AN1410
Application Note

Configuring and Applying the MC74HC4046A Phase-Locked Loop

A versatile device for 0.1 to 16MHz frequency synchronization

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The MC74HC4046A (hereafter designated HC4046A) phase–locked loop contains three phase comparators, a voltage–controlled oscillator (VCO) and an output amplifier. The user of this document should have a copy of the HC4046A data sheet in Motorola Data Book DL129 available for details of device operation and operating specifications. The user should also be aware that the following information is useful for approximating a design **but**, because of process, layout and other variables, there can be substantial deviation between theory and actual results. Therefore, **it is highly recommended that prototypes be built and checked before committing a design to production**.

Typical applications for the HC4046A usually involve a configuration such as shown in Figure 1.

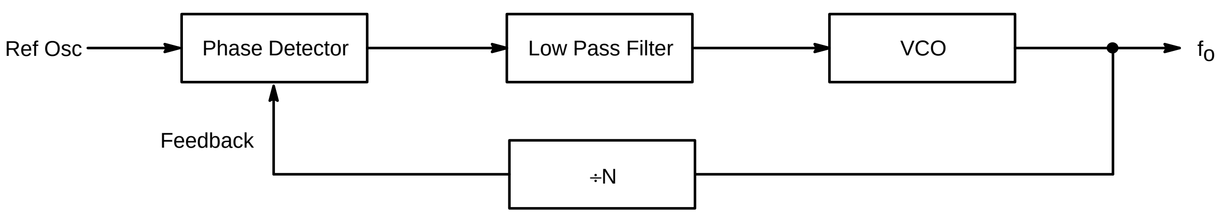

Figure 1. Typical Phase–Locked Loop

VCO/OUTPUT FREQUENCY

The output frequency, F_o, is calculated as a function of the Ref Osc input and the ÷N feedback counter:

$$F_o = \text{Ref Osc} * N \qquad (1)$$

The ability of the loop to emulate the above formula makes it ideal for multiplying an input frequency by any number up to the maximum of the VCO. The HC4046A VCO frequency is controlled by the equation:

$$\text{VCO freq} = f(I * C) \qquad (2)$$

where I is controlled by the external resistors R_1 and R_2 and C by external capacitor C_{ext} .

Frequency of oscillation is calculated by starting with the familiar equation:

$$I = c\frac{dV}{dt} \qquad (3)$$

and reworking it to obtain a formula that incorporates all the detail to fit the HC4046A. First, the charge time of the device for half–cycle time is obtained as follows:

$$dt = dV\frac{C}{I} \quad \text{and} \quad F_o = \frac{1}{2dt}$$

$$\text{or,} \quad F_o = \frac{\frac{1}{2CdV}}{I} = \frac{I}{2CdV} \qquad (4)$$

where I and dV must be obtained for the HC4046A.

There are two components that comprise the I charge for the HC4046A VCO, I_1 and I_2. I_1 is the current that sets the frequency associated with the VCO input and is a function of R_1, VCO_{in}, and an internal current mirror that is ratioed at 120/5 ≈ 24, resulting in the equation:

$$I_1 = \frac{VCO_{in}}{R_1}\left(\frac{120}{5}\right) \qquad (5)$$

I_2 is set by R_2 and adds a constant current to limit the F_o min of the VCO and is a function of V_{dd}, R_2, and an internal current mirror of ratio 23/5, resulting in the equation:

$$I_2 = \left(\frac{2V_{dd}}{3R_2}\right)\left(\frac{23}{5}\right) \qquad (6)$$

The dV of Equation (4) is determined by design to be ≈ 1/3 V_{dd}. Substituting this and $I = I_1 + I_2$ into Equation (4) results in:

$$F_o = \frac{\frac{VCO_{in}}{R_1}\left(\frac{120}{5}\right) + \left(\frac{2V_{dd}}{3R_2}\right)\left(\frac{23}{5}\right)}{2C_{ext}\frac{V_{dd}}{3}}$$

$$= \frac{\frac{VCO_{in}}{R_1}(24) + \left(\frac{2V_{dd}}{3R_2}\right)(4.6)}{2C_{ext}\frac{V_{dd}}{3}}$$

$$= \frac{\frac{3VCO_{in}}{R_1}(24) + \frac{2V_{dd}}{R_2}(4.6)}{2C_{ext}\ V_{dd}} \qquad (7)$$

It was found by experiment that when the C_{ext} potential reaches threshold (at $V_{dd}/3$), the inversion of the charging voltage of C_{ext} is forced below ground due to charge coupling. Therefore, the dV is not just $V_{dd}/3$ as expected and the charging time must start at a point below ground which affects t and thus, F_O. An undershoot voltage must be added to the equation for better accuracy in calculating t and F_O. This modifies Equation (7) as follows:

$$F_O = \frac{\frac{3VCO_{in}}{R_1}(24) + \frac{2V_{dd}}{R_2}(4.6)}{2C_{ext}\,(V_{dd} + 3 * \text{undershoot})}$$

$$= \frac{\frac{3VCO_{in}(I_{constant\ ratio})}{R_1} + \frac{9.2(V_{dd})}{R_2}}{2C_{ext}\,(V_{dd} + 3 * \text{undershoot})} \qquad (8)$$

Equation (8) now contains all the factors to calculate an F_O for the HC4046A VCO.

It was determined by experiment that the undershoot of the charging waveform is a function of C_{ext} and an on–chip parasitic diode that clamps it at a maximum of –0.7V. The size of the C_{ext} capacitor limits the voltage and was found to be near zero volts for $C_{stray} \approx 17pF \le C_{ext} \le 30pF$; the voltage increases at 6 mV/pF for a $30pF \le C_{ext} \le 150pF$ range of C_{ext}. The on–chip diode then takes over and limits the voltage to –0.7V.

It was also found that the $I_{constant\ ratio}$ is a function of R_1 and increases as R_1 becomes larger. The change is attributed to saturation of the current mirror at lower value resistances, and to voltage divider problems at higher value resistances combined with the resistance of the small FET in the current mirror. Experimental data shows that $I_{constant\ ratio}$ follows Table 1 somewhat. The ratio goes to 25 somewhere between 9.1KΩ and 51KΩ, and for those limits, 25 should give reasonable results. In addition, these numbers seem to hold for a range of V_{dd} of $3.0V \le V_{dd} \le 6V$.

Table 1. $I_{constant\ ratio}$ versus R_1

R_1 (KΩ)	$I_{constant\ ratio}$
3.0	13.5
5.1	17.5
9.1	21.5
12	23.0
15	24.0
30	26.5
40	27.0
51	28.5
110	29.0
300	31.0

The VCO calculation [Equation (8)] becomes a bit more accurate by adjusting the VCO_{in} and $I_{constant\ ratio}$. For example, with R_1 = 300K, $R_2 = \infty$, C_{ext} = 0.1µF, VCO_{in} = 1.0V, V_{dd} = 4.5V, and $I_{constant\ ratio}$ = 31, Equation (8) yields:

$$F_O = \frac{\frac{(3)(1)(31)}{300K}}{2(0.1 * 10^{-6})(4.5 + 2.1)}$$

$$= 235\text{Hz}$$

For comparison, from Chart 14D in the HC4046A data sheet, the F_O based on measurements is approximately 270 Hz. Thus, the calculated and measured values are not too far apart taking into consideration such variables as process variation, temperature, and breadboard inaccuracies. The C_{stray} of a PCB layout will affect results if the C_{ext} is not $\gg C_{stray}$. So for $C_{ext} \le 1000pF$, adding C_{stray} to the C_{ext} fixed capacitance will result in better accuracy.

The gain of a VCO is calculated by knowing f_{max} at VCO_{in} max and f_{min} at VCO_{in}min and calculating the following equation:

$$\text{VCO gain} = \frac{f_{max} - f_{min}}{VCO_{in}\,max - VCO_{in}\,min} \qquad (9)$$

$$= \Delta freq/volt$$

The gain of the VCO is needed to calculate a suitable loop filter for a PLL system.

F_O is determined by VCO_{in} and is clamped as a function of a % of V_{dd}. The clamp voltage generally follows the slope of 4%/V for V_{dd} changes from $3.5V \le V_{dd} \le 6V$, starting at 56% at V_{dd} = 3.5V and going to 66% at V_{dd} = 6V. Knowing this limit point allows picking a VCO_{in} max point a few hundred mV below it and keeps F_O in the linear range of operation. It also best to pick a VCO_{in} min point at a level of a few hundred mV above 0V for the same reason given above.

As an example, for a C_{ext} =1100pF, R_1 = 9.1K, $R_2 = \infty$, V_{dd} =5.0V, and VCO_{in} min = 0.25V, VCO_{in} max can be determined and a gain calculated as follows. VCO_{in} limit = (4%/V)(1.5V) + 56% = (62%)(V_{dd}) = 3.1V. So, for sake of linearity, choose VCO_{in} = 2.5V. Using Equation (8), VCO_{in} min and VCO_{in} max can be used to calculate F_O min and F_O max as follows:

$$F_O\ min = \frac{\frac{(3)(0.25)(21.5)}{9.1K}}{2(1100 * 10^{-12})(5 + 2.1)} = 113.4\text{KHz}$$

$$F_O\ max = \frac{\frac{(3)(2.5)(21.5)}{9.1K}}{2(1100 * 10^{-12})(5 + 2.1)} = 1.3\text{MHz}$$

Then, using Equation (9), the VCO gain is:

$$\text{VCO gain} = \frac{1.3 * 10^6 – 0.11 * 10^6}{2.5–0.25} = 528.9\text{KHz/V}$$

This gain factor will be known as K_{vco} in the loop filter equations.

R_2 is used in applications where a minimum output frequency is desired when VCO_{in} is 0V. It is calculated at VCO_{in} = 0V causing Equation (8) to become:

$$F_O = \frac{9.2\ (V_{dd})}{2C\ (R_2)\ (V_{dd} + 3 * \text{undershoot})}$$

The additional I_2 current is a constant that adds to total charge current for C_{ext} and increases the VCO_{in} versus F_O curve by a theoretical constant amount. In reality, the amount of increase actually decreases at a slight rate as VCO_{in} increases. The decrease is slight and the use of Equation (8) will give adequate accuracy for most applications.

The F_{max} of the HC4046A VCO was determined to be about 16MHz. Beyond 16MHz, the output logic swing tends to reduce and is therefore somewhat useless for driving a CMOS input. The VCO will operate at ≈ 28MHz but the output has a $V_{OL} \approx$ 2.0V and a $V_{OH} \approx$ 4.5V at V_{dd} = 5.0V.

The following table was generated to make calculation of R_1 and C_{ext} a function of F_o with V_{dd} = 5V, VCO_{in} = 1V, and room temperature. Use of the table allows a rough estimate of $(R_1)(C_{ext})$ for a given F_o. The final values can be adjusted by use of Equation (8), Table 1 for $I_{constant\ ratio}$, rules for undershoot voltage, V_{dd} variations, and VCO_{in} variations. The example below shows a typical calculation.

Table 2. $(R_1)(C_{ext})$ versus F_o

R_1 (Ω)	C_{ext} (pF)	$(R_1)(C_{ext})$
$3.0K \le R_1 \le 9.0K$	$0 \le C_{ext} \le 30$ $30 \le C_{ext} \le 150$ $150 \le C_{ext} \le \infty$	$5.40/F_o$ $4.15/F_o$ $3.80/F_o$
$9.1K \le R_1 \le 50K$	$0 \le C_{ext} \le 30$ $30 \le C_{ext} \le 150$ $150 \le C_{ext} \le \infty$	$7.50/F_o$ $5.77/F_o$ $5.28/F_o$
$50K \le R_1 \le 900K$	$0 \le C_{ext} \le 30$ $30 \le C_{ext} \le 150$ $150 \le C_{ext} \le \infty$	$9.00/F_o$ $6.92/F_o$ $6.34/F_o$

Assume a desired value of F_o of 1MHz. From Table 2, choose an R_1 range of $9.1K \le R_1 \le 50K$ and a C_{ext} range of > 150pF; this condition leads to $(R_1)(C_{ext}) = 5.28/F_o$. Thus,

$$(R_1)\ (C_{ext}) = \frac{5.28}{1 * 10^6} = 5.28 * 10^{-6}$$

Now choose a C_{ext} of 200pF. Then, from above result,

$$R_1 = \frac{5.28 * 10^{-6}}{200 * 10^{-12}} = 26K$$

This appears reasonable and there are standard values for C_{ext} = 200pF and R_1 = 27K. Using these values, Equation (8) can be adjusted according to the desired F_o min, F_o max, and F_o center.

LOW PASS FILTER DESIGN

The design of low pass filters is well known and the intent here is to simply show some typical examples. Reference should be made to the HC4046A Data Sheet and to Motorola Application Note AN535/D — “Phase–Locked Loop Fundamentals” (available through Motorola Literature Distribution).

Some simple types of low pass filters are shown in Figure 2 and Figure 3.

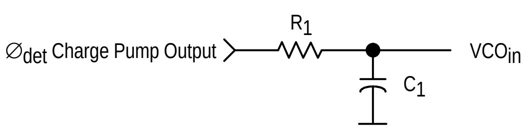

Figure 2. Simple Low Pass Filter A

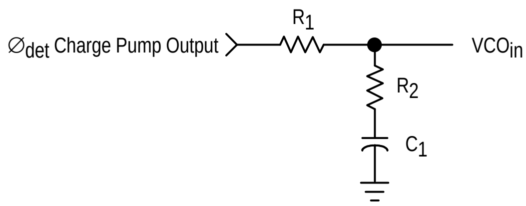

Figure 3. Simple Low Pass Filter B

The equations for calculating loop natural frequency (w_n) and damping factor (d) are as follows:

For Filter A (Figure 2):

$$w_n = \sqrt{\frac{K_\phi K_{VCO}}{NC_1R_1}}$$

$$d = \frac{0.5w_n}{K_\phi K_{VCO}}$$

where $K_\varnothing$ = phase detector gain, K_{VCO} = VCO gain, and N = divide counter.

For Filter B (Figure 3):

$$w_n = \sqrt{\frac{K_\phi K_{VCO}}{NC_1(R_1 + R_2)}}$$

$$d = 0.5w_n(R_2C_1 + \frac{N}{K_\phi K_{VCO}}) \qquad (10)$$

Figure 4 shows an active filter using an op amp from Application Note AN535/D.

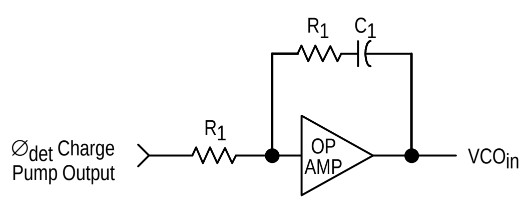

Figure 4. Op Amp Filter

For Figure 4, the equations become:

$$w_n = \sqrt{\frac{K_\phi K_{VCO}}{NC_1R_1}} \qquad (11)$$

$$d = \frac{K_\phi K_{VCO}R_2}{2w_nNR_1} \qquad (12)$$

$$= \frac{w_nC_1R_2}{2}\text{, where Op Amp gain is large}$$

From the above equations, it is possible to design a suitable filter to meet the needs of many PLL applications. The inclusion of R_2 in the equations for Figure 3 and Figure 4 permits the capability to change w_n and d separately while Figure 2 equations do not. Normally, a design is easier if w_n and d can be chosen independently. Both factors affect the loop acquisition time and stability. A good starting value for d is 0.707 and $F_{ref}/10$ for w_n.

Manipulation of the equations allows calculation of R_1, R_2, and C_1 from the other measured, calculated, or picked parameters. For example,

$$R_1 + R_2 = \frac{K_{ø}K_{VCO}}{NC_1{w_n}^2} \qquad (13)$$

$$R_2 = \frac{2d}{C_1 w_n} - \frac{N}{C_1(K_{ø}K_{VCO})} \qquad (14)$$

$$C_1 = \frac{K_{ø}K_{VCO}}{N{w_n}^2(R_1 + R_2)}, \text{ or alternatively,}$$

$$C_1 = \frac{2d}{R_2 w_n} - \frac{N}{R_2(K_{ø}K_{VCO})}$$

Usually, C_1, w_n, and d are picked and the remaining parameters calculated.

DESIGN EXAMPLE

The goal is to design a phase–locked loop that has an F_{ref} of 100KHz, an output F_o of 1MHz center frequency, and the ability to move from 200KHz to 2MHz in 100KHz steps.

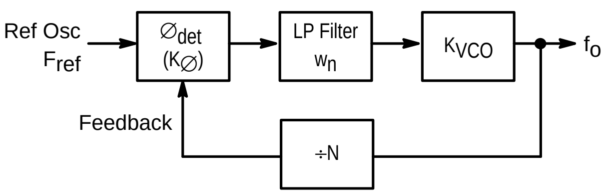

Figure 5. Parametized PLL

To determine N, use equation (1) for F_o min = 200KHz, and F_o max = 2MHz resulting in the following:

N min = 200/100 = 2, and

N max = 2000/100 = 20

The results so far indicate the following starting parameters:

A. A VCO with a 10:1 range is required

B. $w_n = F_{ref}/10 = 10KHz$

C. d = 0.707

D. $R_2 = \infty$

E. $V_{dd} = 5.0V$

The F_o center frequency ≈

$$\frac{F_{max} + F_{min}}{2} = \frac{2.0 + 0.2}{2} = 1.1MHz$$

Recalling that the clamp voltage % at V_{dd} = 5V is about 62, then F_{max} VCO_{in} limit = (0.62)(5) = 3.1V, but as described earlier, this needs to be reduced by a factor to bring it into linearity (≈ 350mV) so the final F_{max} VCO_{in} limit = 2.75V.

For the F_{min} VCO_{in} limit pick 0.25V. This results in a center frequency VCO_{in} of:

$$\text{Center freq } VCO_{in} = \frac{2.75 - 0.25}{2} = 1.25V$$

From Table 2, for picked values of $9.1K \le R_1 \le 50K$ and $30 \le C_{ext} \le 150$, obtain an estimate for $(R_1)(C_{ext})$ of $5.77/F_o$. Thus, at the F_o center frequency,

$$(R_1)(C_{ext}) = \frac{5.77}{1.1 * 10^6} = 5.245 * 10^{-6}$$

Now, a reasonable starting point is established for setting the values of the loop filter and the VCO range. Choosing R_1 = 9.1K, C_{ext} becomes

$$C_{ext} = \frac{5.245 * 10^{-6}}{9.1K} = 576pF \text{ WHOOPS!}$$

This value, 576pF, is outside of the original picked range for C_{ext}; therefore, we need to go back and pick a larger value of R_1, e.g., 42K should be sufficient. Then C_{ext} becomes

$$C_{ext} = \frac{5.245 * 10^{-6}}{42K} = 125pF$$

and now both R_1 and C_{ext} are within selected ranges.

Now calculate F_{max} and F_{min} using Equation (8) with R_1 = 42kΩ, $R_2 = \infty$, V_{dd} = 5.0V, $I_{constant\,ratio}$ = 27 (from Table 1. and R_1 = 42kΩ), $V_{undershoot}$ = 0.57V (calculated from 6pF/mV (125pF–30pF) = 0.57V), VCO_{in} min = 0.25V, and VCO_{in} max = 2.75V:

$$F_o \min = \frac{\frac{(3)(0.25)(27)}{42K} + \cancelto{0}{\frac{(9.2)(5.0)}{\infty}}}{(2)(125 * 10^{-12}f)\ [5.0V + 3(0.57V)]}$$

$$= \frac{20.25}{70.455 * 10^{-6}} = 287.4KHz$$

$$F_o \max \frac{\frac{(3)(2.75)(27)}{42K} + \cancelto{0}{\frac{(9.2)(5.0)}{\infty}}}{(2)(125 * 10^{-12}f)\ [5.0V + 3(0.57V)]}$$

$$= \frac{222.75}{70.455 * 10^{-6}} = 3.16MHz$$

F_{max} is > the required 2.0MHz, but the F_{min} is not low enough for required application. It is necessary to adjust either C_{ext} or R_1 to achieve required specification of 0.2 to 2.0MHz F_o. Since R_1 = 42kΩ is a standard resistor value, try adjusting C_{ext} to a higher value, such as 175pF. Because C_{ext} is now > 150pF, the $V_{undershoot}$ must be adjusted to 0.7V, as per earlier explanation:

So,

$$F_O\,\min = \frac{\frac{(3)(0.25)(27)}{42K} + \cancelto{0}{\frac{(9.2)(5.0)}{\infty}}}{(2)(175 * 10^{-12}f)\ [5.0V + 3(0.7V)]}$$

$$= \frac{20.25}{104.37 * 10^{-6}} = 194.02KHz$$

and

$$F_O\,\max \frac{\frac{(3)(2.75)(27)}{42K} + \cancelto{0}{\frac{(9.2)(5.0)}{\infty}}}{(2)(175 * 10^{-12}f)\ [5.0V + 3(0.7V)]}$$

$$= \frac{222.75}{104.37 * 10^{-6}} = 2.13MHz$$

These values are adequate for the specified application.

The next item to determine is the VCO gain factor, K_{VCO}, using Equation (9):

$$K_{VCO} = \frac{f_{max} - f_{min}}{VCO_{in}\max - VCO_{in}\min}$$

$$K_{VCO} = \frac{2.13 * 10^6 - 0.194 * 10^6}{2.75V - 0.25V} = 774.4KHz/V$$

or in radians

$$= (2\pi)\ (774.4 * 10^3) = 4.86 * 10^6 Rad/sec/V$$

The final values used for the desired frequency range are R_1 = 42kΩ, C_{ext} = 175pF, $R_2 = \infty$, VCO_{in} max = 2.75V, and VCO_{in} min = 0.25V.

The next step is to determine the loop filter. Choosing a filter like the one in Figure 3, calculate the component as follows:

$$K_ø = \frac{V_{dd}}{4\pi} = \frac{5.0}{4\pi} = 0.4V/rad$$

$$w_n = \frac{100KHz}{10} = 10KHz * 2\pi = 62.83 * 10^3 rad/sec$$

d = 0.707 (for starters), and

N = 2 to 20

where

$K_\varnothing$ = phase detector gain
V_{dd} = output swing

Choose C_1 to be 0.01µF, N = 10 for approximate mid–range F_O, and calculate R_1 and R_2 using Equations (13) and (14):

$$R_1 + R_2 = \frac{K_ø K_{VCO}}{NC_1 {w_n}^2} = \frac{(0.4)(4.86 * 10^6)}{(10)(0.01 * 10^{-6})(62.83 * 10^3)^2}$$

$$= \frac{1.944 * 10^6}{394.76} = 4924.5\Omega$$

$$R_2 = \frac{2d}{C_1 w_n} - \frac{N}{C_1(K_ø K_{VCO})}$$

$$= \frac{(2)(0.707)}{(0.01 * 10^{-6})\ (62830)} - \frac{10}{(0.01 * 10^{-6})(0.4)(4.86 * 10^6)}$$

$$= 2250.52 – 514.4 = 1736\Omega$$

Then, R_1 = 4924.5 – 1736 = 3188.5Ω.

Since N is changeable, it is a good idea to check min and max on w_n and d. For more information on why, see Motorola Application Note AN535/D or the MC4044 Data Sheet in the MECL Data Book DL122/D. The following examples show sample calculations for N = 2 and 20.

For N = 20, use Equation (10) to calculate w_n and d:

$$w_n\min = \sqrt{\frac{K_ø K_{VCO}}{NC_1(R_1 + R_2)}}$$

$$= \sqrt{\frac{(0.4)(4.86 * 10^6)}{(20)(0.01 * 10^{-6})(3188.5 + 1736)}}$$

$$= 44.43 * 10^3 rad/sec,\ \text{or}$$

$$= \frac{44.43 * 10^3 rad/sec}{2\pi} \approx 7KHz$$

and

$$d_{\min} = (0.5)(w_n)\left[R_2 C_1 + \frac{N}{K_ø K_{VCO}}\right]$$

$$= (0.5)(44.43 * 10^3) * \left[(1736)(0.01 * 10^{-6}) + \frac{20}{(0.4)(4.86 * 10^6)}\right]$$

$$= 0.6144$$

For N = 2:

$$w_n \max = \sqrt{\frac{(0.4)(4.86 * 10^6)}{(2)(0.01 * 10^{-6})(3188.5 + 1736)}}$$

$$= 140.49 * 10^3 \text{rad/sec}, \text{ or}$$

$$= \frac{140.49 * 10^3 \text{rad/sec}}{2\pi} = 22.36\text{KHz}$$

and

$$d_{max} = (0.5)(140.49 * 10^3) * \left[(1736)(0.01 * 10^{-6}) + \frac{2}{(0.4)(4.86 * 10^6)}\right]$$

$$= 1.292$$

This shows the effect of changing n on loop performance and for this application is adequate.

If the components are not what is desired, choosing a different w_n and/or d allows them to be modified.

Alternatively, picking different C, R_1 or R_2 and recalculating the other parameters can be done. If the filter does not provide adequate performance, making w_n smaller or d larger may improve stability.

Note: Application Note AN535/D can also be found in BR1334/D, Motorola's High Performance Frequency Control Products book, also available through the literature distibution center.

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