types of pseudorandom impulse sequences; the linear shift register may be replaced with a RAM for generating Barker codes, Bent codes, "No" codes, GMW codes or complimentary codes; the impulse sequences may be generated from RAM; other integrator circuits may be used; other doublet waveforms may be used; fine structure waveforms other than doublets may be used; other time bin offsets may be used; the closed loop sensor receiver antenna may not be backed with a high-permeability plate; etc. In summary, it is intended that the scope of the invention be defined by the Claims appended hereto and their equivalents.

What is claimed is:

1. An apparatus for determining a sub-chip length accuracy time-of-arrival of a received impulse sequence, comprising:

5 means for generating a digital integration sequence resembling said received impulse sequence;

means for generating a plurality of delayed integration sequences from said integration sequence;

10 means for integrating each of said delayed integration sequences multiplied by said received impulse sequence to provide a series of output values approximating a time sampling of a correlation function between said integration sequence and said received impulse sequence;

15 first means for determining a first location of a maximum of said output values; and

second means for determining a second location of a peak of said correlation function to an accuracy of less than a time between chips of said digital integration sequence using said location of said maximum of said output values and magnitudes of said output values on both sides of said maximum.

2. The apparatus of claim 1 wherein said second means for determining measures an amount of asymmetry of said magnitudes of said output values on said both sides of said maximum.

3. The apparatus of claim 1 wherein said second means for determining differentiates between patterns in said series of output values, and said output values are produced by said means for integrating using a full-bandwidth version of said received impulse sequence.

4. The apparatus of claim 1 wherein delays between said delayed integration sequences are on the order of one quarter of a bit length in said received pulse sequence.

5. The apparatus of claim 1 wherein delays between said delayed integration sequences are on the order of half of a bit length in said received pulse sequence.

6. The apparatus of claim 1 wherein said means for determining said arrival time comprises a set of neural nets.

7. An apparatus for determining an arrival time of a received impulse sequence, comprising:

means for generating a digital integration sequence resembling said received impulse sequence;

means for generating a plurality of delayed integration sequences from said integration sequence;

means for integrating each of said delayed integration sequences multiplied by said received impulse sequence to provide a series of output values approximating a time sampling of a correlation function between said integration sequence and said received impulse sequence; and

means for determining said arrival time from said series of output values, wherein said received impulse sequence and said integration sequence are sequences of impulse doublets, each impulse doublet waveform $\gamma(t)$ having a first impulse and a second impulse, said second impulse having an opposite polarity from said first impulse, both said integration sequence and said received impulse sequence having a form

$$\gamma(t \bmod \delta t) \circ [t/\delta],$$

65 where t is time, δt is a separation time between said impulse doublets $\gamma(t)$, the square brackets indicate the largest integer less than or equal to the argument inside the square brackets,

and σ is a pseudorandom code sequence having values of positive and negative unity.

8. The apparatus of claim 7 wherein said impulse doublet waveform $\gamma(t)$ of said integration sequence has the approximate form

$$\gamma_i(t) = +k \quad 0 < t < h * \delta t$$

$$\gamma_i(t) = -k \quad \delta t / 2 < t < \delta t / 2 + h * \delta t$$

$$\gamma_i(t) = 0 \quad \text{otherwise,}$$

where k is a constant, h is a width factor, and said delayed integration sequences are delayed from each other by $(\delta t / 2 - g * \delta t)$, where g is a shift factor.

9. The apparatus of claim 8 wherein said width factor h is approximately one half, and said shift factor g is approximately one quarter.

10. The apparatus of claim 8 wherein said width factor h is approximately one quarter, and said shift factor g is approximately one quarter.

11. The apparatus of claim 8 wherein said width factor h is approximately one half, and said shift factor g is approximately zero.

12. The apparatus of claim 8 wherein said width factor h is approximately one half, and said shift factor $g * \delta t$ is approximately a width of an impulse in said received pulse sequence.

13. An apparatus for determining multiple values of a correlation function of an analog signal and a digital signal at a set of evaluation times, comprising:

a shift register array, said digital signal being shifted through said shift register array from a first shift register to a last shift register on a sequence of shift pulses applied thereto, said shift register array having a plurality of taps to generate a plurality of delayed digital signals, said delayed digital signals being delayed by a plurality of delay times;

means for directing a first bit of said digital sequence to said first shift register of said shift register array at a starting time such that said time of arrival of said analog signal is not later than an exit of said first bit of said digital sequence from said last register of said shift register array; and

a plurality of integrators, said delayed digital signals from said taps in said shift register array being directed to said integrators where said delayed digital signals are multiplied by said analog signal to provide analog integrator outputs approximating values of said correlation function of said analog signal and said digital signal sampled at said evaluation times.

14. The apparatus of claim 13 wherein said analog signals are not delayed.

15. The apparatus of claim 13 further comprising an analog-to-digital converter, and a multiplexor for directing said analog integrator outputs to, said analog-to-digital converter, said analog-to-digital converter producing digital correlator output values from said analog integrator outputs.

16. The apparatus of claim 13 wherein said analog signal and said digital signal are each comprised of a plurality of doublet waveforms, each of said doublet waveforms having a first pulse of a first polarity and a second pulse of a second polarity opposite said first polarity, information in said analog and digital signals being encoded via chip polarities of said doublet waveforms, whereby a plot of said output values of said correlation function changes shape upon shifting an arrival time of said analog signal.

17. The apparatus of claim 16 wherein a difference in said evaluation times is approximately one quarter of a length of said doublet waveforms.

18. The apparatus of claim 16 wherein a difference in said evaluation times is approximately one half of a length of said doublet waveforms.

19. The apparatus of claim 16 wherein said plurality of doublet waveforms is substantially greater than two.

20. The apparatus of claim 13 wherein said starting time may be altered by a fraction of a time between shift pulses.

21. The apparatus of claim 13 wherein said digital integrator output values from said analog-to-digital converter are stored in a set of storage registers, a cardinality of said set of storage registers being equal to that of said plurality of integrators.

22. The apparatus of claim 13 wherein said shift register array has a shift register array length which is not equal to a bit length of said digital sequence.

23. The apparatus of claim 22 wherein said shift register array length is less than said bit length of said digital sequence.

24. An apparatus for determining values of a correlation function of an analog signal and a digital signal at a set of evaluation times, comprising:

a shift register array, said digital signal being shifted through said shift register array on a sequence of shift pulses applied thereto, said shift register array having a plurality of taps to generate a plurality of delayed digital signals, said delayed digital signals being delayed by a plurality of delay times; and

a plurality of integrators, said delayed digital signals from said taps in said shift register array being directed to said integrators where said delayed digital signals are multiplied by said analog signal to provide analog integrator outputs equivalent to values of said correlation function of said analog signal and said digital signal sampled at said evaluation times, each of said integrators including:

a transconductance amplifier for converting a differential voltage at a pair of input terminals to an output current at a pair of output terminals;

a first switching network applying a positive polarity version of said analog signal to said input terminals of said transconductance amplifier when one of said delayed digital signals directed to said one of said integrators has said first value, and applying a negative polarity version of said analog signal to said input terminals of said transconductance amplifier when said one of said delayed digital signals has said second value;

an integration capacitor for storing an integration charge produced by said output current from by said transconductance amplifier; and

a means for reading said integration charge on said integration capacitor.

25. The apparatus of claim 24 wherein said means for reading includes:

a sampling capacitor;

a second switching network for connecting said sampling capacitor to said integration capacitor to allow a sampling capacitor to said integration capacitor to allow a sampling charge to accumulate on said sampling capacitor, and for disconnecting said sampling capacitor from said integration capacitor to isolate said sampling capacitor from said transconductance amplifier

after said sampling charge has accumulated on said sampling capacitor; and

means for ascertaining said sampling charge on said sampling capacitor.

26. The apparatus of claim 24 wherein said sequence of values of said delayed digital signals includes a third value, and said first switching network applies a differential voltage of zero to said input terminals of said transconductance amplifier when said one of said delayed digital signals has said third value.

27. An apparatus for integrating the product of a differential analog signal and a digital signal, comprising:

a transconductance amplifier converting a differential voltage at a pair of input terminals to an output current at a pair of output terminals;

a first switching network applying a positive polarity version of said differential analog signal to said input terminals of said transconductance amplifier when said digital signal has a first value, and applying a negative polarity version of said differential analog signal to said input terminals when said digital signal has a second value;

an integration capacitor for storing an integration charge produced by said output current from at said output terminals; and

a means for determining said integration charge.

28. The apparatus of claim 27 wherein said means for determining includes:

a sampling capacitor; and

a second switching network for connecting said sampling capacitor to said integration capacitor to allow a sampling charge to accumulate on said sampling capacitor,

and for disconnecting said sampling capacitor from said integration capacitor to isolate said sampling capacitor from said transconductance amplifier after said sampling charge has accumulated on said sampling capacitor.

29. The apparatus of claim 27 wherein said sequence of values of said delayed digital signals includes a third value, and said first switching network applied a differential voltage of zero to said input terminals of said transconductance amplifier when said one of said delayed digital signals has said third value.

30. A spread spectrum transmitter comprising:

means for transmission of a transmission sequence of impulse doublets, each impulse doublet waveform $\gamma(t)$ having a first impulse and a second impulse, said second impulse having an opposite polarity from said first impulse; and

means for controlling a time t_0 between said first impulse and said second impulse to provide a notch in a frequency spectrum of said transmission sequence at a frequency f by setting an integer multiple of $(1/t_0)$ equal to f , said transmission sequence having a form

$$\gamma(t \bmod \delta t) [t/\delta t] \sigma,$$

where t is time, δt is a separation time between said impulse doublets $\gamma(t)$, the square brackets indicate the largest integer less than or equal to the argument inside the square brackets, and σ is a pseudorandom code sequence having values of positive and negative unity.

* * * * *