



**Piezoelectricity: Venerable Effect,
Modern Thrusts**

Arthur Ballato

ARL-TR-70

August 1994

NOTICES

Disclaimers

The findings in this report are not to be construed as an official Department of the Army position, unless so designated by other authorized documents.

The citation of trade names and names of manufacturers in this report is not to be construed as official Government endorsement or approval of commercial products or services referenced herein.

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate of any other aspect of this collection of information, including suggestions for reducing the burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE August 1994	3. REPORT TYPE AND DATES COVERED Technical Report	
4. TITLE AND SUBTITLE PIEZOELECTRICITY: VENERABLE EFFECT, MODERN THRUSTS			5. FUNDING NUMBERS	
6. AUTHOR(S) Arthur Ballato			8. PERFORMING ORGANIZATION REPORT NUMBER ARL-TR-70	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) US Army Research Laboratory (ARL) Electronics and Power Sources Directorate (EPSD) ATTN: AMSRL-EP-T Fort Monmouth, NJ 07703-5601			10. SPONSORING/MONITORING AGENCY REPORT NUMBER	
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)			11. SUPPLEMENTARY NOTES	
12a. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution is unlimited.			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) A synopsis of the piezoelectric effect is presented in the context of its history, traditional uses, and relation to crystal symmetry. Associated effects are briefly noted. Future prospects, particularly in the area of microelectromechanical systems/structures (MEMS) are discussed.				
14. SUBJECT TERMS Piezoelectricity; piezoelectric effect; micro-electro-mechanical devices			15. NUMBER OF PAGES 36	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT UL	

Table of Contents

Section	Page
Abstract	1
Introduction	1
Material Constitutive Equations	3
Electromechanical Coupling Factors	6
The Piezoelectric Effect and Crystal Symmetry	6
Piezoelectric Forces	9
Enantiomorphism	10
Optical Behavior	10
Pyroelectricity	11
Ferroelectricity	12
Piezoelectric Polymers	14
Piezoelectric Semiconductors	14
Quantum Effects in Piezosemiconductors	14
Wide Bandgap Semiconductors	15
Polytypism in Silicon Carbide	15
High Power Devices	16
Conclusion	16
References	17
Tables	21
Figures	26

List of Figures

Figure		Page
1	Couplings between the electrical, mechanical, and thermal fields	26
2	Piezoelectric binary semiconductors	27
3	Bandgap of important semiconductors	28

List of Tables

Table		
1	REPRESENTATIVE VALUES OF PIEZOCOUPLING FACTORS	21
2	THE SEVEN CRYSTALS SYSTEMS AND THIRTY-TWO POINT GROUPS	22
3	PIEZOELECTRIC [e] MATRIX FOR CLASS 1	23
4	PIEZOELECTRIC [e] MATRIX FOR CLASS 2	23
5	PIEZOELECTRIC [e] MATRIX FOR CLASS m	23
6	PIEZOELECTRIC [e] MATRIX FOR CLASS 222	23
7	PIEZOELECTRIC [e] MATRIX FOR CLASS mm2	23
8	PIEZOELECTRIC [e] MATRIX FOR CLASSES 4 AND 6	23
9	PIEZOELECTRIC [e] MATRIX FOR CLASS 4bar	23
10	PIEZOELECTRIC [e] MATRIX FOR CLASSES 422 and 622	24
11	PIEZOELECTRIC [e] MATRIX FOR CLASSES 4mm AND 6mm	24
12	PIEZOELECTRIC [e] MATRIX FOR CLASS 4bar 2m	24
13	PIEZOELECTRIC [e] MATRIX FOR CLASS 3	24
14	PIEZOELECTRIC [e] MATRIX FOR CLASS 32	24

15	PIEZOELECTRIC [e] MATRIX FOR CLASS 3m	24
16	PIEZOELECTRIC [e] MATRIX FOR CLASS 6bar	24
17	PIEZOELECTRIC [e] MATRIX FOR CLASS 6bar m2	25
18	PIEZOELECTRIC [e] MATRIX FOR CLASSES 23 AND 4bar 3m	25

Abstract

A synopsis of the piezoelectric effect is presented in the context of its history, traditional uses, and relation to crystal symmetry. Associated effects are briefly noted. Future prospects, particularly in the area of microelectromechanical systems/structures (MEMS), are discussed.

Introduction

Piezoelectricity was discovered by the brothers Curie in 1880. They found that, in certain materials such as zincblende, tourmaline, cane sugar, topaz, and quartz, mechanical stresses were accompanied by the production of electric surface charges. The following year, Lippmann, from thermodynamic considerations, predicted the converse effect: an imposed voltage produces mechanical deformations. The name "piezo" derives from the Greek, meaning "to press"; in more modern terminology, we say that the effect couples electric and elastic phenomena, as discussed below. (It is interesting to note that, in the 19th Century, when mechanics reigned supreme, luminaries like Kelvin and Maxwell "explained" light phenomena in terms of mechanical models such as coupled gyroscopes. Today, electromagnetism and electronics reign, and the art of mechanics seems in many respects an all-but-forgotten discipline. To present the workings of modern mechanical structures such as microactuators to the "real world," we now make use of equivalent electrical circuits!)

The piezoelectric effect remained a curiosity until the early 1920s when its presence in quartz was utilized to realize crystal resonators for the stabilization of oscillators, thereby launching the field of frequency control.¹ With the introduction of quartz control, timekeeping moved from the sun and stars to small, man-made sources that exceeded astronomy-based references in stability. Since then, devices based on piezoelectricity have expanded dramatically in application. The quartz resonator has continued to evolve to become a device capable today of precision one million times greater than the original, and serves as well as the "flywheel" in atomic frequency standards, which make frequency the most accurate entity known.²

Piezoelectric devices are additionally used as transducers in applications from telephone speakers to sonar arrays; a newer and rapidly burgeoning area of utilization is the integral incorporation of mechanical actuation and sensing microstructures into electronic chips. These microelectromechanical structures/systems (MEMS) promise signal sensing, processing, and outputting features unattainable by exclusively electronic/photonic means. In many traditional applications, applied voltages conform to the norms for electronic circuits; accompanying mechanical displacements are then usually nanometers or less. Newer configurations available today for actuators often have much larger amplitudes at comparable voltages. Key to MEMS exploitation is the piezoelectric cantilever bimorph, consisting of a two-layer laminate, fashioned like a subminiature diving board.³⁻⁵ Usually the bimorph substrate is silicon, with thin patches of piezoelectrically active films of materials such as aluminum nitride or zinc oxide to drive the structure into flexural motion. This bending mode delivers the greatest possible displacement for a given driving voltage, so, for example, a proof mass located at the "diver's" position provides the greatest sensitivity to accelerations; lenses/mirrors so situated yield maximal photonic excursions, while FET gates or optical waveguides at the support end experience mechanical stress maxima for modulating the electronic or optical variables. The bimorph MEMS devices provide otherwise unavailable capabilities, and require piezoelectricity as the transduction mechanism. An alternative configuration is the laminated plate, where aluminum nitride or zinc oxide thin-film layers drive silicon plates for integrated frequency control devices.⁶

One of the most appealing aspects of piezoelectricity for modern applications is the compelling immediacy and simplicity of the transduction mechanism. Micro- and nano-electronics are built upon the behavior of charged species subjected to electric fields; the extreme miniaturization of these structures is owed in large measure to their ability to take on a capacitor-like form.⁷ Bulky inductors are banished and done without, and thin, planar electrodes introduce the electric fields to operate the circuits. These fields also provide the forces required to drive mechanical motions in a piezoelectric device. Elastic field/mechanical considerations are therefore incorporated into the operations of modern electronic components in a clean, efficient, and very direct manner, by making use of the voltages resident on the chips, via the piezoeffect.

Material Constitutive Equations

Formally stated, piezoelectricity couples the mechanical stress (T) and strain (S) fields with the electric intensity (E) and displacement (D) fields. Depending on variable choice, four sets of material constitutive relations are defined for the linear case of insulating dielectric materials; these are, in compressed matrix form.⁸⁻¹⁰

$$[T] = [c^E][S] - [e]^T[E] \quad (1a)$$

$$[D] = [e][S] + [\epsilon^S][E] \quad (1b)$$

$$[T] = [c^D][S] - [h]^T[D] \quad (2a)$$

$$[E] = -[h][S] + [\beta^S][D] \quad (2b)$$

$$[S] = [s^E][T] + [d]^T[E] \quad (3a)$$

$$[D] = [d][T] + [\epsilon^T][E] \quad (3b)$$

$$[S] = [s^D][T] + [g]^T[D] \quad (4a)$$

$$[E] = -[g][T] + [\beta^T][D] \quad (4b)$$

Because the electric variables [E] and [D] are tensors of rank 1 (i.e., three-dimensional vectors), and the mechanical variables [T] and [S] are tensors of rank two which have been converted to six-dimensional vectors, [c^E], [c^D] and [s^E], [s^D] are (6 X 6) symmetric matrices representing the elastic stiffnesses and compliances at constant E and D; [ϵ^S], [ϵ^T] and [β^S], [β^T] are symmetric (3 X 3) dielectric permittivity and impermeability matrices at constant S and T, while [e], [h], [d], and [g] are (3 X 6) piezoelectric matrices. A prime denotes transpose. Alternative formulations, using the electric polarization vector [P] in place of [D], are sometimes used, particularly in electrooptic applications; the piezoelectric polarization [a] and [b] matrices are then used.¹¹ We subsequently drop the matrix brackets [] for simplicity.

The four equivalent pairs of material constituent equations (1) - (4) differ in their combinations of independent and dependent variables; the material constants used in the sets are interrelated. These relations may be determined by first pairing the equations sharing common variables:

$$\begin{aligned} (1a) \text{ and } (3a): & T, S, E \\ (2a) \text{ and } (4a): & T, S, D \\ (1b) \text{ and } (2b): & E, D, S \\ (3b) \text{ and } (4b): & E, D, T \end{aligned}$$

One variable is then eliminated from each pair, yielding the required results. For example, from (1a) and (3a) we have:

$$T = c^E S - e' E = c^E (\epsilon^{ET} + d' E) - e' E = c^E \epsilon^{ET} + c^E d' E - e' E = T$$

Therefore

$$c^E s^E = I \text{ and } e = d c^E \text{ or } d = e s^E.$$

The full set obtained in this manner is:

$$\epsilon^+ \beta^+ = c^* s^* = I, \text{ where } + \text{ is } T \text{ or } S, \quad * \text{ is } E \text{ or } D, \text{ and } I = \text{unit matrix}$$

and

$$e = \epsilon^S h = d c^E; \quad d = \epsilon^T g = e s^E; \quad h = \beta^S e = g c^D; \quad g = \beta^T d = h s^D$$

In addition to these multiplicative identities, there exist difference relations between the dielectric quantities at constant stress and at constant strain and between the elastic constants at constant electric field and at constant displacement. To obtain these, we equate the right hand sides of the following pairs of equations: (2b) = (4b); (1b) = (3b); (3a) = (4a); and (1a) = (2a). These are then compared respectively to (-g) times (2a); (e) times (3a); (g') times (3b); and (h') times (1b). After some algebra, the following are found:

$$(c^D - c^E) = h' e = e' \beta^S e = h' \epsilon^S h$$

$$(s^E - s^D) = g' d = d' \beta^T d = g' \epsilon^T g$$

$$(\epsilon^T - \epsilon^S) = e d' = e s^E e' = d c^E d'$$

$$(\beta^S - \beta^T) = g h' = h s^D h' = g c^D g'$$

These relations show that the presence of piezoelectricity modifies the elastic and dielectric constants, that the mechanical (elastic) conditions must be specified for dielectric quantities, and that electric conditions must be specified for elastic quantities. To obtain an order of magnitude estimate of the size of the effect, we may neglect the matrix nature of the above equations and treat them as scalars. Then, using the symbol Δ to represent differences, we have, from the first difference relation:

$$\frac{\Delta C}{C} = e\beta^S e/c = e^2 /(\epsilon c) = k^2,$$

and similarly for the other relations. Thus the fractional differences are determined by dimensionless combinations of elastic, piezoelectric, and dielectric constants. We call each combination the square of a quantity, k , known as a piezoelectric coupling factor; these will be discussed subsequently.

Units of the various quantities are as follows.

Field tensors:

Mechanical stress, T:	pascal, Pa = newton/meter ² = N/m ²
Mechanical strain, S:	meter/meter = m/m = dimensionless
Electric intensity, E:	volt/meter = V/m
Displacement, D:	coulomb/meter ² = C/m ²

Matter tensors:

Permittivity, ϵ^T , ϵ^S :	farad/meter = F/m = C/(m-V)
Impermeability, β^T , β^S :	meter/farad = m/F = (m-V)/C
Piezo constants: e	C/m ² = N/(m-V)
d	m/V = C/N
h	V/m = N/C
g	m ² /C = (m-V)/N
Elastic stiffness, c^E , c^D	Pa = N/m ² = J/m ³
Compliance, s^E , s^D	(Pa) ⁻¹ = m ² /N = m ³ /J

The material constitutive relations given may be further broadened to include couplings to thermal, magnetic, and other fields. Figure 1 depicts the phenomenology arising from the mutual couplings among the electric, elastic, and thermal fields. The outer quantities are the thermodynamic intensive variables (generalized forces); the inner quantities are the extensive variables (generalized displacements).^{1, 12, 13}

Piezoelectricity is a linear effect; reversal of the electric field reverses the mechanical deformation. Conditions for its existence in crystals are given below. Electrostriction, on the other hand, exists in all dielectric solids. It is a deformation quadratic in the polarization field.¹⁴
¹⁵ Biased electrostriction, where small field variations are superimposed on a constant component, is phenomenologically equivalent to linear piezoelectricity; this artifice may be used with nonpiezoelectric crystals such as silicon, but the coupling depends upon the bias, and is often not large.

Resonance measurements on thickness mode plate vibrators and pulse-echo (transit-time) measurements determine values for the matrix elements $[c^E]$, $[e]$, and $[\epsilon^S]$ from which the other material parameter sets may be computed if desired. Resonance measurements on low frequency bar and rod specimens lead alternatively to determination of the $[s^E]$, $[d]$, and $[\epsilon^T]$ set.¹⁶⁻¹⁸ These dynamic techniques are both more accurate and more precise than static measurements.

Electromechanical Coupling Factors

Electromechanical coupling factors k ($0 \leq k < 1$) are dimensionless measures of efficacy of piezoelectric transduction, and are far more important than the piezoelectric constants taken by themselves. They appear in considerations of bandwidth and insertion loss in transducers and signal processing devices, in location and spacing of critical frequencies of resonators, and in electrical/mechanical energy conversion efficiency in actuators. For high frequency plate resonators, coupling factors have the generic form $k = e / \sqrt{\epsilon c}$; for low frequency bar and rod vibrators, the form becomes $k = d / \sqrt{\epsilon s}$; alternative forms using the "h" and "g" piezo parameters are used as well.^{13, 18} These quantities are also called piezocoupling factors; representative values are listed in Table 1. Additional material values are contained in Refs.¹⁹⁻²⁰

The Piezoelectric Effect and Crystal Symmetry²¹⁻²⁵

Crystallographers have, over the centuries, cataloged the various geometrical arrangements of atoms that can exist in crystal structures. The starting point is the unit cell, which normally contains the smallest grouping of atoms representing the chemical formula of the substance. In a crystal, this cell, with its particular size, shape, and arrangement of atoms within it, is repeated over and over in three dimensions. The result is an orderly stacking of cells that has translational invariance, meaning that moving one's observation point by an integral number of cells in any direction yields a completely equivalent view. The shapes of the unit cells suitable for such stacking fall into seven general types, or systems. These are: triclinic, monoclinic, orthorhombic, tetragonal, trigonal, hexagonal, and cubic (also called isometric). When the actual arrangements of atomic species possible within the unit cell is compounded with the possible shapes of unit cells, the total number of independent geometrical arrangements available in three dimensions is 230. These are the space groups.

In most practical situations, one deals with a continuum approximation, where considerations of the exact placement of atoms in the cells are not important, and the situation simplifies considerably. For example, elasticity is described by the few phenomenological stiffness and compliance constants used in the equations above. These numbers arise from a "smearing-out" of the effects of the individual interatomic potentials; only important are the directional aspects stemming from the atomic arrangements, not the arrangements themselves. Variation with direction of continuum properties such as acoustic wave speed is known as anisotropy. All the requisite geometric information specifying the varieties of anisotropy reside in the classification that the crystallographers call the point groups. These are only 32 in number, and arise simply from three types of symmetry elements: pure rotation axes (1-, 2-, 3-, 4-, or 6-fold), planes of reflection (mirror) symmetry, and axes of rotatory inversion (rotation followed by inversion through a center). The point groups are described by their Hermann-Mauguin symbols; these are shorthand listings of the symmetries. The names "point group" and "crystal class" are used synonymously. The classes are arranged in Table 2 according to the seven crystal systems, labeled "I" through "VII." Systems IV through VII are further subdivided into "a" and "b" categories; these are discussed briefly below.

The crystallographic point-group symmetry elements completely determine the form and symmetries of the elastic, piezoelectric, and dielectric matrices that appear in the constitutive relations given earlier. The specific values of the individual components result, of course, from the particular substance considered. The piezoelectric $[e]$ and $[h]$ matrix forms for each point group are identical; the $[d]$ and $[g]$ are likewise the same, but differ from the $[e]$, $[h]$ sets by factors of 2 for certain matrix elements in classes 3, 32, 3m, 6bar, and 6bar m2 because of the conversion between the tensor and matrix formulations.

That the material tensor term schemes are determined by the point group symmetry is a manifestation of Neumann's Principle which may be stated in several equivalent ways:²²

- The symmetry elements of any physical property of a crystal must include all the symmetry elements of the point group of the crystal.
- Every physical property of a crystal must possess at least the symmetry of the point group of the crystal.
- Any kind of symmetry which is possessed by the crystallographic form of a material is possessed by the material in respect of every physical property.

Of the 32 point groups, 11 have centers of symmetry (these are referred to as the Laue groups), and therefore cannot be piezoelectric, because piezoelectricity is a polar effect; see the column of Table 2 labeled "centric." The division of crystal systems IV, V, VI, and VII into "a" and "b" categories is based upon X-ray patterns. Classical X-ray diffraction has the effect of adding a center of symmetry to the intrinsic symmetry of the crystal under study; each acentric point group appears as one of the eleven centric Laue groups. The groups that appear as holohedral under X-ray examination are assigned to the "b" category; the remainder are put in the "a" category. The structure in each of the seven systems that possesses the highest point group symmetry compatible with that system is the holohedral class; these are denoted by the letter "h." Class 432 lacks a center of symmetry, but has other symmetries that, taken together, preclude the existence of piezoelectricity. The 20 piezo classes are: triclinic class 1; monoclinic classes 2 and m; orthorhombic classes 222 and mm2; tetragonal classes 4, $\bar{4}2m$, 422, 4mm, and $\bar{4}2m$; trigonal classes 3, $\bar{3}2$, and 3m; hexagonal classes 6, $\bar{6}2m$, 622, 6mm, and $\bar{6}2m$; and cubic classes 23 and $\bar{4}3m$. See the columns of Table 2 labeled "acentric."

Tables 3 - 18 give the [e] forms of the piezoelectric matrices (also called "term schemes") for the twenty piezo classes; four pairs share the same schemes, so that there are but sixteen independent matrices. Tables 15, 14, 11, and 18 are, respectively, the piezo schemes of four popular crystal classes: 3m (the strong piezoelectrics lithium niobate and lithium tantalate), $\bar{3}2$ (quartz and langasite), 6mm (AlN and ZnO, used in thin-film form on Si for MEMS devices, and transversely isotropic, poled polycrystalline ceramics such as lead zirconate titanate), and $\bar{4}3m$.

Nearly all compound semiconductors, such as gallium arsenide, indium phosphide, and silicon carbide are members either of class 6mm or of class 4bar 3m. Class 4mm, which includes the popular piezoelectric transducer and filter material lithium tetraborate, has an [e] matrix identical in form to that of class 6mm.

The matrices are to be read in conjunction with equations (1) to (4) as follows. An applied electric field, E_i , directed along the X_i axis, produces, according to the constitutive relations given earlier, mechanical stresses, T_λ equal to $(-e_{i\lambda} E_i)$. The axis index "i" takes the values 1,2,3; these correspond to orthogonal X,Y,Z axes assigned to each crystal class by standard convention. The index "λ" takes on values 1,2,...,6; these represent the tensor indices according to the scheme: 1 → 11; 2 → 22; 3 → 33; 4 → 23 or 32; 5 → 13 or 31; 6 → 12 or 21. Each of the three rows of the [e] matrix is "driven" by a different electric field component, and each will produce up to six stress components. For example, in class 3m materials (Table 15), an electric field along the Y axis (E_2) will produce, according to equation (1a), compressive or tensile stresses along both the X and Y axes, but not along the Z axis. Moreover, the X- and Y-directed stresses are equal and opposite in sign, because $e_{21} = -e_{22}$. The longitudinal stress along Z vanishes because $e_{23} = 0$. In addition, E_2 produces a shear stress $T_4 = T_{23} = T_{32}$, via the constant e_{24} , which, for this class, equals e_{15} .

Alternatively, an applied strain S_μ , produces a dielectric displacement D_j via the $D_j = e_{j\mu} S_\mu$ portion of constitutive equation (1b). Continuing the example of a class 3m material, it will be seen that a shear strain $S_4 = S_{23} = S_{32}$ leads, because of the presence of the piezo coefficient e_{24} , to a component of dielectric displacement D_2 , and consequent polarization charge accumulation on free surfaces having normals in the X_2 (Y) direction.

Piezoelectric Forces

The volumetric force density is given by

$$F_j = \partial T_{ij} / \partial X_i.$$

Piezoelectric force density components may be found from (1 a) as

$$-\partial (e_{k\lambda} E_k) / \partial X_i.$$

This means that piezoelectric forces may arise either from spatial gradients of the piezoelectric constant, or from spatial gradients of the electric field. In single crystal materials such as quartz, it is not usual that the piezoelectric "constant" will vary from place to place, although the presence of microtwins, etc., makes this a possibility. In polycrystalline materials such as ceramics, and in ferroelectric single crystal materials such as lithium niobate and lithium tantalate (see below), this situation arises. In practice, sometimes by design.

Usually, piezoelectric forces arise because of spatial gradients in the applied electric field. An excellent example of this is the use of interdigital transducer (IDT) electrode arrays to produce surface acoustic waves (SAWs) and related acoustic wave types. From the electrode array placement, and the crystal term scheme (rotated, if necessary, to the orientation of the crystal surface), one may find the force-components, and infer qualitatively if a particular type of wave motion may be driven piezoelectrically by the electrode array.²⁶

Enantiomorphism

Eleven crystal classes are devoid of a plane of symmetry. These are 1, 2, 222, 4, 422, 3, 32, 6, 622, 23, and 432. In these classes, two structures of the same kind can exist; each is the mirror image of the other. These are known as enantiomorphic pairs; quartz (class 32) is probably the most famous example, with "left-" and "right-handed" varieties. The handedness arises at the atomic level from the spiral arrangement of the SiO₂ molecules in the crystal, but from Neumann's Principle, the external appearances of the facets in completely developed specimen-pairs exhibit the mirror-symmetric aspect macroscopically. The enantiomorphic groups are indicated in Table 2 by the symbol "e."

Optical Behavior

The first-order optical behavior of materials is governed- by the dielectric permittivity tensor. In crystals, three cases are distinguished, depending on whether the principal dielectric constants are all equal (isotropic medium), two are equal, and one is unequal (uniaxial medium), or all are unequal (biaxial medium); the corresponding crystal class distributions are indicated in Table 2 in the last column.

One second-order optical effect of importance T is that of optical activity, or gyration. In optically active substances, the passage of plane polarized light is accompanied by a rotation of the direction of the polarization vector. The effect comes about from the chiral nature of the molecules comprising the material. A common example is a sugar-water solution. Molecules of sugar (dextrose or levulose) are chiral in nature; a solution comprised of sugar of either handedness rotates a light beam accordingly, despite the fact that the molecules are randomly oriented in the solution. This is because reversal of the axis of a spiral does not reverse its handedness, so no cancellation of the effect takes place. Optical activity is characterized phenomenologically by an axial second rank tensor called the gyration tensor.

Only crystals that lack a center of symmetry can be optically active (gyrotropic). Crystals that are enantiomorphic are necessarily gyrotropic; in these eleven classes the gyration tensor determinant is nonvanishing. Optical activity also exists in four nonenantiomorphic classes: m , $mm2$, $4bar$, and $4bar 2m$; in these classes the gyration tensor determinant vanishes. The symbol "o" denotes these groups in Table 2.

Two effects that are closely associated with piezoelectric materials are pyroelectricity and ferroelectricity.

Pyroelectricity

Of the 20 piezoelectric point groups, 10 contain a unique polar axis. In Table 2, the symbol "p" appears in the polar column to indicate that the classes therein are both piezoelectric and pyroelectric, while the symbol "p" in the nonpolar column indicates piezoelectric classes only.¹ The entry "p" with an overbar, appearing with class 432, indicates that this class is nonpiezoelectric. Crystals in the polar classes possess electric dipole moments along their polar axes. When the crystals are subjected to a uniform change of temperature, electric charges accumulate on the ends of the polar axes. This phenomenon is known as pyroelectricity; because a temperature change (a scalar) produces a charge separation, and consequently an electric field (a vector), the pyroelectric coefficients form a tensor of rank 1, i.e., a vector, and would be represented as a (3 X 1) matrix if we were to extend the constitutive equations given earlier to include this effect.

The pyroelectric classes are: 1, 2, m , $mm2$, 4, $4mm$, 3, $3m$, 6, and $6mm$. Thus, α -SiC and lithium niobate are pyroelectric, while, β -SiC, quartz, and gallium arsenide are not. The presence of piezoelectricity is necessary but not sufficient for a crystal to be pyroelectric.

The name ferroelectricity is given to those polar crystals capable of having the spontaneous polarization along the polar axis reversed, usually in response to an applied electric field. The name is derived by analogy with ferromagnetism, but in the magnetic case the very atoms themselves possess permanent magnetic moments; in the electric case, the permanent electric moment is a property of the placement of the atoms within the unit cells of the structure. The orientations of the intrinsic atomic magnetic moments permitted in ferromagnetic crystals, in addition to the spatial atomic arrangements allowed, produce additional complexity with regard to crystal symmetry. When the spin orientations are taken in combination with the thirty-two conventional point groups, the result is ninety crystallographic magnetic point groups. Coupling to the magnetic field variables is not considered further here.

The presence of the ferroelectric state requires that the crystal be of a pyroelectric class; the converse is, however, not true. One cannot conclude *a priori* that a pyroelectric crystal is ferroelectric; one must settle this issue experimentally or by numerical simulation. The ferroelectric state usually exists only below a certain critical temperature, called the Curie temperature or Curie point. Above this point, the material may belong to a class that is not pyroelectric, or even piezoelectric. Upon cooling through the Curie point, the crystal undergoes a phase transition (which may be either first- or second-order), where the atoms of the structure shift their positions slightly and the crystal changes its symmetry, usually from a nonpolar form, to the symmetry of a pyroelectric class.

Since the ferroelectric state has reversible dipoles, upon cooling it is a matter of chance which polarity will be assumed; near the Curie point the structure is very susceptible to disturbance. Because the lattice is relatively unstable around this point, small forces can produce large effects; this is the case with the dielectric constant. This quantity is the measure of dielectric displacement produced in response to an applied electric field. Near the Curie point, dielectric constants assume very large values; this behavior ("dielectric anomaly") led to the initial discovery of this class of materials. Very often ferroelectrics have large piezoelectric coupling values.

The archetypical ferroelectric is Rochelle salt ($\text{KNaC}_4\text{H}_4\text{O}_6 \cdot 4\text{H}_2\text{O}$). This crystal is unusual in that it possesses two Curie points. When cooled into the ferroelectric phase, it passes from class 222 to class 2. Its piezo effect was established by the Curie brothers in 1880. Pockels found the dielectric anomaly in 1894. It was used for ultrasonics applications in the early 20th Century, but because of its solubility in water it is not considered any longer to be a practical material for these uses.

Barium titanate, another historically important material, exists in the nonpiezoelectric perovskite class $m\bar{3}m$ above its upper Curie point, and under-goes a succession of structural phase transformations, passing through $4mm$ and $mm2$ classes before reaching $3m$ symmetry as the temperature is reduced.

Piezoelectric ceramics, such as lead zirconate titanate ($\text{Pb}(\text{Ti,Zr})\text{O}_3$), are solid solutions comprised of microscopic crystallites, each of which is ferroelectric; the material originally is macroscopically isotropic at all temperatures because of the random orientations of the crystallites. When cooled through the Curie point in the presence of a static electric field (a process called "poling"), the domains are preferentially oriented and frozen into a configuration where the body is macroscopically piezoelectric. It remains isotropic perpendicular to the field axis, but the isotropy is destroyed in the parallel direction. The result is cylindrical polar symmetry (transverse isotropy), represented by the symbol $oo\bar{m}$; as far as the elastic, piezoelectric, and dielectric matrices are concerned, the schemes of coefficients are identical to those for the class $6mm$. In fact, for all tensors up to and including rank five, the schemes of coefficients are identical to the corresponding class $6mm$ schemes; one may, therefore, differentiate transversely isotropic substances from $6mm$ crystals by measuring higher-order effects, e.g., third-order elastic constants (tensor of rank six).

Above the Curie point, most (but not all) ferroelectrics belong to one of three classes: 222 (e.g., Rochelle salt), $4\bar{2}m$ (e.g., potassium dihydrogen phosphate, KDP), and $m\bar{3}m$ (e.g., BaTiO_3); in the ferroelectric state, most of the practically important compounds likewise fall into three classes: $4mm$, $3m$, and $mm2$.

Unpoled single crystal ferroelectrics such as lithium niobate are comprised of domain regions where the directions of polarization are collinear, but oppositely directed. The presence of domains can alter various macroscopic properties (e.g., piezoelectric voltage), and not change others (e.g., index of refraction).

Piezoelectric Polymers¹⁹

Certain polymers, such as polyvinyl chloride (PVC), polyvinyl fluoride (PVF), and polyvinylidene fluoride (PVF₂ or PVDF) can be made piezoelectric by a combination of mechanical stretching and electric field poling at elevated temperatures. The induced anisotropy varies with the polymer and the subsequent treatment; polymethyl glutamate, for example, has symmetry $\infty 22$, which is equivalent to class 622 for the properties discussed here. PVDF sheet, poled along the thickness, belongs to class ∞mm (equivalent to 6mm); uniaxial stretching or rolling converts it to orthorhombic class $mm2$, while a biaxial stretching again produces class ∞mm .

Piezoelectric Semiconductors²⁹⁻³¹

In the case of semiconductors, the piezoelectric equations are broadened to incorporate the further coupling to charge transport mechanisms. It is apparently not well appreciated how widespread is the phenomenon of piezoelectricity in semiconductors. The single-element semiconductors silicon and germanium have, of course, no piezo effect because of the inherent symmetry by which the atoms are arrayed in their crystals; they share with diamond the perovskite structure of point group $m3m$. Binary semiconductors, however, because of the dissymmetry of the two atomic species, are generally piezoelectric. Figure 2 provides a partial listing of these materials, grouped according to the columns of the periodic table; it is seen that the compounds fall into two categories: those marked "c" belong to the cubic point group $4\bar{3}m$, the sphalerite or zinc blende structure, while those indicated with "h" belong to the hexagonal point group $6mm$, the wurtzite structure.

Piezosemiconductors have an encouraging future because of the appealing promise of monolithic, integrated, mixed-effect devices; for example, electronic drivers that modulate photonic processors via submicroscopic mechanical actuators containing optical components.

Quantum Effects in Piezosemiconductors

References 32-36 discuss new acoustic wave anomalies in experiments with surface acoustic waves on GaAs/AlGaAs heterostructures driven by their piezoeffect. These experiments are carried out at low temperatures; one may anticipate future areas of application.

A growing number of advanced applications, particularly those involving high power and high temperature devices require semiconductors with wide bandgaps. For a variety of reasons, silicon carbide and diamond are particularly apt candidates for these uses; see Figure 3.⁴¹ Diamond is nonpiezoelectric in both its crystalline (m3m) and amorphous forms, whereas both the cubic and hexagonal forms of silicon carbide are piezoelectric in nature. In those applications necessitating mixed-effect devices that incorporate traditional semiconductor ideas with mechanical forces and motions, the piezosemiconductors are highly commended: where, in addition, these devices are required for high temperature operation, then silicon carbide is a material of choice. The cubic form, β -SiC, has a bandgap energy of 2.2 eV, while the hexagonal form, α -SiC, has a bandgap energy of 2.9 eV; these are significantly higher than that of GaAs, with a value of 1.43 eV. The piezocoupling values are comparable; see Table 1. As material quality continues to improve with attainment of lower impurity and defect levels, and as semiconductor processing skills increase with silicon carbide, one may anticipate the extension of smart MEMS technology to a variety of hostile but environmentally important areas.

Polytypism in Silicon Carbide⁴²⁻⁴⁴

Alpha-SiC, of symmetry 6mm, exhibits a curious variety of forms known as polytypes. Polytypism arises because the molecules may be stacked in an infinite variety of zig-zag sequences, while preserving the point group symmetry. Theoretically, the number of polytypes is unbounded; practically, hundreds are known, each with a different unit cell, and with a variety of space groups and X-ray diffraction patterns. Condensation under different growth conditions is thought to determine the polytype produced; the most common varieties are known as 6H and 4H. Each polytype can theoretically differ in its phenomenological constants, because some bond angles and lengths vary, in most cases the differences are imperceptible, but differences of several percent in the elastic constants of 6H and 4H material have been reported.³⁸ Beta-SiC, because of its $4\bar{3}m$ symmetry, cannot have polytypes.

High Power Devices

For applications such as acoustic resonators, the power level is usually low. Here silicon carbide of either the alpha or beta variety is an attractive choice for high temperature operation. The acoustic losses are at present not very high, so the quality factor (Q) is quite acceptable; as the material quality continues to improve with attainment of lower and lower impurity levels and defects, Q values will substantially increase in the future, leading to higher stability oscillators for "hot" environments.

For acoustic transducer operation, where power levels are a concern at any temperature, silicon carbide, in the beta (cubic) form, is a desirable material because of its structural stability, and its nonferroelectric nature. Lithium niobate and lithium tantalate, strongly piezoelectric ferroelectrics commonly used as transducers, can experience depoling and consequent loss of efficiency at very high power and temperature levels.

Conclusion

The piezoelectric effect has been briefly reviewed from the standpoints of origin, traditional uses, connection with associated effects, and relation to crystal symmetry. Sample material coefficients are given, with ample references to the pertinent literature. Future prospects for use of the piezoeffect appear bright because it mediates directly between the elastic and electronic variables in the rapidly growing area of MEMS devices and technology.

References

- [01] W G Cady, Piezoelectricity, McGraw Hill, New York, 1946; Dover, New York, 1964
- [02] E A Gerber and A Ballato, eds., Precision Frequency Control, Vol. 1 and 2, Academic Press, New York and Orlando, 1985.
- [03] J G Smits, S I Dalke, and T K Cooney, "The constituent equations of piezoelectric bimorphs," Sensors and Actuators, Vol. A28, 1991, pp. 41 - 61.
- [04] J G Smits and W S Choi, "The constituent equations of heterogeneous piezoelectric bimorphs," IEEE Trans. Ultrason. Ferroelec. Freq. Contr., Vol. 38, No. 3, May 1991, pp. 256-270.
- [05] A Ballato and J G Smits, "Network representation for piezoelectric bimorphs," IEEE Trans. Ultrason. Ferro. Freq. Contr., Vol. 38, No. 6, November 1991, pp. 595-602.
- [06] Y K Yong, J T Stewart, and A Ballato, "A laminated plate theory for high frequency, piezoelectric thin-film resonators," J. Appl. Phys., Vol. 74, No. 5, 1 September 1993, pp. 3028-3046.
- [07] US Congress, Office of Technology Assessment, "Miniaturization Technologies," OTA-TCT-514 (Washington, DC: US Government Printing Office, November 1991), 48pp.
- [08] "IRE Standards on Piezoelectric Crystals, 1949," Proc. IRE, Vol. 37, No. 12, December 1949, pp. 1378 - 1395.
- [09] "IEEE Standard on Piezoelectricity," IEEE Standard 176-1978, IEEE, New York, 55pp.
- [10] B A Auld, Acoustic Fields and Waves In Solids, 2nd edition, Vol. I and II, R. E. Krieger Pub. Co., Malabar, FL, 1990.
- [11] A Ballato, "Polarization matrices of lithium niobate," Technical Report SLCET-TR-89-1, U. S. Army Laboratory Command, Fort Monmouth, NJ, April 1989, 30 pp.
- [12] J F Nye, Physical Properties of Crystals, Clarendon Press, Oxford, 1957; Oxford University Press, 1985.

- [13] W P Mason, Crystal Physics of Interaction Processes, Academic Press. New York and London, 1966.
- [14] R E Newnham, "Tunable transducers: nonlinear phenomena in electroceramics," National Institute of Standards and Technology Special Publication 804, Chemistry of Electronic Ceramic Materials, Proceedings of the International Conference held in Jackson WY, August 17-22, 1990. Issued January 1991.
- [15] V Sundar and R E Newnham, "Electrostriction and polarization," *Ferroelectrics*, Vol. 135, 1992, pp. 431-446.
- [16] A Ballato, "Doubly rotated thickness mode plate vibrators," in Physical Acoustics: Principles and Methods, (W P Mason and R N Thurston, eds.), Vol. 13, Chap. 5. Academic Press, New York, 1977, pp. 115-181.
- [17] J F Rosenbaum, Bulk Acoustic Wave Theory and Devices, Artech House, Boston and London, 1988.
- [18] "IRE Standards on Piezoelectric Crystals: Determination of the Elastic, Piezoelectric, and Dielectric Constants - The Electromechanical Coupling Factor, 1958," *Proc. IRE*, Vol. 46, No. 4, April 1958, pp. 764-778. IEEE Standard 178.
- [19] Landolt-Börnstein, Numerical Data and Functional Relationships in Science and Technology, New Series, Group III: Crystal and Solid State Physics, Volumes III/1, 1966; III/2, 1969; III/3, 1969; III/9, 1974; III/11, 1979; III/16a, 1981; III/16b, 1982; and III/17a, 1982. Springer-Verlag, Berlin, New York.
- [20] J G Gualtieri, J A Kosinski, and A Ballato, "Piezoelectric materials for acoustic wave applications," *IEEE Trans. Ultrason., Ferroelec., and Freq. Control*, Vol. 41, No. 1, January 1994, pp. 53-59.
- [21] M J Buerger, Elementary Crystallography, John Wiley and Sons, New York, 1956.
- [22] S Bhagavantam, Crystal Symmetry and Physical Properties, Academic Press, London and New York, 1966.
- [23] M J P Musgrave, Crystal Acoustics, Holden-Day, San Francisco, 1970.
- [24] H J Juretschke, Crystal Physics, W A Benjamin, Reading, MA, 1974.

- [25] T Ikeda, Fundamentals of Piezoelectricity, Oxford University Press, 1990.
- [26] A Ballato and T J Lukaszek, "Shallow bulk acoustic wave progress and prospects," IEEE Trans. Microwave Theory Tech., Vol. MTT-27, No. 12, December 1979, pp. 1004-1012.
- [27] B Jaffe, W R Cook, Jr, and H Jaffe, Piezoelectric Ceramics, Academic Press, New York, 1971.
- [28] "IEEE Standard Definitions of Primary Ferroelectric Terms," ANSI/IEEE Standard 180-1986, IEEE, New York, 21pp.
- [29] J J Kyame, "Conductivity and viscosity effects on wave propagation in piezoelectric crystals," J. Acoust. Soc. Amer., Vol. 26, November 1954, pp. 990-993.
- [30] A R Hutson and D L White, "Elastic wave propagation in piezoelectric semiconductors," J. Appl. Phys., Vol. 33, January 1962, pp. 40-47.
- [31] A Ballato and C D Bosco, "Acoustic waves in cubic crystals: networks for semiconducting vibrators, and applications to gallium arsenide," Technical Report DELET-TR-79-9, April 1979, 45 pp., US Army Electronics Technology & Devices Laboratory, Fort Monmouth, NJ 07703.
- [32] B Schwarzschild, "Half-filled Landau level yields intriguing data and theory," Physics Today, Vol. 46, No. 7, July 1993, pp.17-20.
- [33] B I Halperin, P A Lee, and N Read, "Theory of the half-filled Landau level," Phys. Rev. B, Vol. 47, No. 12, 15 March 1993, pp. 7312-7343.
- [34] R L Willett, R R Ruel, M A Paalanen, K W West, and L N Pfeiffer, "Enhanced finite-wave-vector conductivity at multiple even-denominator filling factors in two-dimensional electron systems," Phys. Rev. B, Vol. 47, No. 12, 15 March 1993, pp. 7344-7347.
- [35] R L Willett, M A Paalanen, R R Ruel, K W West, L N Pfeiffer, and D J Bishop, "Anomalous sound propagation at $\nu = 1/2$ in a 2D electron gas: observation of a spontaneously broken translational symmetry?," Phys. Rev. Lett., Vol. 65, No. 1, 2 July 1990, pp. 112-115.
- [36] A Wixforth, J P Kotthaus, and G Weimann, "Quantum oscillations in the surface-acoustic-wave attenuation caused by a two-dimensional electron system," Phys. Rev. Lett., Vol. 56, No. 19, 12 May 1986, pp. 2104-2106.

- [37] R C Marshall, J W Faust, Jr, and C E Ryan, eds., Silicon Carbide -1973, Univ. of South Carolina Press, Columbia. SC, 1974.
- [38] S Karmann, R Helbig, and R A Stein, "Piezoelectric properties and elastic constants of 4H and 6H SiC at temperatures 4 - 320 K," J. Appl. Phys., Vol. 66, No. 8, 15 October 1989, pp. 3922-3924.
- [39] M E Sherwin and T J Drummond, "Predicted elastic constants and critical layer thicknesses for cubic phase AlN; GaN, and InN on β -SiC," J. Appl. Phys., Vol. 69, No. 12, 15 June 1991, pp. 8423-8425.
- [40] T R Watkins, D J Green, and E R Ryba, "Determination of Young's modulus in chemically vapor-deposited SiC coatings," J. Am. Ceram. Soc., Vol. 76, No. 8, August 1993, pp. 1965-1968.
- [41] Based on material provided by Dr. Max N Yoder, Office of Naval Research, Arlington, VA 22217.
- [42] L S Ramsdell and J A Kohn, "Developments in Silicon Carbide Research," Acta Crystallographica, Vol. 5, Part 2, March 1952, pp. 215-224.
- [43] A Addamiano, "Speculations on the origins of the polytypism of SiC," in R C Marshall, J W Faust, Jr, and C E Ryan, eds., Silicon Carbide - 1973, Univ. of South Carolina Press, Columbia, SC, 1974, pp.179-205.
- [44] L L Hench and J K West, Principles of Electronic Ceramics, Wiley-Interscience, New York, 1990.

TABLE 1. REPRESENTATIVE VALUES OF PIEZOCOUPLING FACTORS

Material Type	Crystal Class	Substance	Orientation	Coupling Factor (%)
Dielectrics	3m	lithium niobate (LiNbO ₃)	X-cut 36° rotated Y-cut	k ₁₅ = 68.9 k ₂₂ = 48.7
	32	quartz	AT-cut BT-cut	k ¹ ₂₆ = 8.8 k ¹ ₂₆ = 5.0
Ceramics (solid solutions)	∞mm	lead titanate zirconate	Z-cut	k ₃₃ = 30 to 60
Piezoelectric polymers	mm2	PVDF	Z-normal sheet	k ₃₁ = 16
Binary semi-conductors	4bar 3m	gallium arsenide	(110) cut (111) cut	k ¹ ₂₆ = 6.1 k ¹ ₁₁ = 4.3
	6mm	α- silicon carbide	X- or Y-cut Z-cut	k ₁₅ = 2.5 k ₃₃ = 3.5
	4bar 3m	β- silicon carbide	(110) cut (111) cut	k ¹ ₂₆ = ?* k ¹ ₁₁ = ?* *Estimated ≈ α form

TABLE 2. THE SEVEN CRYSTAL SYSTEMS AND THIRTY-TWO POINT GROUPS ⁴⁴

CRYSTAL SYSTEM	CENTRIC POINT GROUPS		ACENTRIC POINT GROUPS			OPTIC AXES		
			POLAR _p		NONPOLAR _p			
TRICLINIC _I	$\bar{1}$ _h		1 _c		NONE		B I A X I A L	
MONOCLINIC _{II}	2/m _h		2 _c	m _o	NONE			
ORTHORHOMBIC _{III}	mmm _h		mm2 _o		222 _c			
TETRAGONAL _{IV}	4/m _a	4/m mm _{b h}	4 _a	4mm _b	$\bar{4}$ _a	$\bar{4}2m$ _b	422 _b	U N I A X I A L
TRIGONAL _V	$\bar{3}$ _a	$\bar{3}m$ _{b h}	3 _a	3m _b	32 _b			
HEXAGONAL _{VI}	6/m _a	6/m mm _{b h}	6 _a	6mm _b	$\bar{6}$ _a	$\bar{6}m2$ _b	622 _b	
CUBIC _{VII}	m3 _a	m3m _{b h}	NONE		23 _a	$\bar{4}3m$ _b	432 _{b p}	ISO-TROPIC
	11 GROUPS		10 GROUPS		11 GROUPS			

TABLE 3	POINT GROUP {Triclinic, 1,1}				
e_{11}	e_{12}	e_{13}	e_{14}	e_{15}	e_{16}
e_{21}	e_{22}	e_{23}	e_{24}	e_{25}	e_{26}
e_{31}	e_{32}	e_{33}	e_{34}	e_{35}	e_{36}
TABLE 4	POINT GROUP 2 [IEEE axial convention] {Monoclinic, II, 3}				
0	0	0	e_{14}	0	e_{16}
e_{21}	e_{22}	e_{23}	0	e_{25}	0
0	0	0	e_{34}	0	e_{36}
TABLE 5	POINT GROUP m [IEEE axial convention] {Monoclinic, II, 4}				
e_{11}	e_{12}	e_{13}	0	e_{15}	0
0	0	0	e_{24}	0	e_{26}
e_{31}	e_{32}	e_{33}	0	e_{35}	0
TABLE 6	POINT GROUP 222 {Orthorhombic, III, 6}				
0	0	0	e_{14}	0	0
0	0	0	0	e_{25}	0
0	0	0	0	0	e_{36}
TABLE 7	POINT GROUP mm2 {Orthorhombic, III, 7}				
0	0	0	0	e_{15}	0
0	0	0	e_{24}	0	0
e_{31}	e_{32}	e_{33}	0	0	0
TABLE 8	POINT GROUPS 4 {Tetragonal, IVa, 9} AND 6 {Hexagonal, VIa, 21}				
0	0	0	e_{14}	e_{15}	0
0	0	0	e_{15}	$-e_{14}$	0
e_{31}	e_{31}	e_{33}	0	0	0
TABLE 9	POINT GROUP 4bar {Tetragonal, IVa, 10}				
0	0	0	e_{14}	e_{15}	0
0	0	0	$-e_{15}$	e_{14}	0
e_{31}	$-e_{31}$	0	0	0	e_{36}

TABLE 10	POINT GROUPS 422 {Tetragonal, IVb, 12} AND 622 {Hexagonal, VIb, 24}				
0	0	0	e_{14}	0	0
0	0	0	0	$-e_{14}$	0
0	0	0	0	0	0
TABLE 11	POINT GROUP 4mm {Tetragonal, IVb, 13} AND 6mm {Hexagonal, VIb, 25}; TRANSVERSE ISOTROPY				
0	0	0	0	e_{15}	0
0	0	0	e_{15}	0	0
e_{31}	e_{31}	e_{33}	0	0	0
TABLE 12	POINT GROUP $4\bar{2}m$, {Tetragonal, IVb, 14}				
0	0	0	e_{14}	0	0
0	0	0	0	e_{14}	0
0	0	0	0	0	e_{36}
TABLE 13	POINT GROUP 3 {Trigonal, Va, 16}				
e_{11}	$-e_{11}$	0	e_{14}	e_{15}	$-e_{22}$
$-e_{22}$	e_{22}	0	e_{15}	$-e_{14}$	$-e_{11}$
e_{31}	e_{31}	e_{33}	0	0	0
TABLE 14	POINT GROUP 32 {Trigonal, Vb, 18}				
e_{11}	$-e_{11}$	0	e_{14}	0	0
0	0	0	0	$-e_{14}$	$-e_{11}$
0	0	0	0	0	0
TABLE 15	POINT GROUP 3m (Trigonal, Vb, 19)				
0	0	0	0	e_{15}	$-e_{22}$
$-e_{22}$	e_{22}	0	e_{15}	0	0
e_{31}	e_{31}	e_{33}	0	0	0
TABLE 16	POINT GROUP $6\bar{2}$ {Hexagonal, VIa, 22}				
e_{11}	$-e_{11}$	0	0	0	$-e_{22}$
$-e_{22}$	e_{22}	0	0	0	$-e_{11}$
0	0	0	0	0	0

TABLE 17	POINT GROUP 6bar m2 {Hexagonal, VIb, 26}					
e_{11}	$-e_{11}$	0	0	0	0	0
0	0	0	0	0	0	$-e_{11}$
0	0	0	0	0	0	0

TABLE 18	POINT GROUPS 23 {Cubic, VIIa, 28} AND 4bar 3m {Cubic, VIIb, 31}					
0	0	0	e_{14}	0	0	0
0	0	0	0	e_{14}	0	0
0	0	0	0	0	0	e_{14}

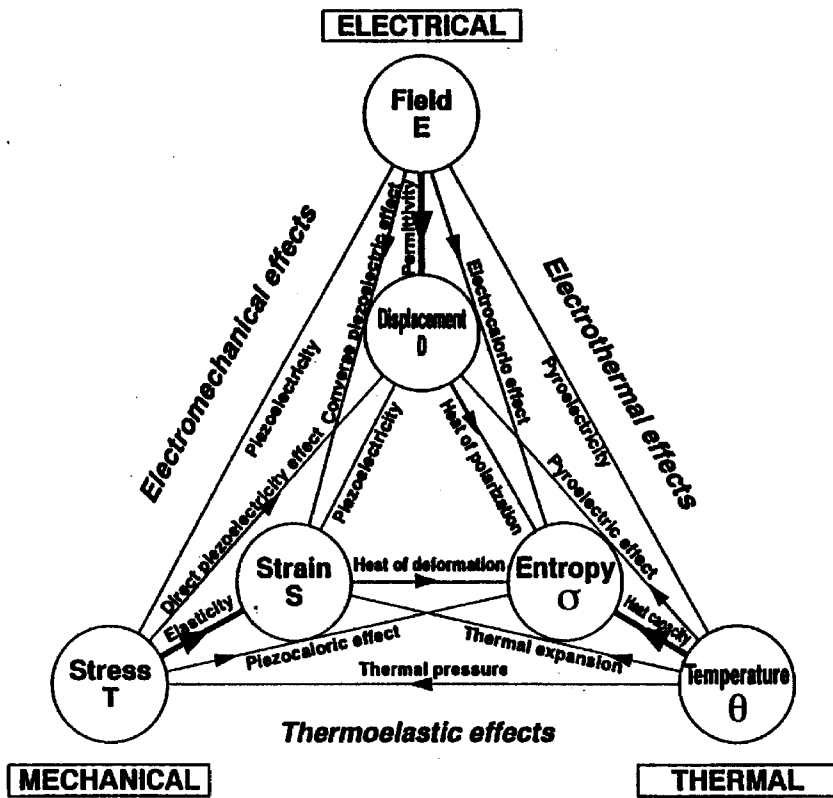


Figure 1. Couplings between the electrical, mechanical, and thermal fields.

3-5	N	P	As	Sb
B	c	c		
Al	h	c	c	c
Ga	h	c	c	c
In		c	c	c

2-6	O	S	Se	Te
Be	h			
Zn	h	(α -h) (β -c)	c	c
Cd		h	h	c

1-7	Br	Cl	I
Cu	c	c	c
Ag			h

4-4	C
Si	(α -h) (β -c)

**h = hexagonal, 6mm
(wurtzite)**

**c = cubic, $\bar{4}3m$
(sphalerite; zinc blende)**

Figure 2. Piezoelectric binary semiconductors

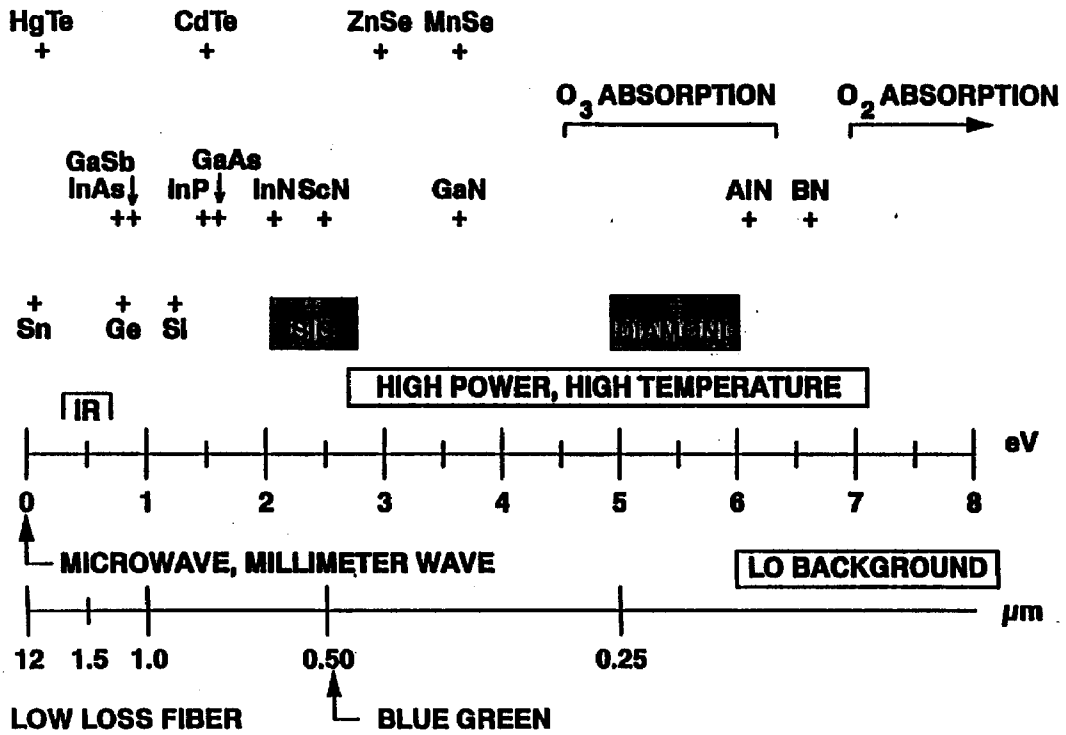


Figure 3. Bandgap of important semiconductors⁴¹