

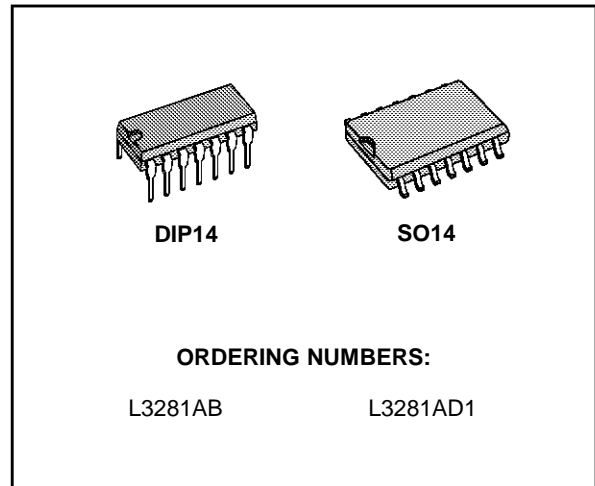
**LOW VOLTAGE TELEPHONE SPEECH CIRCUITS**

PRELIMINARY DATA

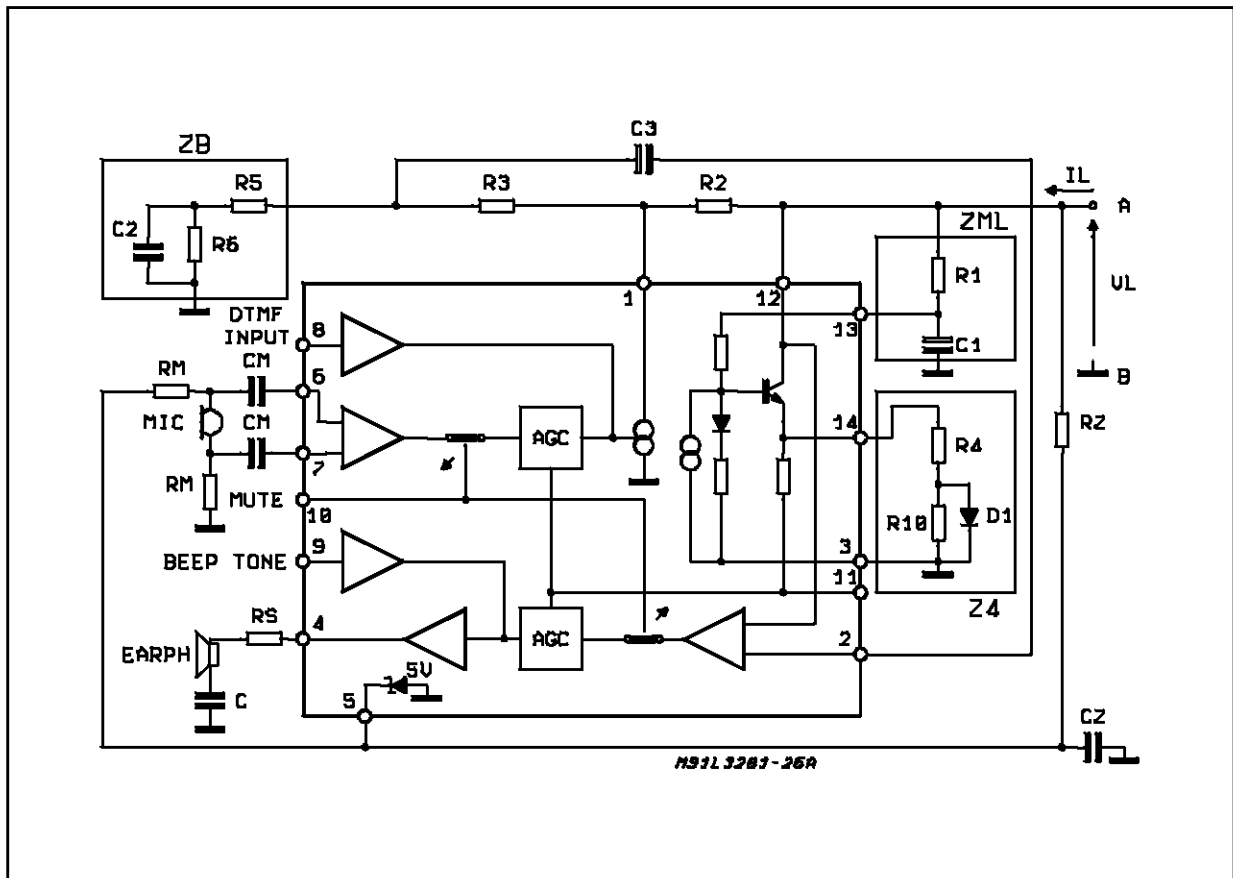
- OPERATION DOWN TO 1.6V / 6.5mA
- DTMF & BEEP TONE INPUTS
- EXTERNAL MUTING FOR EARPHONE AND MICROPHONE
- SUITABLE FOR DYNAMIC EARPHONE AND DYNAMIC OR ELECTRET MICROPHONE
- AGC CONTROL ON BOTH SENDING AND RECEIVING

**DESCRIPTION**

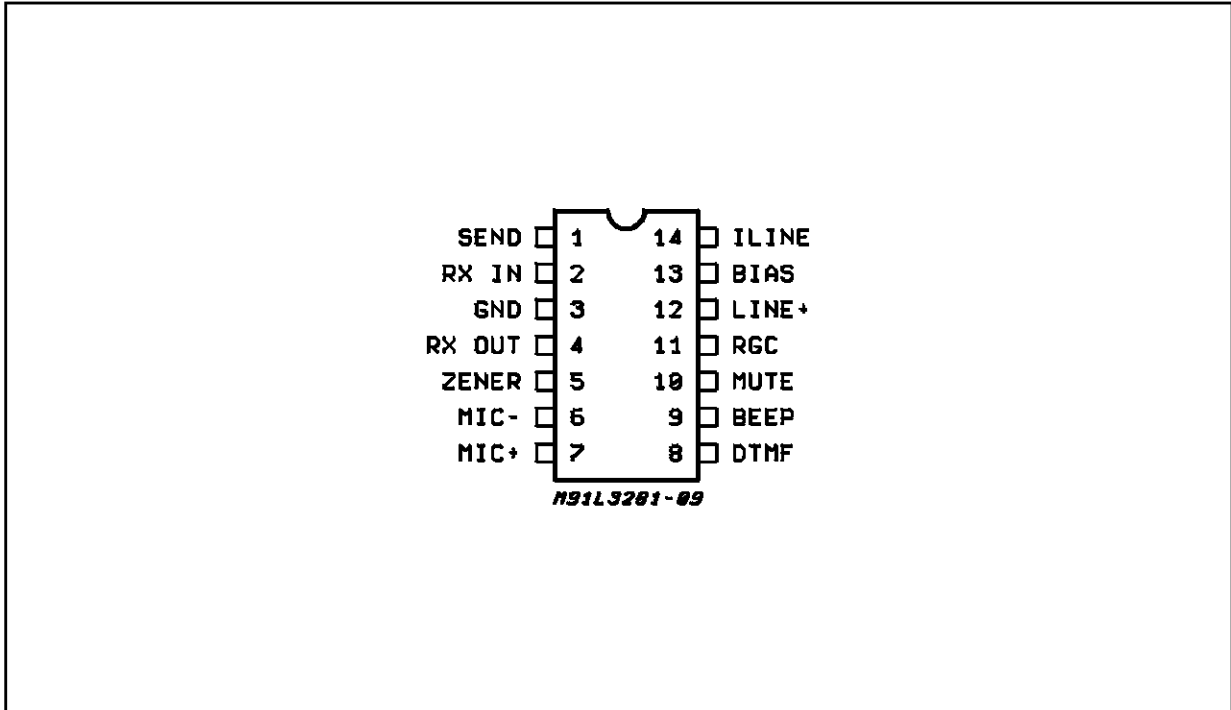
The L3281 is an electronic speech circuit developed to replace hybrid circuits in telephone sets that can be operated in parallel with other phones.



**BLOCK DIAGRAM**



**PIN CONNECTION** (top view)



**ABSOLUTE MAXIMUM RATINGS**

Symbol	Parameter	Value		Unit
		DIP-14	SO-14	
$V_L$	Line Voltage (3 ms pulse)	15		V
$I_L$	Line Current	150		mA
$P_{tot}$	Total Power Dissipation, $T_{amb} = 55^{\circ}C$	1.0	0.6	W
$T_{op}$	Operating Temperature	- 20 to 55		$^{\circ}C$
$T_j$	Junction Temperature	- 65 to 150		$^{\circ}C$

**THERMAL DATA**

Symbol	Parameter	Value		Unit
		DIP-14	SO-14	
$R_{th\ j-amb}$	Thermal Resistance Junction Ambient Max	90	130	$^{\circ}C/W$

TEST CIRCUITS  
Figure 1.

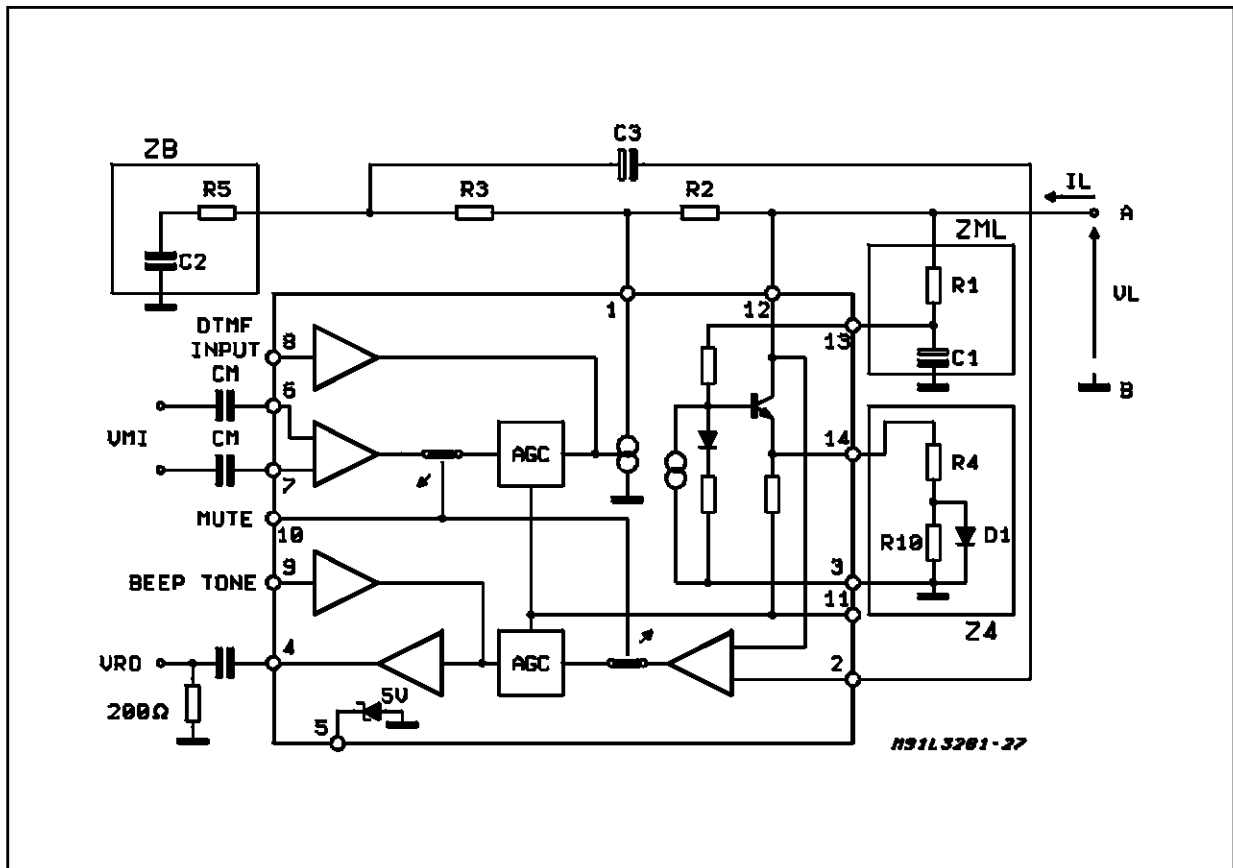


Figure 2.

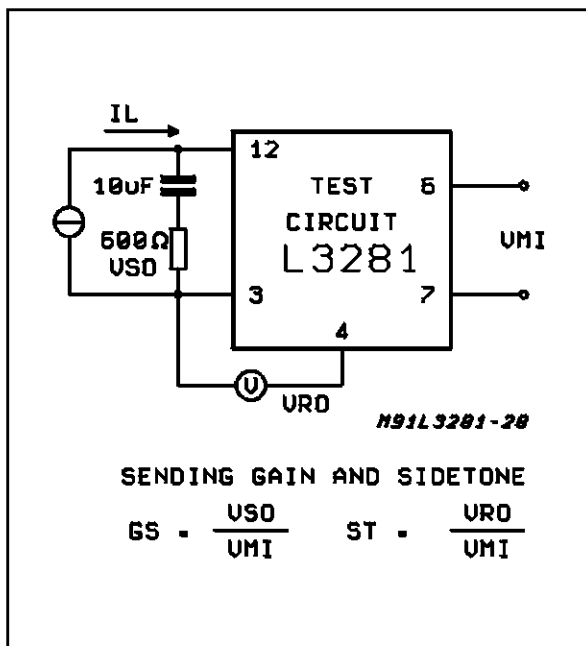
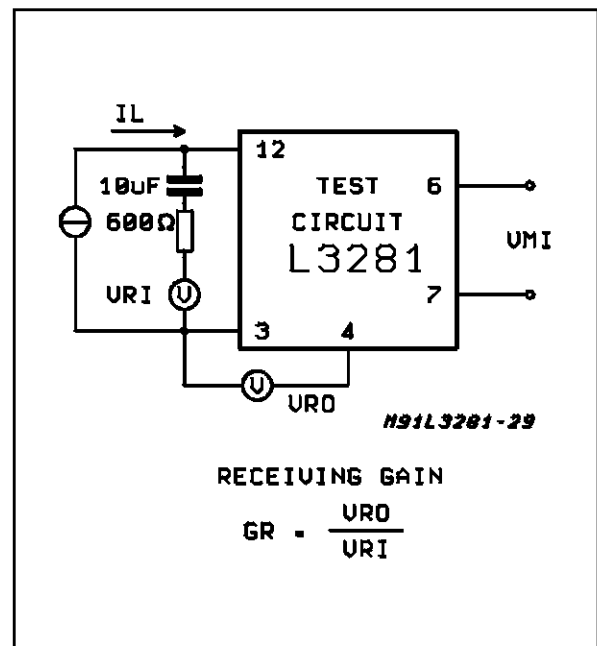


Figure 3.



**ELECTRICAL CHARACTERISTICS**  $I_L = 20$  to  $100\text{mA}$ ;  $R_4 = (51\Omega // \text{diode}) + 33\Omega$ ;  
 $T = 25^\circ\text{C}$ ;  $f = 1\text{kHz}$ ; Unless Otherwise Specified

Symbol	Parameter	Test Condition	Min.	Typ.	Max.	Unit
$V_I$	Line Voltage	$I_L = 6.5\text{mA}$		1.65		V
		$I_L = 20\text{mA}$		3.4	3.7	V
		$I_L = 50\text{mA}$		6.0	6.5	V
		$I_L = 80\text{mA}$		8	9.5	V
CMRR	Common Mode Rej. Ratio		50			dB
$G_{tx}$	Sending Gain	$V_{mi} = 10\text{mV}$ ; $I_L = 20\text{mA}$	30	31.5	33	dB
$DG_{tx}$	Delta Sending Gain	$V_{mi} = 10\text{mV}$ ; $I_L = 70\text{mA}$	- 7.2	-5.7	-4.2	dB
$THD_{tx}$	Sending Distortion	$V_{so} = 700\text{mV}$ ; $I_L = 20\text{mA}$			5	%
$N_{tx}$	Sending Noise	$V_{mi} = 0\text{V}$ ; $I_L = 50\text{mA}$		- 70		dB
$Z_{mi}$	Mic. Input Impedance	$V_{mi} = 10\text{mV}$	40			k $\Omega$
$G_{rx}$	Receiving Gain	$I_L = 20\text{mA}$ ; $V_{ri} = 0.2\text{V}$	- 10.7	- 9.2	- 7.7	dB
$DG_{rx}$	Delta Receiving Gain	$I_L = 70\text{mA}$ ; $V_{ri} = 0.2\text{V}$	- 7.2	- 5.7	- 4.2	dB
$THD_{rx}$	Receiving Distortion	$V_{ro} = 350\text{mV}$ ; Load = $350\Omega$			5	%
		$V_{ro} = 300\text{mV}$ ; $I_L = 10\text{mA}$			5	%
$N_{rx}$	Receiving Noise	$V_{ri} = 0\text{V}$		100		$\mu\text{V}$
$Z_{ro}$	Rec. Output Impedance	Load = $200\Omega$ ; $V_{ro} = 50\text{V}$		10		$\Omega$
	Sidetone	$V_{mi} = 10\text{mV}$		10	20	dB
$Z_m$	Line Match. Impedance	$V_{ri} = 0.2\text{V}$	500	600	700	$\Omega$
$V_{so}$	Sending Output Voltage	$I_L = 6.5\text{mA}$ ; THD = 5%	100			mV
$I_{ro}$	Receiving Output Current	$I_L = 6.5\text{mA}$ ; THD = 5%	0.5			mA
$MU_{lo}$	Mute Input Low	Dialing Mode		50	100	$\mu\text{A}$
$MU_{hi}$	Mute Input Open	Speaking Mode			1	$\mu\text{A}$
$G_{mf}$	DTMF Gain	$V_{mf\text{ IN}} = 10\text{mV}$	14.5	16	17.5	dB
$R_{mf}$	DTMF Input Impedance		5	10		k $\Omega$
$THD_{mf}$	DTMF Distortion	$V_{mf\text{ LN}} = 140\text{mV}$			5	%
$G_{beep}$	Beeptone Gain	$V_{beep\text{ IN}} = 25\text{mV}$		8.5		dB
$R_{beep}$	Beeptone Input Impedance		5.5	8		k $\Omega$
$THD_{beep}$	Beeptone Distortion	$V_{beep\text{ IN}} = 100\text{mV}$ ; $I_L = 20\text{mA}$		0.5	5	%
$V_z$	Zener Voltage (Pin 5)	$I_z = 1\text{mA}$	4.2	5.1	6.2	V
$I_{leak}$	Leakage Current, $V_{pin5} = 3\text{V}$			20		$\mu\text{A}$

## LOGIC OF MUTE SWITCHING

MUTE	DTMF	BEEP	MIC IMP	RX IMP
LOW (DIAL)	ACTIVE TO LINE OUTPUT	ACTIVE TO EARPHONE OUTPUT	MUTED	MUTED
OPEN (SPEECH)	ACTIVE TO LINE OUTPUT	ACTIVE TO EARPHONE OUTPUT	ACTIVE	ACTIVE

## CIRCUIT DESCRIPTION

## TWO TO FOUR WIRE CONVERSION

The L3281AB is based on a Wheatstone bridge configuration. To balance the bridge the following relation must be satisfied:

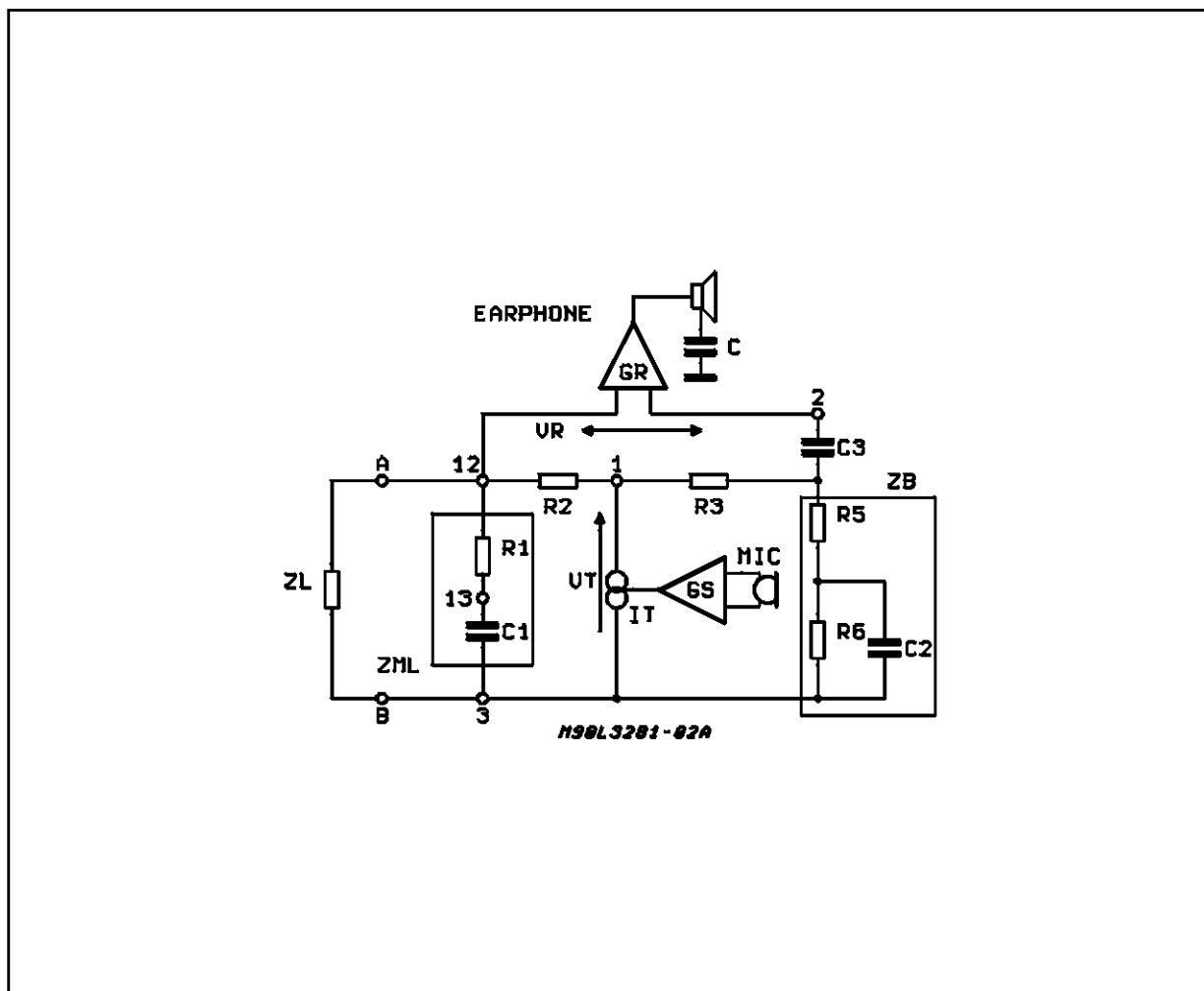
$$\frac{Z_L // Z_m}{Z_b} = \frac{R_2}{R_3}$$

The AC signal from the microphone is sent to one diagonal of the bridge (pins 1 and 3). A small percentage of the signal power is lost on  $Z_b$  (being  $Z_b > (Z_m // Z_i)$ ); the main part is sent to the line via  $R_2$ .

In receiving mode, the AC signal coming from the LINE is sensed across the second diagonal of the bridge (pins 12 and 2).

The impedance  $Z_m$  and  $Z_b$  can be complex.

Figure 4: 2/4 Wire Conversion



**DC CHARACTERISTIC**

The fig.5 shows the equivalent simplified circuit of the DC regulator that provides to give the opportune DC impedance Zdc.

$$V_L = \left[ \frac{I_{dc} \cdot Z_4}{R_B} \cdot (R_A + R_B) \right] + V_D + V_{R1}$$

$$V_L = \left[ (I_{dc} \cdot Z_4) \cdot \left( \frac{R_A}{R_B} + 1 \right) \right] + V_D + V_{R1}$$

since  $R_A = R_B$

$$V_L = (I_{dc} \cdot Z_4 \cdot 2) + V_D + V_{R1}$$

When  $I_L = 18 \text{ mA}$  and considering neglectable the  $V_D + V_{R1}$  variation versus line current :

$$Z_{DC} = \frac{\Delta V_L}{\Delta I_{dc}} = 2 \cdot Z_4$$

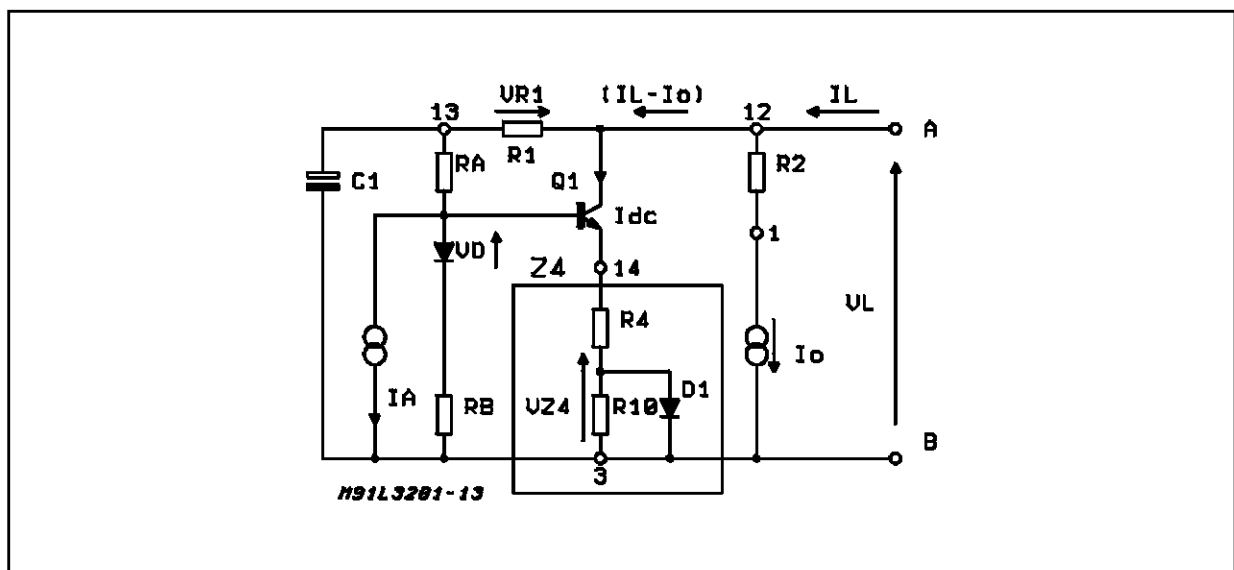
At  $I_L = 6.5 \text{ mA}$  no current flows through  $Z_4$  but only in the rest of the circuit for internal biasing ( $I_o; I_a$ ). The bias current  $I_o$  is fixed by the resistor  $R_2$ . The line voltage in this case is :

$$V_L = I_a R_A + V_{R1} = 1.6 \text{ V}$$

The Fig.6 shows the DC characteristic (voltage between pin 12 and pin 3 versus line current). The device own an equivalent zener voltage at pin 5 that can be used as supply voltage for electret microphone (see Block Diagram).

The value of the resistor  $R_2$  and the capacitor  $C_2$  should be chosen in order to not affect the AC line impedance. The Fig.7 shows the zener

**Figure 5:** Equivalent Simplified Circuit



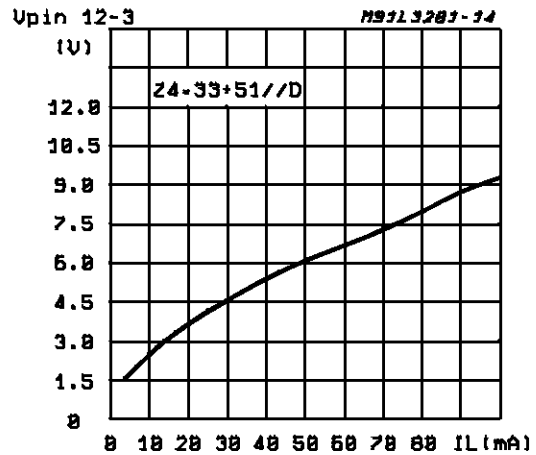
equivalent.

The zener voltage will be:

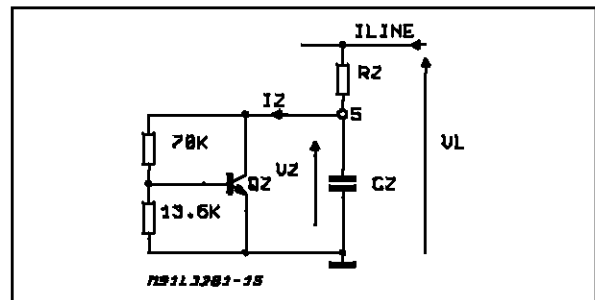
$$V_z = \left( \frac{70K}{13.6K} + 1 \right) \cdot V_{be}$$

It is possible to supply 1mA to the electret voltage if  $V_L > (1\text{mA} + I_z) \cdot R_z + V_z$

**Figure 6:** Low Voltage Speech Circuit.



**Figure 7:** Zener Equivalent.



**AC CHARACTERISTIC**

The AC Impedance measured at line terminals is equal to:

$$Z_m = (R1 + \frac{1}{j\omega C1}) // (R2 + R3 + Z_b)$$

The value of the capacitor C1 must be in the range of 22 μF to 100 μF.

The external resistor R1 can be replaced by a resistor/capacitor network in order to realize a complex Impedance Zm.

**TRANSMITTING CIRCUIT**

The first block of the TX stage is basically a differential amplifier which converts voltage to current. The inputs are internally polarized at 300 mVdc. The differential Input impedance is 60 KΩ to allow

a good matching to microphone. The AGC in TX is function of voltage at pin 14 in order to decrease to max gain of 5.5dB to 6.0dB when the line current increases.

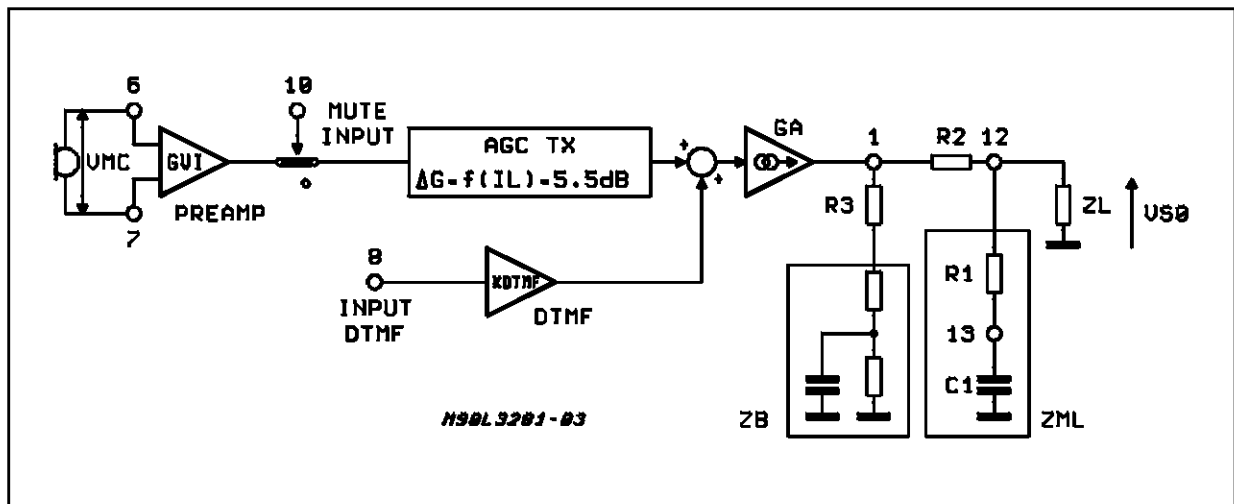
**RECEIVING CIRCUIT**

Fig.9 shows the equivalent receiving circuit. The differential input of RX signal across R2+R3 is transferred to the AGC block when the mute signal (pin 10) is not active.

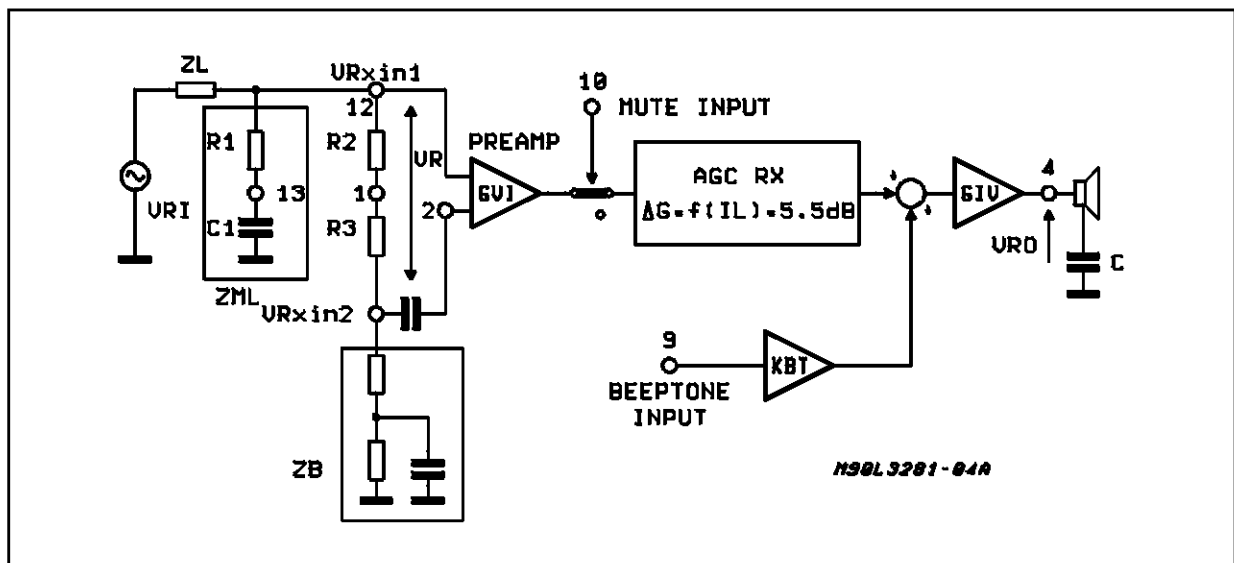
The AGC in RX is a function of the voltage at pin 14 and decreases the gain when the line current increases (5.5dB to 6.0dB).

The final stage is a single ended amplifier with low output impedance optimized to drive magnetic/dynamic transducers.

**Figure 8:** Equivalent Transmitting Circuit.

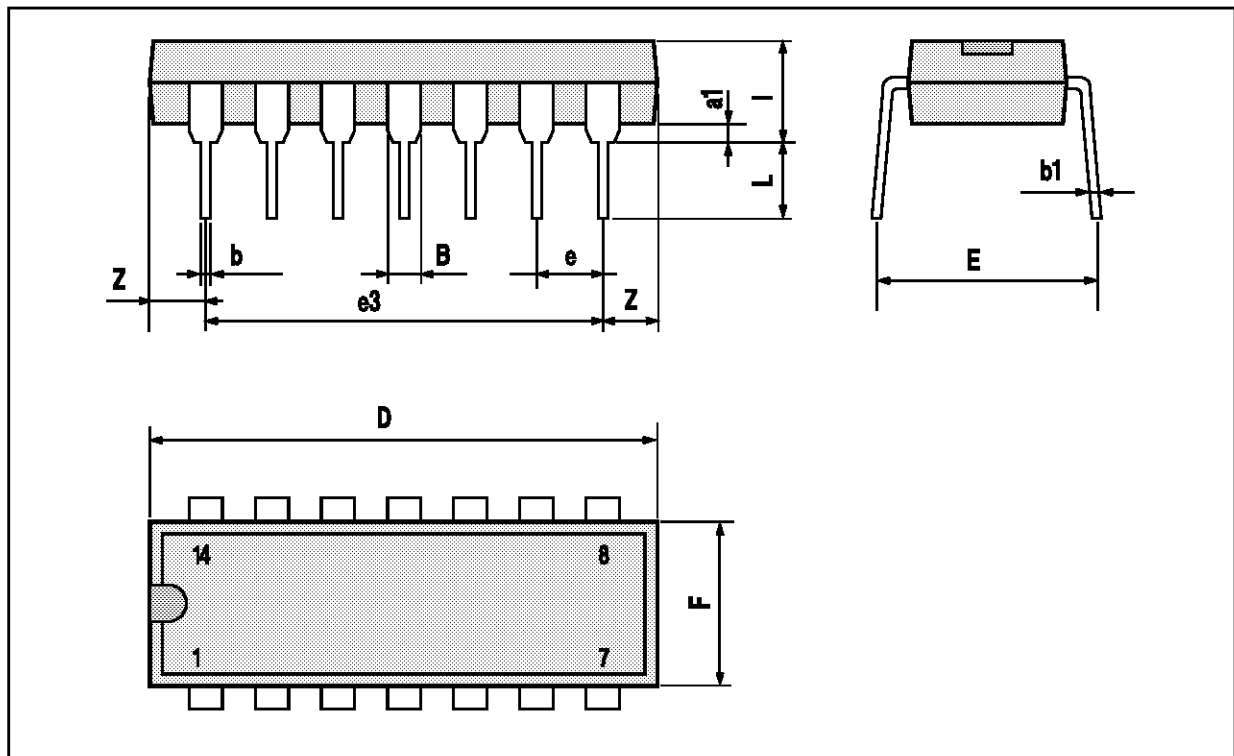


**Figure 9:** Equivalent Receiving Circuit.



DIP14 PACKAGE MECHANICAL DATA

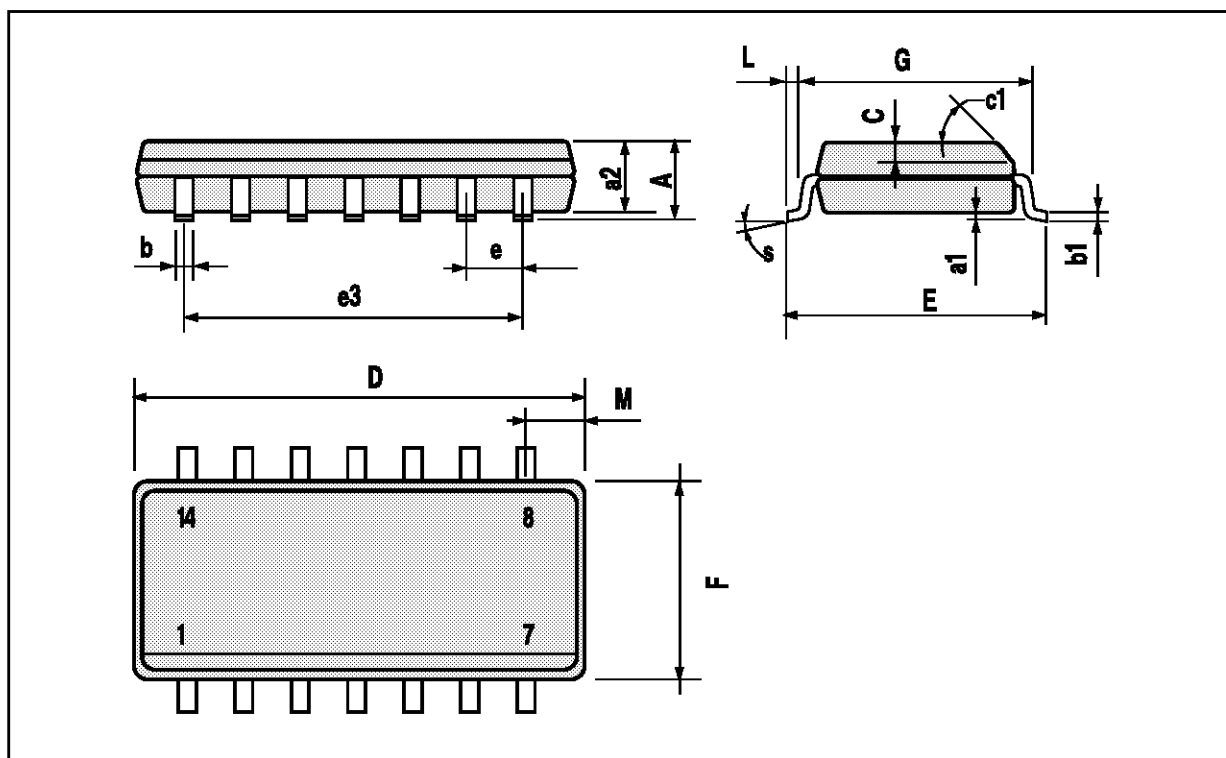
DIM.	mm			inch		
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.
a1	0.51			0.020		
B	1.39		1.65	0.055		0.065
b		0.5			0.020	
b1		0.25			0.010	
D			20			0.787
E		8.5			0.335	
e		2.54			0.100	
e3		15.24			0.600	
F			7.1			0.280
I			5.1			0.201
L		3.3			0.130	
Z	1.27		2.54	0.050		0.100





## SO14 PACKAGE MECHANICAL DATA

DIM.	mm			inch		
	MIN.	TYP.	MAX.	MIN.	TYP.	MAX.
A			1.75			0.069
a1	0.1		0.2	0.004		0.008
a2			1.6			0.063
b	0.35		0.46	0.014		0.018
b1	0.19		0.25	0.007		0.010
C		0.5			0.020	
c1	45° (typ.)					
D	8.55		8.75	0.336		0.344
E	5.8		6.2	0.228		0.244
e		1.27			0.050	
e3		7.62			0.300	
F	3.8		4.0	0.15		0.157
L	0.5		1.27	0.020		0.050
M			0.68			0.027
S	8° (max.)					



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